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## RESEARCH ARTICLE

# Beam-Steering Antenna Technique Using Operational Amplifiers for Sub-6 GHz

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**ABSTRACT** A methodology for beam-steering using operational amplifiers (Op-amps) is presented. Continuous steering is required in various advanced applications and its implementation necessitates additional efforts since singularly control of the feeding of the radiators is mandatory for both phase and amplitude. The present work proposes a technique for generating the required sequence of the feeding signal using two Op-amps for each input port. It leads to generating incremental phases with sequential Op-amps without any limitation in the value of the phase differences, controlled by the bias voltage applied to the Op-amps, hence giving rise to a continuous beam-steering capability. The study case consists of a four-stage oscillator designed for creating a sequence of signals with progressive phase shifts between consecutive outputs. The general scheme allows continuous control of the phase differences here applied for generating a uniform, i.e., constant signal magnitude, feeding sequence. This set of signals is then used to feed a four-element microstrip array operating at 1.2 GHz. The effectiveness of the method is validated by numerical simulation of the array performances. Additionally, the low power consumption of active Op-amps, easy implementation, and high sensitivity are characteristics of the presented paradigm.

**INDEX TERMS** Active devices, beam-steering, operational amplifier (Op-amp), oscillator, phase manipulation.

## I. INTRODUCTION

In radio and radar systems, beam-steering refers to altering the direction of the main lobe of a radiation pattern. This can be obtained by changing the relative phases of the single radiators with respect to a reference one [1], [2], [3], [4]. The beam-steering techniques result in reducing the interference and enhancing the gain and directivity of the antennas [5], [6], [7]. Recently, various innovative methods have been proposed to achieve beam-steering and in the following, a short review of some of them is reported.

In [4], a passive system for discrete and continuous beam steering with planar dielectric phase transformers is presented. A procedure based on the use of two perforated dielectric structures collocated in the near-field region of an

antenna having a fixed beam is discussed in [8]. In other studies, [9], [10], a frequency-diverse array is detailed; its working principle is based on the range- and angle-dependent directional modulation. An optically controlled system is described in [11] that is investigating the fast-switching approach for orbital angular momentum. In [12], a beam-steering control method is described leading to the design speedy maneuvering platform for synthetic aperture radar imaging and to reduce Doppler bandwidth. Scarborough et al. [13] present a method for reducing the computational domain of traveling-wave modulated structures for beam-steering and amplification.

Although there are various modi operandi targeting beam-steering, the most challenging problem of generating a continuous phase control is still not fully solved. The present dissemination aims to contribute to this open question. To the best of the authors' knowledge, a beam-steering methodology

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with active Op-amps leading to generate various phases with no limitation to  $2^N$  radiating elements is proposed for the very first time. In this method, an arbitrary number stage oscillator structure with two amplifiers in each stage is generated for producing various sequentially incremental phases. The achieved phases are inserted into the far-field analysis of a microstrip array working at 1.2 GHz. The simulation environments for generating phases with Op-amps and for performing the far-field analysis are LTSpice and Microwave Studio (Dassault Systèmes), sequentially. Even if the case study considers a  $2^2$  configuration, the presented method can be applied to an arbitrary number of radiators.

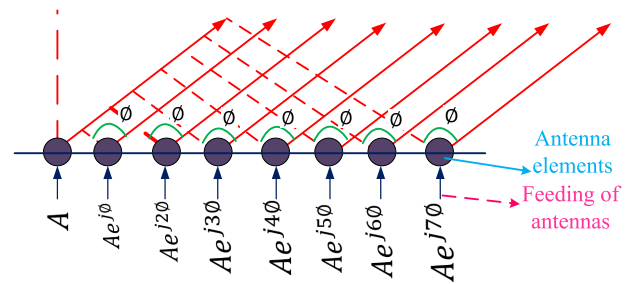
The paper is organized as follows: Sec. II, presents the proposed methodology for generating the progressive phase shift between consecutive output ports of the active circuit. These phases represent the input for the array elements to realize the required beam-steering. Section III is devoted to providing the numerical validation of the proposed method, while Sec. IV concludes the discussion.

## II. PROPOSED METHODOLOGY IN A NUTSHELL

This section is devoted to presenting the proposed method for generating the continuous phases required for the beam-steering of a linear array. The wording “beam-steering” refers to the possibility of the antenna changing the direction of the main beam; i.e., to generate the highest power density in a given direction in the space. Phased array antenna [4] are a classical example. The steering is obtained by proper selection of the phases of the single radiators; usually, one of them is considered as a reference. However, the overall radiation pattern, including the angular displacement of the main beam, also depends on the distance between the radiators, which in the simplest case is considered equal. A constant phase difference  $\Delta\phi$  between consecutive radiators corresponds to a linear phase error. Figure 1 presents the phase front of the radiated fields by the different radiators for a uniform, equispaced array with constant phase shifts between them. In such a situation, according to the Fourier theory, the results will be a shift in space of the initial pattern of the array, i.e., that obtained for  $\Delta\phi = 0$ . Depending on the amount of steering, the beam will also suffer some distortions; a non-symmetric pattern with respect to the main direction and a reduction of the gain are the most imminent manifestations.

From an application point of view, considering  $2^N$  radiators can be useful since equal length beam forming network (BFN) will ensure the same phase for each radiator using a single source. In such case, each arm can be equipped with a single phase shifter, that is individually controlled to impose the required phase for the considered radiator. The effect of the BFN is strongly reduced. However, this solution presents a limitation on the number of radiators. The proposed solution described below overcomes this problem.

The method proposed here consists of generating the single phases using a sequence of cascaded Operational amplifiers (Op-amps). A feed-back circuit applied to each Op-amp will



**FIGURE 1.** The concept of beam-steering: different elements are fed by different phase signals. The representation refers to an equi-spaced array configuration with a uniform (constant amplitude  $A$ ) feeding signal with a progressive phase between consecutive radiators ( $\phi$ ).

give rise to oscillators that are cascaded in such a way as to obtain a progressive summation of the single phases of the different Op-amp outputs. The general structure of the oscillator is presented in Fig. 3. In the electronic field, the oscillators refer to the designs for generating the output signal with constant amplitudes and include both active and passive elements. The main objective of the oscillators is to convert DC voltage into a periodic AC signal.

Applying Op-amps theory, the gain of the oscillator for a frequency dependent feedback, can be expressed as (1):

$$A_f(s) = \frac{A(s)}{1 - B_f(s)A(s)} \quad (1)$$

For sustained oscillations, at the resonant angular frequency  $\omega = \omega_0$  the “Barkhausen criteria” must be satisfied [14]. Equation (2) expresses the condition to fulfil this criteria where  $\Phi(\omega_0)$  is the phase of  $B_f(\omega_0)A(\omega_0)$ .

$$|B_f(\omega_0)A(\omega_0)| e^{j\Phi(\omega_0)} = 1 \quad (2)$$

Figure 2 reports the concept of the methodology for generating non-limited phases by using active Op-amps. For generating  $N$  phases such as  $\Phi_n = n\Phi(\omega_0)$ ,  $n \in (0, \dots, N - 1)$ ,  $N$  stage oscillators is required. The proposed method is quite general since the number of back-to-back Op-amps can be increased without any limitation according to the number of radiators.

In the present investigation, identical ‘LTC6269-10’ (Linear Technology) Op-amps have been considered and the employed diodes behave as capacitors for feedback. This model of Op-amp is selected by considering the operational frequency band of the antenna, and by getting the help of Op-amps’s data sheet [15].

The circuits in the blue boxes in Fig. 2, i.e., the second Op-amp at each stage, are used for high-frequencies that are keeping the clipping and oscillating [16]. As Eq. (3) presents, the  $R_f$  is the feedback resistor and the  $R_{in}$  is the input impedance of the amplifier. Hence for our proposed design,  $R_4$  denotes to feedback resistor and  $R_3$  affects the input resistor of the design. For this case,  $R_4$  must be larger than  $R_3$  as for Eq. (3).

$$V_{out} = -I_{in}R_f = -\left(\frac{R_f}{R_{in}}\right)V_{in} \quad (3)$$

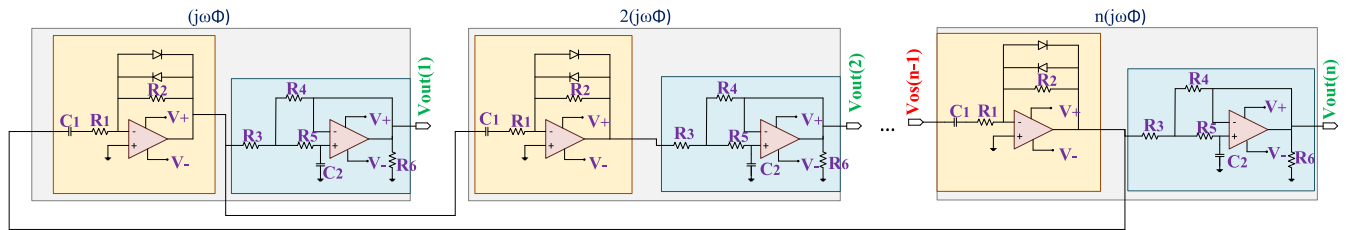


FIGURE 2. Proposed Op-amp based phase generation as a method for beam-steering.

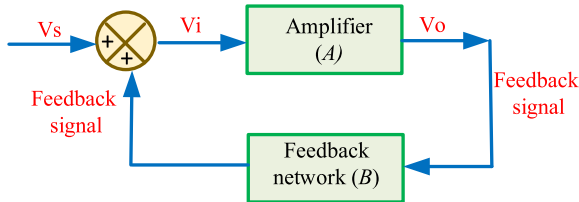


FIGURE 3. General concept of oscillator structure with a voltage gain of "A" and a positive feedback network with feedback gain of "B."

In our design  $R_6$  is the input impedance of the microstrip antenna, here considered equal to  $50 \Omega$ . However, a dispersive value, reporting the actual active impedance of the single patches can be incorporated into the model.

### III. VALIDATION OF THE SUGGESTED PARADIGM

This section presents the practical simulation results of the proposed methodology leading to generating non-limited phases through Op-amp bases phase shifters. Successively, these values are considered in an electromagnetic analysis.

In this work, the design of beam steering at 1.2 GHz frequency is targeted. For this purpose, a 4-element antenna array working at 1.2 GHz has been designed (see Fig. 4 for the sketch and the Computer-Aided Design (CAD) model). It includes four square patch radiators, and each of them is fed individually by a coaxial cable. The considered substrate is characterized by the following specifications:  $\tan \alpha = 0.044$ ,  $\epsilon_r = 1.3$ , and a thickness of 0.17 mm.

Separately, a four-stage oscillator has been implemented. It provides the four incremental phases that have been considered in the analysis. For this case, four-stage amplifiers are sequentially connected; feedback that connects the output to the input is also present. In simple words, we use four-stage oscillators to generate  $\Phi(\omega)$ ,  $2\Phi(\omega)$ ,  $3\Phi(\omega)$ , and  $4\Phi(\omega)$  phases, respectively. The overall structure is biased with two DC voltage sources namely:  $V+$  and  $V-$ . For the determined design goals, i.e., having beam-forming at 1.2 GHz and generating four sequential phases, the optimal design parameters according to Eqs. (1-2) have been determined. Table 1 presents these optimal design parameters for generating four sequential phases at 1.2 GHz.

Regarding Eq. (3), we assume that  $R_4$  and  $R_3$  are 1.6 k $\Omega$  and 0.5 k $\Omega$ , respectively. Additionally,  $R_5$  is determined to be 1 k $\Omega$  as it provides well-performance to the whole design in terms of sensitivity.

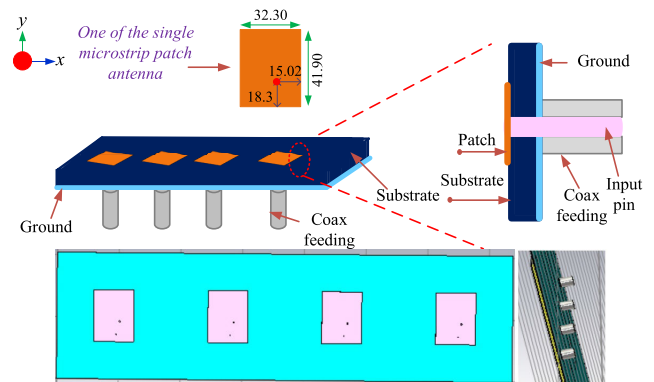


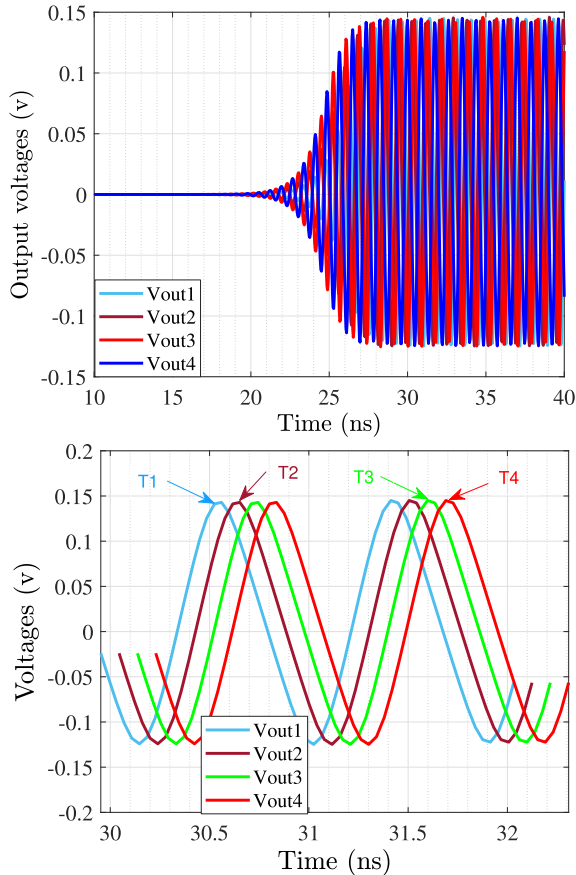
FIGURE 4. Four antenna arrays that are feeding by coax cable sketch (top), CAD model of the antenna with patches, and individual coaxial feedings (bottom).

TABLE 1. Optimal values of proposed beam-steering through active Op-amps presented in Fig. 2.

| parameter | value             | parameter | value             |
|-----------|-------------------|-----------|-------------------|
| $R_1$     | 22 (k $\Omega$ )  | $R_2$     | 47 (k $\Omega$ )  |
| $R_3$     | 0.5 (k $\Omega$ ) | $R_4$     | 1.6 (k $\Omega$ ) |
| $R_5$     | 1 (k $\Omega$ )   | $R_6$     | 50 (k $\Omega$ )  |
| $C_1$     | 100 (nF)          | $C_2$     | 40 (nF)           |

In the "s" domain,  $B_f(s)$  is defined as  $\left(\frac{s + R_{in}C}{1 + sR_{in}C}\right)^4$  where  $R_{in}$  is the input impedance of each stage of oscillator. Indeed,  $A_f(s)$  is also defined approximately by the  $\frac{R_4}{R_3}$ . For satisfying the condition in Eq. (2),  $C_2$  is determined to be between 40 nF - 60 nF; here we prefer using the smallest value capacitor. Lastly, for having the oscillation the  $R_2 = 2R_1$  constrain must be fulfilled.

After inserting the optimal design parameters, the whole Op-amp-based phase shifter has been simulated. Based on the simulation output, firstly  $T_1$ ,  $T_2$ ,  $T_3$ , and  $T_4$  have been extracted that represent the time value at the maximum magnitude for first, second, third, and fourth stages. They are used to determine the phases associated with the delay of the signal. Figure 5 (top) presents the simulation results of the Op-amp-based phase shifter; output voltages, including the transient time, between 10 (ns) and 40 (ns) are reported. The plot illustrates the various output specifications namely as  $V_{out1}$ ,  $V_{out2}$ ,  $V_{out3}$ , and  $V_{out4}$ . For better visualization, Fig. 5 (bottom) shows in detail the magnified version of Fig. 5 (top) in the 30 ns to 33 ns interval. Continuously, Tab. 2 reports the time differences between the sequential outputs namely  $T_2 - T_1$ ,  $T_3 - T_2$ , and  $T_4 - T_3$  for four different DC



**FIGURE 5.** Performances of the proposed Op-amp based phase delay generation. (0-40 ns (top) and zoom for the 30 ns - 33 ns interval (bottom)).

**TABLE 2.** Time delay of the different outputs for various values of the control voltages; units are (V) and (ns).

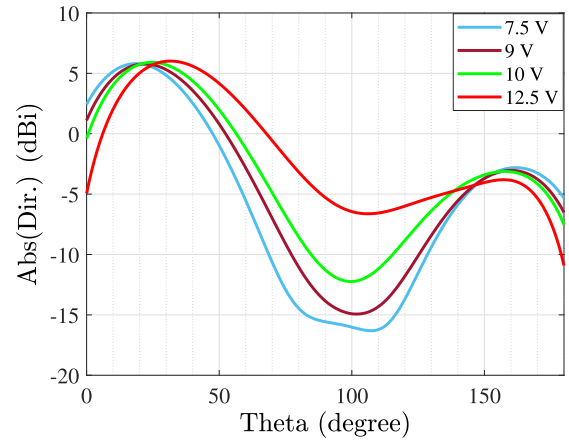
| V+ Or -(V-) | T <sub>1</sub> - T <sub>2</sub> | T <sub>3</sub> - T <sub>2</sub> | T <sub>4</sub> - T <sub>3</sub> |
|-------------|---------------------------------|---------------------------------|---------------------------------|
| 7.5         | 0.09                            | 0.10                            | 0.10                            |
| 9           | 0.09                            | 0.13                            | 0.10                            |
| 10          | 0.13                            | 0.11                            | 0.15                            |
| 12          | 0.18                            | 0.15                            | 0.15                            |

voltages as 7.5 V, 9 V, 10 V, and 12 V. As expected, the time variation between sequential outputs are approximately the same for all values of the control voltage.

After the determination of the time-variant, the phase variant is achieved from various DC voltage sources. For this case, equation  $\Delta\Phi = 360f\Delta T$  ( $^\circ$ ) is used, where  $f$  indicates the frequency, and  $\Delta T$  is the time variance (i.e.,  $T_n - T_{n-1}$ ). Table 3 presents the various achieved values for the first, second, third, and fourth phases, respectively, for various control voltages. These phases are set in the Microwave Studio (Dassault Systèmes) post-processor utility and used to excite the microstrip array elements under unitary amplitude conditions. The main lobe direction has been monitored. As expected, the phases for each voltage are increasing sequentially which results in incremental steering of the main lobe direction. Figure 6 presents the radiation pattern of the antenna in Fig. 4 for different control voltages present in Tab. 3.

**TABLE 3.** Summary of the beam steering performances for different control voltages and associated phases applied to the individual radiators @ 1.2 GHz. The 1<sup>st</sup> radiator is considered as reference.

| Voltages (V) | $\Phi_1$ | $\Phi_2$ | $\Phi_3$ | $\Phi_4$ | Lobe direction |
|--------------|----------|----------|----------|----------|----------------|
| 7.5          | 0        | 39.86    | 86.54    | 130.30   | 19 $^\circ$    |
| 9            | 0        | 42.78    | 101.61   | 147.08   | 22 $^\circ$    |
| 10           | 0        | 56.68    | 106.52   | 173.18   | 25 $^\circ$    |
| 12           | 0        | 78.76    | 144.84   | 212.67   | 32 $^\circ$    |



**FIGURE 6.** Directivity for various DC supply voltages.

In the proposed design, by altering the DC supply voltages the phases are also differing respectively. For instance, as Tab. 3 shows, when a DC supply voltage of 9 V is considered the circuit generates 0, 42.78 $^\circ$ , 101.61 $^\circ$ , and 147.08 $^\circ$  phases, respectively. By augmenting the voltage (see row for 10 V in Tab. 3) the phases are altering and increasing: in particular 0, 56.68 $^\circ$ , 106.52 $^\circ$ , and 173.18 $^\circ$  phases have been obtained. Additionally, Tab. 3 proves the accuracy of the method whereby by altering the phases, the main lobes are also controlled in a desired way. One can note, that as expected, the increasing tilt angle introduces a variation at side-lobe level as well. Controlling of such dependence can be incorporated in the generation of the phase values, and represent one of the future aspects. These increments result in the steering of the main lobe direction of the considered array. The corresponding steering angles are reported in the last column of Tab. 3. For the circuit designs including Op-amps, considering signal-to-noise ratio (SNR) specification plays an important role. The selected Op-amp (here, ‘LTC6269-10’) includes a FET-input operational amplifier with low input bias current and low input capacitance. Hence, it characterizes low input-referred current noise and voltage noise [15]. Figure 7 presents the overall SNR performance of four-stage amplifiers in which the SNR value varies between 64.7-71.8 dB for the voltages from 7.5-12 V.

Additionally to underline the novelty of the proposed method, Tab. 4 is provided. As it is clear, the presented method in this study is proposed for the very first time in the literature leading to the employ of active devices in the field of antenna technology and beam-steering methods.



TABLE 4. Summary of various reported beamforming techniques in the literature.

| Ref.             | Method   | Goal(s)  | Performance metrics   |
|------------------|--|--|---|
| [17]             | Design of linear antenna array with integrated butler matrix beamforming network         | - Generating four beams in four different directions used for 5G applications  | Steered in: 40°, 15°, +15°, and +45°  |
| [18]             | Design of whole array with adaptive digital beamforming                                  | - Dividing whole array into subarrays and multiple phase centers results in accurate estimation of angle of arrival for the signal source  | Direction of arrival as: 29.82°, 30.59°, 31.99°                                   |
| [19]             | Presenting a steerable differential beamformer for linear acoustics vector sensor arrays | - Solving the problem of non-steerable beam patterns of linear arrays  | Steering angle as: 0°, 30°, 60° and 90°   |
| [20]             | Presenting echo separation scheme with digital beamforming and bandpass filtering        | - Resulting in high-efficiency echo separation for the spaceborne multiple-input and multiple-output (MIMO) synthetic aperture radar   | Bore-sight angle as: 28°  |
| [21]             | Design of broadband 16-way two-dimensional Butler matrix-based beamforming network       | - Enhancing in size and bandwidth  | Phase difference fluctuation as: ±21°   |
| [22]             | Presenting the beampattern matching design technique                                     | - Much faster compared to the well-known traditional semidefinite quadratic programming counterpart  | Range of angle as: [90° ≈ 90°]  |
| [23]             | Presenting the harmonic-based MIMO transceiver based on the time-modulated array         | - Linearly mapping the actual multipath channels between multiple users and the antenna elements   | Angle of arrival as: 0°/30° for a special case and 4°/25° for a more general case |
| <b>This work</b> | <b>Generating diverse continuous phases via active Op-amps</b>                           | - <b>Controlling an arbitrary number of radiators;</b><br>- <b>Generating phases without limitation in the value of the phase differences;</b><br>- <b>Generating constant signal magnitude and feeding sequence</b> | <b>No limitation in phase differences and all phases are continuous</b>           |

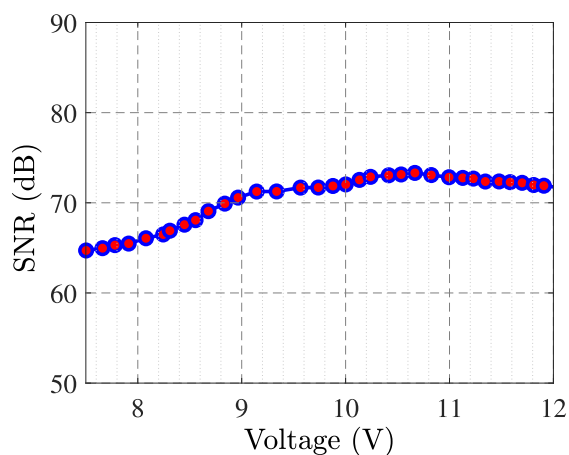


FIGURE 7. SNR value versus voltages.

IV. CONCLUSION

A method to generate continuous beam-steering for a linear array has been presented. For the very first time in the literature, this dissemination presents a novel concept in creating various continuous phases through active Op-amps. The design of the proposed active RF circuit incorporating an oscillator and clipping has been presented; it allows for generating various phases continuously. The paradigm permits sequential connection of a non-limited number of oscillator stages hence controlling an arbitrary number of radiators. Using Op-amps leads to having few external components with reduced design size. For validating the proposed procedure, a four-stage oscillator leading to generating four sequential phases has been presented and these phases are controlled by changing the DC supply voltage. The simulation results verify that the main lobe direction of the

considered printed linear patch array is incrementally increasing for crescent DC supply voltage. The presented method in this study is suitable and adaptable to be implemented for all larger antenna arrays by designing a compatible Op-amp-based phase generator in terms of frequency and operational bandwidth. Additionally, by paying attention to the operated bandwidth, various strategies for enhancing the SNR value can be executed.

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