

# Notes on Input Design: From Multi-Sine Design to Data-Driven Procedures

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**Abstract**—We show that a class of optimal input design problems have only discrete spectral measures as solutions. If we fix any finite set of possible frequencies then a randomized version of the resulting convex problem has a unique (sparse) solution with probability 1. We also propose a data-driven approach to optimal input design via virtual off-line estimators that coincide with the optimized PE estimator modulo a negligible error, both for open loop and closed loop systems.

**Index Terms**—Closed loop systems, data-driven modeling, performance evaluation, system identification.

## I. INTRODUCTION

INPUT design for linear stochastic control systems is of fundamental importance in many industrial control systems, see [1] for an excellent survey. Remarkably, input design has become central also in machine learning, see [2]. Considering a family of linear stochastic control systems with input  $u$ , parameterized by  $\theta$ , a central issue of input design is to minimize the expected loss in a performance index  $J(\theta)$  due to uncertainty, incurred by replacing the true parameter by its estimate  $\hat{\theta}_N$ , subject to constraints on the input. A preliminary problem is to optimize the information matrix  $M$ , depending linearly on the spectral measure of  $u$ . It is readily seen that this is a convex problem with a unique solution, see (16) and Section II. Thus, the input design problem can be reduced to a generalized moment problem of finding a spectral measure  $d\Phi^u(\cdot)$  such that it generates  $M^u$  via (13) below. This approach has been pursued in [3].

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For practical reasons significant attention has been paid to finding sub-optimal solutions by restricting the search space to a convex set of feasible spectral measures with a density, depending linearly on a parameter  $\eta$  belonging to a compact, convex set in a Euclidean space. A benchmark example is the set of spectral measures of FIR (Finite Impulse Response) processes, with the feasible parameters being the coefficients of the half spectra, constrained by LMI-s (Linear Matrix Inequalities), as first introduced in [4].

In the case of closed loop systems, allowing a LTI (Linear Time Invariant) feedback  $K$ , a preliminary convex optimization problem over the pairs of spectral density and cross spectra,  $(\Phi_u, \Phi_{ue})$ , as variables can be formulated, see [5]. Elaborating this idea  $K$  itself can be treated as an additional design parameter. A smart way of describing the pairs  $(\Phi_u, \Phi_{ue})$  is obtained by using the Youla-Kučera parameterization of  $K$ , leading to a linear parameterization, see [6] for an advanced exposition. A remarkable feature of closed loop identification is that feedback reduces the asymptotic covariance matrix of the estimate of the signal transfer function, see [7].

In this letter we revisit the problem of multi-sine input design, recently attracting renewed interest, see [8]. Our starting point is that the optimization problem can be redefined as a convex optimization problem over the space of spectral measures  $d\Phi^u(\cdot)$  with discrete spectrum subject to energy constraints. In turn, the latter can be approximated with arbitrary prescribed accuracy by a convex design problem over the space of spectral measures  $d\Phi^u(\cdot)$  with support on a fixed set of frequencies. We will establish the remarkable fact that the relaxed version of this problem, obtained by adding the energy constraint multiplied by a freely chosen Lagrange-multiplier, has a unique solution w.p.1 (with probability 1) when the weights are chosen randomly according to a probability law that has a density. This sub-optimal spectral measure can be readily realized by a multi-sine.

An additional issue to be considered is what was called the “Achilles’ heel of optimal input design” in [1], namely the fact that the optimization problem depends on the true system. This paradox has actually been resolved in [9] for ARMAX systems excited by inputs generated by a FIR filter, with a full-scale technical analysis relying on advanced results on recursive estimation given in [10]. In Section IV we reformulate and extend the basic idea of the above paper. The key tool is the definition of a virtual off-line estimator, having a very accurate characterization. Although we can not compute it in

practice, its on-line approximation, obtained along the lines of [11], [12], is computable leading to an adaptive input design method. This data-driven approach is presented first for open loop system. However, it readily generalizes to closed loop systems with a  $\theta$ -dependent feedback loop, obtained for some optimal control problem, yielding the optimal spectral density for the external excitation. As far as we can see our approach is a digression from the main-stream literature, in which the transfer function of the feedback loop is a design variable for the input design problem itself.

## II. TECHNICAL PRELIMINARIES

To be specific, we consider a discrete time single input single output linear stochastic control system with input  $u$ , external noise  $e$  and output  $y$ , defined in the range  $-\infty < n < +\infty$

$$y = H^u(\theta^*, q^{-1})u + H^e(\theta^*, q^{-1})e. \quad (1)$$

Here  $H^u$  and  $H^e$  are rational functions of the backward shift operator  $q^{-1}$  of fixed degrees, depending on a parameter  $\theta$ . We assume  $\theta \in D \in \mathbb{R}^p$ , where  $D$  is an open domain. The true parameter will be denoted by  $\theta^*$ . The associated transfer functions are obtained when replacing  $q^{-1}$  by  $e^{-i\omega}$ .

*Condition 1:* The transfer function  $H^u(\theta)$  is stable, and  $H^e(\theta)$  is stable and inverse stable for all  $\theta \in D$ . Moreover, they are three-times continuously differentiable functions of  $\theta$ . In addition, we assume that the input is delayed 1 unit.

The smoothness condition imposed on  $H^u(\theta)$  and  $H^e(\theta)$  is interpreted via a state-space realization, see also [13].

*Condition 2:* The input process  $u = (u_n)$  and the noise process  $e = (e_n)$ , with  $-\infty < n < +\infty$ , are jointly w.s.st. (wide sense stationary) stochastic processes. Moreover,  $(e_n)$  is a martingale difference process with respect to (w.r.t.) an increasing family of  $\sigma$ -algebras  $(\mathcal{F}_n)$  such that

$$\mathbb{E}[e_n | \mathcal{F}_{n-1}] = 0 \quad \text{and} \quad \mathbb{E}[e_n^2 | \mathcal{F}_{n-1}] = \sigma^2 \quad \text{a.s.} \quad (2)$$

Finally we assume that  $u$  is orthogonal to  $e$ , written as  $u \perp e$ .

For the basic concepts of the theory of w.s.st. processes and system identification see [14], [15], and [16]. It follows that  $e$  is the innovation process of  $y - H^u(\theta^*, q^{-1})u$ .

The spectral distribution measure of  $u$  is denoted by  $d\Psi^u(\omega)$ , with  $-\pi \leq \omega \leq \pi$ . Since it is symmetric, its restriction to  $[0, \pi]$ , with  $d\Psi^u(\{0\})$  and  $d\Psi^u(\{\pi\})$  halved, is denoted by  $d\Phi^u(\omega)$ .

A *multi-sine input*  $u$  is defined as

$$u_n := \sum_{k=1}^t \sigma_k 2 \cos(\varphi_k + \omega_k n) \quad (3)$$

where  $0 \leq \omega_k \leq \pi$  are different, and the random phases  $\varphi_k$  are independent and uniformly distributed in  $[-\pi, \pi]$ . Thus  $d\Phi^u(\cdot)$  is discrete, assigning the energy  $\sigma_k^2$  to each frequency.

To fix notations for the description of the off-line PE (prediction error) estimator of  $\theta^*$  define for any  $\theta \in D$  the assumed innovation process  $\varepsilon(\theta)$  as the w.s.st. process

$$\varepsilon(\theta) = H^e(\theta)^{-1}(y - H^u(\theta)u), \quad (4)$$

defined for  $-\infty < n < \infty$ . Assuming the observations are collected for  $1 \leq n \leq N$  the (idealized) off-line PE method of  $\theta^*$  is then obtained by minimizing the cost function

$$V_N(\theta) := \frac{1}{2} \sum_{n=1}^N \varepsilon_n^2(\theta). \quad (5)$$

The solution will be denoted by  $\hat{\theta}_N$ . A precise definition, taking into account the possibility of no solution or multiple solutions, can be obtained along the lines of [13]. In practice the w.s.st. process  $\varepsilon(\theta)$  is approximated by a process defined via (4) with  $u_n = y_n = 0$  for  $n \leq 0$ . The asymptotic cost function associated with the PE method is then

$$W(\theta) := \frac{1}{2} \mathbb{E} \varepsilon_n^2(\theta). \quad (6)$$

The Hessian of  $W(\theta)$  for  $\theta = \theta^*$  is given by

$$M = M(\theta^*) := \frac{\partial^2}{\partial \theta^2} W(\theta)_{\theta=\theta^*} = \mathbb{E} \varepsilon_{\theta n}(\theta^*) \varepsilon_{\theta n}^\top(\theta^*), \quad (7)$$

where  $\varepsilon_{\theta n}(\theta)$  denotes the gradient of  $\varepsilon_n(\theta)$  w.r.t.  $\theta$ , considered to be a column vector. The system or  $\theta^*$  is *locally identifiable* if  $M$  is positive definite, written as  $M \in \mathbb{R}_+^{p \times p}$ .

*Condition 3:* The system (1) is locally identifiable if the input  $u$  is a w.s.st. orthogonal process, independent of  $e$ . Equivalently, there exists a multi-sine input (3), independent of  $e$ , such that  $M$  is non-singular (see Proposition 1).

Precise conditions for the non-singularity of  $M$  are given in [17]. The existence of an asymptotic covariance matrix of  $\hat{\theta}_N$  is established under a variety of conditions in the literature, see [16]. To ease reference we state two yet unpublished results that can be obtained by straightforward extensions of [13, Th. 2.1]. For the concept of  $L$ -mixing, an extremely useful extension of what was defined as exponentially stable processes in [18], see [19].

*Theorem 1:* Assume Conditions 1, 2 and 3, and let  $M(\theta^*)$  be non-singular. In addition, let  $(u, e)$  be  $L$ -mixing w.r.t. a family of pairs of  $\sigma$ -algebras  $(\mathcal{F}_n, \mathcal{F}_n^+)$ . Then

$$\hat{\theta}_n - \theta^* = -M(\theta^*)^{-1} \sum_{n=1}^N \varepsilon_{\theta n}(\theta^*) e_n + r_N \quad (8)$$

where  $r_N = O_M(N^{-1})$ , indicating that the  $L_p$ -norms of  $r_N$  decay with rate  $O(N^{-1})$  for all  $p \geq 1$ . It follows that

$$\Sigma_{\theta\theta} := \lim_{n \rightarrow \infty} N^{1/2} (\hat{\theta}_n - \theta^*) (\hat{\theta}_n - \theta^*)^T = \sigma^2 M(\theta^*)^{-1}.$$

An extension of this theorem for multi-sine inputs, which are far from being mixing in any sense, can be easily obtained, noting that if  $u$  is a multi-sine, independent of  $e$ , then the products of processes of the form  $D(q^{-1})u$  and  $D(q^{-1})e$  satisfy a law of large numbers with controlled rate.

The Hessian  $M$ , modulo a constant multiplier, is the information matrix. To capture the effect of  $u$  onto  $M(\theta^*)$  consider the gradient process  $(\varepsilon_{\theta n}(\theta^*))$ . Equation (4) gives

$$\varepsilon_\theta(\theta^*) = -H^e(\theta^*)^{-1} (H_\theta^u(\theta^*)u + H_\theta^e(\theta^*)e), \quad \text{or} \quad (9)$$

$$\varepsilon_\theta(\theta^*) = D^u(\theta^*)u + D^e(\theta^*)e, \quad (10)$$

with  $D^u(\theta^*)$  and  $D^e(\theta^*)$  given by

$$D^u(\theta^*, e^{-i\omega}) = -H^e(\theta^*, e^{-i\omega})^{-1} H_\theta^u(\theta^*, e^{-i\omega}), \quad (11)$$

$$D^e(\theta^*, e^{-i\omega}) = -H^e(\theta^*, e^{-i\omega})^{-1} H_\theta^e(\theta^*, e^{-i\omega}). \quad (12)$$

Taking into account that  $u \perp e$ , we get  $M = M^u + M^e$  where  $M^u$  and  $M^e$  are given via the expressions:

$$M^u = 2 \int_0^\pi \Re\left(D^u(e^{-i\omega})D^{u\top}(e^{i\omega})\right) d\Phi^u(\omega), \quad (13)$$

$$M^e = \int_0^\pi D^e(e^{-i\omega})D^{e\top}(e^{i\omega}) d\omega \cdot \sigma^2, \quad (14)$$

where the r.h.s. of (13) is a Riemann-Stieltjes integral. Here the transfer functions  $D^u(e^{-i\omega}) := D^u(\theta^*, e^{-i\omega})$  and  $D^e(e^{-i\omega}) := D^e(\theta^*, e^{-i\omega})$  are explicitly known.

The set of feasible matrices  $M^u$  is defined via (13) with  $d\Phi^u(\omega)$  being arbitrary subject to (s.t.) constraint as follows. Let  $w(\omega)$ ,  $\omega \in [0, \pi]$  be a bounded, continuous function, for which  $w(\omega) \geq w_0 > 0$  for all  $\omega \in [0, \pi]$  holds, and impose

$$\int_0^\pi w(\omega) d\Phi^u(\omega) \leq K. \quad (15)$$

The set of spectral distribution measures  $d\Phi^u(\cdot)$ , satisfying the above the weighted energy constraint, is a compact convex set in the weak topology. Since the matrices  $M^u$  are obtained from  $d\Phi^u(\cdot)$  via a continuous linear operator (13), they also constitute a compact, convex set of symmetric, non-negative definite matrices  $\mathcal{M}^u \subset \mathbb{R}^{p \times p}$ .

Assume that the performance index  $J(\theta)$  is sufficiently smooth in  $\theta$ . Let its Hessian at  $\theta = \theta^*$  be denoted by  $P$ . Obviously  $P^\top = P \geq 0$ . Assume that  $P$  is positive definite. The objective of the input design then is to minimize the asymptotic value of the normalized performance degradation  $\lim_N N\mathbb{E}(J(\hat{\theta}_N) - J(\theta^*))$ . The *primary input design* problem is then to optimize the information matrix  $M$  via

$$\min_{M^u \in \mathcal{M}^u} \text{tr}\left(\left(M^u + M^e\right)^{-1} P\right), \quad (16)$$

with  $\text{tr}(M^{-1}P)$  defined as  $+\infty$ , if  $M \geq 0$  is singular.

It is easily seen that  $M \rightarrow M^{-1}$  is strictly convex on  $\mathbb{R}_+^{p \times p}$  w.r.t. the usual ordering of symmetric matrices. It follows that  $\text{tr}(M^{-1}P)$  is a strictly convex function of  $M \in \mathbb{R}_+^{p \times p}$ . It is readily seen that the optimization problem (16) has a unique solution in  $\mathcal{M}^u$ , to be denoted by  $M^{u*}$ . The question remains how to construct a spectral distribution measure  $d\Phi^{u*}(\cdot)$  or input  $u^*$  that would generate  $M^{u*}$ .

### III. MULTI-SINE INPUT DESIGN

The matrices  $\Re(D^u(e^{-i\omega})D^{u\top}(e^{i\omega}))$ , defining  $M^u$  via (13), are elements of the vector-space of real, symmetric matrices of dimension  $s := p(p+1)/2$ . The following result was essentially stated for the case of  $w(\cdot) \equiv 1$ , in [20, Ch. 3.2, Th. 1]:

*Proposition 1:* Let  $M^u \in \mathcal{M}^u$  be defined in terms of  $d\Phi^u(\cdot)$ , satisfying (15) with equality, via (13). Then there exist at most  $s+1$  frequencies  $0 \leq \omega_k \leq \pi$  and energy levels  $\alpha_k \geq 0$ ,  $k = 1, \dots, s+1$ , such that

$$M^u = 2 \sum_{k=1}^{s+1} \alpha_k \Re\left(D^u(e^{-i\omega_k})D^{u\top}(e^{i\omega_k})\right), \quad (17)$$

$$\sum_{k=1}^{s+1} \alpha_k w(\omega_k) = \int_0^\pi w(\omega) d\Phi^u(\omega) = K. \quad (18)$$

For extremal points of  $\mathcal{M}^u$  just  $s$  frequencies suffice.

The above fact is a folklore in the literature on input design. The proof is based on Carathéodory's theorem, and is given in [20] for the case  $w(\cdot) \equiv 1$ . The general case is readily obtained by introducing the measure  $d\bar{\Phi}^u(\omega) = w(\omega) d\Phi^u(\omega)/K$ , and rewriting (13) as

$$M^u = 2 \int_0^\pi \frac{K}{w(\omega)} \Re\left(D^u(e^{-i\omega})D^{u\top}(e^{i\omega})\right) d\bar{\Phi}^u(\omega).$$

For extremal points of  $\mathcal{M}^u$  the discrete representation (17) is not only a possibility but in some cases a must. Adapting the arguments of [20, Ch. MA3, Th. 2], we get:

*Theorem 2:* Let  $d\Phi^{u*}(\cdot)$  be a spectral measure defining an extremal point of  $\mathcal{M}^u$ , denoted by  $M^{u*}$ . Then there exists a  $p \times p$  matrix  $\Lambda^*$  such that

$$L(\omega) := \text{tr} \Lambda^* \Re\left(D^u(e^{-i\omega})D^{u\top}(e^{i\omega})\right) + w(\omega) \geq 0 \quad (19)$$

for all  $0 \leq \omega \leq \pi$ , and the set of the points of increase of  $d\Phi^{u*}(\cdot)$  is a subset of the solutions of  $L(\omega) = 0$ .

The theorem is a kind of infinite-dimensional Karush-Kuhn-Tucker condition, see Lemma 1.

*Corollary 1:* Let  $w(\cdot)$  be a piece-wise rational function of  $e^{i\omega}$ . Then any optimal spectral measure  $d\Phi^{u*}(\cdot)$  is discrete, supported by a finite number of frequencies.

*Proof of Theorem 2:* Adapting the argument in [20, p. 45] we obtain that  $M^{u*}$  is in the boundary of the convex, closed set  $\mathcal{M}^u$ . Thus, there exists a matrix  $\tilde{\Lambda}$  and a number  $c \neq 0$  such that  $\text{tr} \tilde{\Lambda} M^u \leq c$  for any matrix  $M^u \in \mathcal{M}^u$  and  $\text{tr} \tilde{\Lambda} M^{u*} = c$ . Using the definition (13) of  $M^u$  we can write the above condition as

$$\int_0^\pi \left( \text{tr} \tilde{\Lambda} \Re\left(D^u(e^{-i\omega})D^{u\top}(e^{i\omega})\right) - \frac{c}{K} w(\omega) \right) d\Phi^u(\omega) \leq 0$$

for any  $d\Phi^u(\cdot)$ , for which  $\int_0^\pi w(\omega) d\Phi^u(\omega) = K$  holds. Since the function  $w(\cdot)$  is strictly positive, it follows that  $\text{tr} \tilde{\Lambda} \Re\left(D^u(e^{-i\omega})D^{u\top}(e^{i\omega})\right) - \frac{c}{K} w(\omega) \leq 0$  for  $\omega \in [0, \pi]$ . Setting  $\Lambda = -\frac{K}{c} \tilde{\Lambda}$  we obtain  $\int_0^\pi L(\omega) d\Phi^u(\omega) \geq 0$  for any  $d\Phi^u(\cdot)$ , with equality for  $d\Phi^{u*}(\omega)$ , implying the claim.

Since  $M^{u*} \in \mathcal{M}^u$  is in the boundary of  $\mathcal{M}^u$  Proposition 1 implies that it can be generated via a *multi-sine* of at most  $s$  terms, see (3). The matrix

$$M^u = 2 \sum_{k=1}^s \alpha_k \Re\left(D^u(e^{-i\omega_k})D^{u\top}(e^{i\omega_k})\right), \quad (20)$$

is linear in the  $\alpha_k$ -s, and hence, for a fixed set of  $\omega_k$  frequencies, the cost function  $\text{tr}(M^{-1}P)$  is convex in the  $\alpha_k$ -s. Unfortunately, it is a *non-convex* function in the frequencies  $\omega_k$ ,  $k = 1, \dots, s$ .

A sub-optimal solution to this can be obtained by taking a large  $t$ , and a set of equidistant frequencies denoted by  $\Omega = \{\omega_k: 0 \leq \omega_k \leq \pi, k = 1, \dots, t\}$ , and considering

$$M^u = 2 \sum_{k=1}^t \alpha_k \Re\left(D^u(e^{-i\omega_k})D^{u\top}(e^{i\omega_k})\right). \quad (21)$$

The convex set of matrices  $M^u$  generated by (21), s.t. the energy constraint will be denoted by  $\mathcal{M}^u(\Omega)$ . With this notation our input design problem (16) reduces to the problem with  $M^u \in \mathcal{M}^u$  being replaced by  $M^u \in \mathcal{M}^u(\Omega)$ .

To capture the effect of the approximation replacing  $\mathcal{M}^u$  by  $\mathcal{M}^u(\Omega)$  in the primary input design problem (16) note that any  $M^u \in \mathcal{M}^u$  is defined by a Riemann-Stieltjes integral, given by (13), in which the integrand is continuously differentiable and the total mass of the measure  $d\Phi^u(\cdot)$  on  $[0, \pi]$  is bounded, due to the energy constraint (15) and the condition  $w(\omega) \geq w_0 > 0$  for all  $\omega$ . It readily follows that any  $M^u \in \mathcal{M}^u$  can be approximated by an  $M^{ud} \in \mathcal{M}^u(\Omega)$  with an error of the order  $1/t$ , inducing an error of the same order of magnitude in approximating the optimal value.

Letting  $d_k := D^u(e^{-i\omega_k})$  and  $w_k = w(\omega_k)$  we thus get the following convex optimization problem:

$$\min_{\alpha \geq 0} \operatorname{tr} \left[ \left( 2\Re \sum_{k=1}^t \alpha_k d_k \bar{d}_k^\top + M_e \right)^{-1} P \right] \quad (22)$$

$$\text{s.t.} \quad \sum_{k=1}^t \alpha_k w_k \leq K. \quad (23)$$

The formulation of the the Karush-Kuhn-Tucker condition for (22) – (23) is of didactic interest in light of Theorem 2:

*Lemma 1:* Let  $\alpha^*$  be an optimal solution of (22) – (23). Then there exists a  $p \times p$ , symmetric negative definite matrix  $\Lambda^*$ , and Lagrange multipliers  $\lambda^* \geq 0$  and  $\mu_k^* \leq 0$  such that

$$\operatorname{tr} \left[ \Lambda^* \Re \left( d_k \bar{d}_k^\top \right) \right] + \lambda^* w_k + \mu_k^* = 0, \quad (24)$$

for all  $k = 1, \dots, t$  and  $\alpha_k^* > 0$  implies  $\mu_k^* = 0$ .

*Proof:* Let the cost function in (22) be denoted by  $F(\alpha)$ . Let  $\lambda^* \geq 0$  be the Lagrange multiplier corresponding (23) and let  $\mu_k^* \leq 0$  be the Lagrange multipliers corresponding to the constraints  $\alpha_k \geq 0$ . Let

$$M = M(\alpha) = 2\Re \sum_{k=1}^t \alpha_k d_k \bar{d}_k^\top + M_e. \quad (25)$$

The gradient of the cost function  $F(\alpha)$  is then as follows:

$$\frac{\partial}{\partial \alpha_k} F(\alpha) = 2\operatorname{tr} \left[ -M^{-1} \Re \left( d_k \bar{d}_k^\top \right) M^{-1} P \right]. \quad (26)$$

Letting  $\Lambda = \Lambda(\alpha) := -2M^{-1}PM^{-1}$  we can write:

$$\frac{\partial}{\partial \alpha_k} F(\alpha) = \operatorname{tr} \left[ \Lambda \Re \left( d_k \bar{d}_k^\top \right) \right]. \quad (27)$$

Setting  $\Lambda^* = \Lambda(\alpha^*)$ , the Karush-Kuhn-Tucker condition, implying also  $\mu_k^* \alpha_k^* = 0$ , gives the claim. ■

For a fixed a set of equidistant  $\omega_k$ -s let us consider a *relaxation* of the problem defined in (22)-(23) with  $\gamma > 0$ ,

$$\min_{\alpha \geq 0} \operatorname{tr} \left[ \left( 2\Re \sum_{k=1}^t \alpha_k d_k \bar{d}_k^\top + M_e \right)^{-1} P \right] + \gamma \sum_{k=1}^t \alpha_k w(\omega_k).$$

Let  $\alpha^*$  be an optimal solution of this *relaxed problem*, and let  $\Omega^+ = \{\omega_k: \alpha_k^* > 0\}$ . Then the Karush-Kuhn-Tucker conditions, with minor modifications of Lemma 1, imply for  $\omega \in \Omega^+$

$$\operatorname{tr} \left[ \Re \left( D^u(e^{-i\omega}) \bar{D}^u(e^{i\omega})^\top \right) \Lambda^* \right] + \gamma w(\omega) = 0. \quad (28)$$

Let us introduce the notation for the vectorized matrices

$$\operatorname{vec} \Re \left( D^u(e^{-i\omega}) \bar{D}^u(e^{i\omega})^\top \right) =: \Delta(\omega). \quad (29)$$

*Lemma 2:* The relaxed optimization problem has a solution such that the vectors  $\{\Delta(\omega_k), \omega_k \in \Omega^+\}$  are linearly independent. In particular,  $|\Omega^+| \leq s$ .

*Proof:* Let  $I^+ = \{k: \alpha_k^* > 0\}$ . If the vectors  $\{\Delta(\omega_k), \omega_k \in \Omega^+\}$  are linearly dependent, then there exists a nontrivial linear combination  $\sum_{k \in I^+} \beta_k \Re(d_k \bar{d}_k^\top) = 0$ , where we can assume  $|\beta_k| < \alpha_k^*$  for all  $k \in I^+$ . Adding and subtracting this linear combination from the optimal one that cost function cannot decrease. Thus  $\sum_{k \in I^+} \beta_k w(\omega_k) = 0$ . Taking  $\alpha_k^* + \lambda \beta_k$  for some appropriate  $\lambda$  we can achieve that  $\alpha_k^* + \lambda \beta_k = 0$  for some  $k = l$  while ensuring  $\alpha_k^* + \lambda \beta_k \geq 0$  for all other  $k \in I^+$ , thus reducing the size of  $\Omega^+$ . Repeating this procedure will yield the desired optimal solution. ■

Let  $I \subset \{1, \dots, t\}$  and let  $\alpha_I^\top := (\alpha_k, k \in I)$  denote the reduced parameter vector. Enforcing  $\alpha_k = 0$  for  $k \notin I$ , let  $L_I(\alpha_I)$  be the restricted cost function of the relaxed problem.

*Lemma 3:* Assume that  $\{\Delta(\omega_k), k \in I\}$  are linearly independent. Then the Hessian of  $L_I(\alpha_I)$  is positive definite.

The proof is obtained considering the quadratic form induced by the Hessian for  $v \in \mathbb{R}^I$ , with  $G_k = 2\Re d_k \bar{d}_k^\top$

$$2\operatorname{tr} \left( P^{1/2} M^{-1} \left( \sum_{k=1}^t v_k G_k \right) M^{-1} \left( \sum_{l=1}^t v_l G_l \right) M^{-1} P^{1/2} \right).$$

Restricting summation to  $k, l \in I^+$  gives the claim.

*Theorem 3:* Let the  $t$ -dimensional vector with components  $w_k := w(\omega_k)$  be chosen randomly according to a distribution having a density in  $\mathbb{R}^t$ . Then the relaxed problem has a unique solution w.p.1, and the vectorized matrices  $\operatorname{vec} \Re(D^u(e^{-i\omega}) \bar{D}^u(e^{i\omega})^\top)$ ,  $\omega \in \Omega^+$  are linearly independent w.p.1. In particular, we have  $|\Omega^+| \leq s$ .

*Proof:* Let us take an optimal solution  $\alpha^*$  with  $\Omega^+$  as defined above. Let  $I \subset \{1, \dots, t\}$  be arbitrary and let  $\Omega_I := \{\omega_k, k \in I\}$  be the corresponding subset of frequencies. Note that  $P(\Omega^+ = \Omega_I) \leq P(\Omega_I \subseteq \Omega^+)$ . Express the latter event  $\{\Omega_I \subseteq \Omega^+\}$  via the Karush-Kuhn-Tucker condition as

$$(\operatorname{vec} \Lambda^*)^\top \Delta(\omega) + \gamma w(\omega) = 0 \quad \text{for } \omega \in \Omega_I. \quad (30)$$

Arrange the column-vectors  $\{\Delta(\omega_k), k \in I\}$  into a matrix  $S_I$ , and define  $w_I^\top := (w(\omega_k), k \in I)$ . Write (30) as

$$(\operatorname{vec} \Lambda^*)^\top S_I + \gamma w_I^\top = 0. \quad (31)$$

If  $\operatorname{rank} S_I < |I|$ , i.e., the vectors  $\{\Delta(\omega_k), k \in I\}$  are linearly dependent, then its rows span a proper subspace  $L(S_I) \subset \mathbb{R}^{|I|}$ . But the marginal distribution of the random vector  $w_I$  has a density in  $\mathbb{R}^{|I|}$ , hence the event  $\{w_I \in L(S_I)\}$  has probability 0. Since the number of subsets  $I$  is finite, the second claim follows.

To prove unicity, assume the contrary. Then, by convexity, there is an interval of  $\alpha$ -s such that the cost function is constant, and optimal along this interval. Consider its midpoint, say  $\bar{\alpha}^*$  and let  $I := \bar{I}^+ = \{k: \bar{\alpha}_k^* > 0\}$ , and  $\bar{\Omega}^+ = \{\omega_k: k \in \bar{I}^+\}$ . Then by the proven second claim of the theorem the vectors  $\{\Delta(\omega_k), k \in I\}$  are linearly independent w.p.1. Hence, by Lemma 3 the Hessian of  $L_I(\alpha_I)$  is positive definite. But this is a contradiction, since  $L_I(\alpha_I)$  being constant along an interval, its Hessian has a zero eigenvalue. ■

#### IV. A DATA-DRIVEN APPROACH

A shortcoming of the cited literature on input design is that the optimal spectral measure of the input is determined under the hypothesis that the true system parameter  $\theta^*$ , is actually known. To bypass this paradox we present the basics of a data-driven method within a fairly general context, recapitulating and extending the basic idea of [9].

The key idea is the construction of a data-driven virtual off-line estimator, approximating the off-line PE estimator of Section II, obtained with optimal input, with accuracy  $O_M(N^{-1})$ . To be specific, consider a parametric family of inputs

$$u(\eta) = F(\eta, q^{-1})f, \quad (32)$$

where  $F$  is a rational, stable filter, such that  $|F|^2$  is linearly parameterized by  $\eta \in \mathcal{C} \subset \mathbb{R}^r$ , where  $\mathcal{C}$  is a closed, convex set. E.g.,  $F$  may be a FIR filter with  $\eta$  denoting the coefficients of its half-spectra.  $f$  is an i.i.d. sequence of random variables, independent of  $e$ , with finite moments of all order.

Consider the system dynamics (1) with  $u = u(\eta)$ ,  $\eta \in \mathcal{C}$ :

$$y(\eta) = H^u(\theta^*, q^{-1})u(\eta) + H^e(\theta^*, q^{-1})e. \quad (33)$$

Define, for  $\theta \in D$ , the assumed innovation process  $\varepsilon(\theta, \eta)$

$$\varepsilon(\theta, \eta) = H^e(\theta)^{-1}(y(\eta) - H^u(\theta)u(\eta)). \quad (34)$$

Renaming the cost function of the PE estimator defined in (5) as  $V_N(\theta, \eta)$  let  $\hat{\theta}_N(\eta)$  and  $M(\theta^*, \eta)$  denote the corresponding off-line PE estimator and information matrix, respectively. Assume that for  $\theta \in D$ , as true systems parameter, the optimal input design problem has a unique solution  $\eta^*(\theta)$ , such that  $\eta^*(\cdot)$  is three-times continuously differentiable. Then the *virtual* off-line PE estimator of  $\theta^*$  is obtained by minimizing the cost function

$$V_N(\theta, *) := V_N(\theta, \eta^*(\theta)) = \frac{1}{2} \sum_{n=1}^N \varepsilon_n^2(\theta, \eta^*(\theta)). \quad (35)$$

The solution is denoted by  $\hat{\theta}_N(*)$ . This estimator is virtual in the sense that it is not practical, since  $V_N(\theta, *)$  can not be evaluated for two different values of  $\theta$ . Nevertheless, we proceed with its analysis along the lines of Section II.

Noting that  $\varepsilon(\theta^*, \eta) = e_n$  for all  $\eta$ , we get  $\frac{\partial}{\partial \eta} \varepsilon(\theta^*, \eta) = 0$  for all  $\eta$ . Setting  $\varepsilon_{\theta 0, n}(\theta, \eta) := \frac{\partial}{\partial \theta} \varepsilon_n(\theta, \eta)$ , we conclude:

$$\frac{\partial}{\partial \theta} \varepsilon_n(\theta, \eta^*(\theta)) = \varepsilon_{\theta 0, n}(\theta, \eta^*(\theta)). \quad (36)$$

It follows that for the Hessian of the asymptotic cost function associated with the above virtual PE method, given as,

$$W(\theta, *) := W(\theta, \eta^*(\theta)) := \frac{1}{2} \mathbb{E} \varepsilon_n^2(\theta, \eta^*(\theta)), \quad (37)$$

evaluated at  $\theta^*$ , we have, with self-explanatory notation,

$$M(\theta^*, *) = M(\theta^*, \eta^*(\theta^*)). \quad (38)$$

Once again referring to [13, Th. 2.1] we get by its straightforward extension, in analogy with Theorem 1.

*Theorem 4:* Let  $u(\eta)$  be given by (32). Assume Conditions 1, 3, and let  $M(\theta^*, *)$  be non-singular. Then

$$\hat{\theta}_N(*) - \theta^* = -M(\theta^*, *)^{-1} \sum_{n=1}^N \varepsilon_{\theta 0, n}(\theta^*, \eta^*(\theta^*))e_n + r_N,$$

where  $r_N = O_M(N^{-1})$ , implying the strong approximation:

$$\hat{\theta}_N(*) = \hat{\theta}_N(\eta^*(\theta^*)) + O_M(N^{-1}). \quad (39)$$

In particular, the asymptotic covariance matrix of  $\hat{\theta}_N(*)$  is

$$\Sigma_{\theta\theta}(\theta^*) = \sigma^2 M^*(\theta^*, *)^{-1} = \sigma^2 M^*(\theta^*, \eta^*(\theta^*))^{-1}.$$

Thus the virtual estimator  $\hat{\theta}_N(*)$  is optimal from the perspective of input design. The asymptotic estimation problem in the spirit of [12] is defined by the algebraic equation

$$\frac{\partial}{\partial \theta} W(\theta, *) = \mathbb{E} \varepsilon_{\theta 0, n}(\theta, \eta^*(\theta)) \varepsilon_n(\theta, \eta^*(\theta)) = 0. \quad (40)$$

Following the ideas of [11], extended in [12], a computable recursive PE estimator  $\hat{\theta}_N(*)$  can be constructed.

The viability of the proposed approach for data-driven input design has been demonstrated, with all technical details included, in [9] for the case of ARMAX systems excited with inputs  $u$  generated by a FIR filter.

To conclude this section we briefly describe the extension of the above approach to *closed loop* systems. Consider a class of linear stochastic control systems with excitation  $v$ :

$$y^c(\theta') = H^u(\theta^*, q^{-1})u^c(\theta') + H^e(\theta^*, q^{-1})e \quad (41)$$

$$u^c(\theta') = -K(\theta', q^{-1})y^c(\theta') + v. \quad (42)$$

Here  $v$  is an external excitation independent of  $e$ . We consider the practical scenario when the true parameter  $\theta^*$  is unknown and we use its tentative value  $\theta'$  in the feedback loop. The feedback loop or  $K(\theta, q^{-1})$  is designed by optimizing a performance criterion for any assumed  $\theta$  showing up in  $H^u$  and  $H^e$ . Thus if we had a prior estimate  $\hat{\theta}$  of  $\theta^*$  we would set  $\theta' = \hat{\theta}$ . Write (41) - (42) as

$$y^c(\theta') = H^{cu}(\theta^*, \theta')v + H^{ce}(\theta^*, \theta')e, \quad (43)$$

with  $H^{cu}(\theta^*, \theta')$  and  $H^{ce}(\theta^*, \theta')$  denoting the closed loop filters. The role of the dither  $v$ , being independent of  $e$ , is thus identified with that of the input  $u$  in open loop identification. Thus, pretending the knowledge of  $\theta^*$  (and knowing  $\theta'$ ) we can proceed with any of the open loop input design methods.

Following (32) assume that  $v$  is generated by

$$v(\eta) = F(\eta, q^{-1})f, \quad (44)$$

yielding the input and output processes  $u^c(\theta', \eta)$  and  $y^c(\theta', \eta)$ . For fixed  $\theta', \eta$  the off-line PE estimator of  $\theta^*$  is obtained via the assumed innovation process defined by

$$\varepsilon^c(\theta, \theta', \eta) = H^e(\theta)^{-1}(y^c(\theta', \eta) - H^u(\theta)u^c(\theta', \eta)).$$

The off-line PE estimator is then defined as the solution of

$$\min_{\theta \in D} \sum_{n=1}^N \varepsilon_n^2(\theta, \theta', \eta), \quad (45)$$

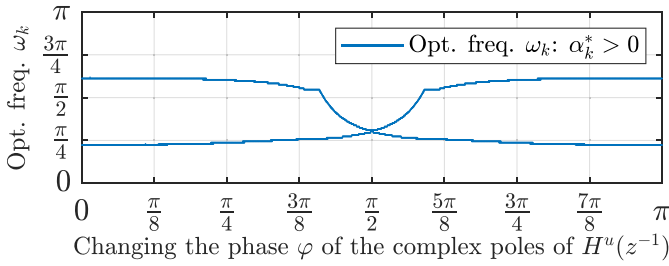


Fig. 1. The two optimal frequencies for  $b = 3.0$  and  $\omega_c = \frac{3\pi}{4}$ .

to be denoted by  $\hat{\theta}_N(\theta', \eta)$ , which can be analyzed along the lines of Section II. For any  $\theta, \theta'$  let the solution of the input design problem be denoted by  $\eta^*(\theta, \theta')$ . We redefine the assumed innovation process by enforcing  $\theta' = \theta$  and  $\eta = \eta^*(\theta, \theta')$ . Thus we define a virtual closed loop off-line PE estimator, as in [21], which can be considered as the off-line mirror-image of an adaptive control algorithm optimized for the asymptotic covariance matrix of  $\hat{\theta}_N(\theta^*, \eta)$ , by

$$\min_{\theta \in D} \sum_{n=1}^N \varepsilon_n^c(\theta, \theta, \eta^*(\theta, \theta)). \quad (46)$$

Let the solution be denoted by  $\hat{\theta}_N(*, *)$ . Noting that  $\varepsilon^c(\theta^*, \theta', \eta) = e_n$  for all  $\theta', \eta$ , the partial derivatives of  $\varepsilon^c(\theta^*, \theta', \eta)$  w.r.t.  $\theta', \eta$  are 0, and hence the gradient of the cost function or rather  $(\partial/\partial\theta)\varepsilon_n^c(\theta, \theta, \eta^*(\theta, \theta))_{\theta=\theta^*}$  is easily computed. Thus, in analogy with Theorem 4 we get the strong approximation result

$$\hat{\theta}_n(*, *) = \hat{\theta}_n(\theta^*, \eta^*(\theta^*)) + O_M(N^{-1}), \quad (47)$$

amounting to the fact that  $\hat{\theta}_n(*, *)$  is optimal both from control and input design perspective.

## V. EXPERIMENTAL RESULTS

We have tested our algorithm for finding the optimal multi-sine on a system modeling a lightly damped oscillator with complex poles  $re^{\pm i\varphi}$  and amplification  $b$ . Thus we have

$$H^u(z^{-1}) = \frac{b}{1 - 2r \cos(\varphi)z^{-1} + r^2z^{-2}}. \quad (48)$$

Fixing  $r = 0.95$ , we let the phase vary uniformly in  $[0, \pi]$ , while  $b$  varied in the interval  $[3, 10]$ . The transfer function  $H^e$  is defined by its stable zeros and poles yielding

$$H^e(z^{-1}) = \frac{1 + c_1z^{-1} + c_2z^{-2}}{1 + d_1z^{-1} + d_2z^{-2}} = \frac{1 + 0.6z^{-1} - 0.07z^{-2}}{1 - 0.866z^{-1} + 0.25z^{-2}}.$$

Thus we have  $p = 7$  parameters:  $r, \varphi, b$  and  $c_1, c_2, d_1, d_2$ , implying  $s = p(p+1)/2 = 28$ . For the weight function  $w(\cdot)$  we use a sigmoid-type functions taking their values between 0.1 and 1.0, setting their medians equal to three possible cut-off frequencies  $\omega_c$  equal to  $\frac{\pi}{4}, \frac{\pi}{2}, \frac{3\pi}{4}$ . We let  $t = 5s = 140$ . We solved the relaxed problem with  $P = I$ , and  $\gamma = 0.1$ . In all experimental scenarios a sparse solution was obtained with a maximum of 4 optimal frequencies. In Fig. 1, we present a typical result with two optimal frequencies assuming a moderate SNR (signal-to-noise ratio)  $b = 3.0$ , and using a weight function with broad band-pass width:  $\omega_c = \frac{3\pi}{4}$ .

## VI. DISCUSSION

A nice project for future research may be the extension of Theorem 2 to input design problems admitting frequency-wise specifications, introduced in [22]. A second problem of interest may be the clarification if the proposed data-driven approach of Section IV is applicable for multi-sine design. Extension of our results to vector-valued multi-sine design along the lines of [23] may be also of interest. Finally, the authors thank to Hakan Hjalmarsson for inspiring this letter, while visiting HUN-REN SZTAKI in 2021.

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