

# Robust Beamforming Design for Integrated Sensing and Communication Systems

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Abstract—Integrated sensing and communication (ISAC) can improve spectral, energy, and transmission efficiency. To overcome the impact of channel uncertainties, we investigate a robust beamforming design problem for a multiple-input single-output based ISAC system with imperfect channel state information (CSI), where a multiantenna base station (BS) serves multiple wireless users and obtains state information of a point target. Based on bounded CSI error models, a total throughput maximization problem is formulated under the constraints of the minimum rate threshold of each communication user, sensing performance based on Cramér-Rao lower bound thresholds, and the maximum transmit power of the BS. The formulated problem with parameter perturbations belongs to a nonconvex one that is challenging to solve. To address this complexity, an iterative robust beamforming algorithm is designed by employing S-procedure, semidefinite relaxation technique, Schur complementarity conditions, and successive convex approximation. Simulation results demonstrate that the proposed algorithm exhibits better convergence and stronger robustness.

**Index Terms**—Integrated sensing and communication (ISAC), robust beamforming, throughput maximization.

## **N**OMENCLATURE

ISAC Integrated sensing and communication.

BS Base station.

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RCC Radar communication coexistence.
DFRC Dual-function radar communication.
LFM Linear frequency modulation.

PSK Phase-shift keying.

CPM Continuous phase modulation.

SF Step frequency.

OFDM Orthogonal frequency division multiplexing.

MIMO Multiple-input multiple-output. MUSIC Multiple signal classification.

SINR Signal-to-interference-plus-noise ratio.

CRLB Cramér-Rao lower bound.

SCA Successive convex approximation.

CSI Channel state information.

MISO Multiple-input single-output.

SDR Semidefinite relaxation.

#### I. INTRODUCTION

ITH the growing number of communication users and the rising demand for various sensing services, spectrum resources have become exceptionally congested. Moreover, the mutual interference between terminals has pushed the corresponding performance close to theoretical limits [1], [2], [3]. To address these challenges, integrated sensing and communication (ISAC) has surfaced as a cost-effective solution, injecting new momentum to tackle the issues at hand. Specifically, the objective of ISAC is to tightly integrate sensing and wireless communication by sharing spectrum, hardware platforms, and signal processing frameworks, aiming for performance equilibrium and maximizing gains [4], [5], [6]. ISAC significantly enhances both spectrum and energy efficiency, concurrently curbing hardware costs and system power consumption.

Currently, ISAC systems are broadly classified into radar communication coexistence and dual-function radar communication (DFRC). The former employs separate waveforms, enhancing spectrum utilization by sharing communication and radar spectrum resources with minimal modifications required for existing hardware facilities [7], [8], [9]. However, its implementation requires clever design of transmission waveforms for both communication and radar to effectively control interference, leading to a higher level of signal processing complexity [10], [11]. In contrast, DFRC employs the same transmitter to produce dual-function waveforms in the same frequency band, significantly improving spectrum efficiency while reducing the

complexity of signal processing [12], [13]. Nevertheless, the DFRC system still presents several key issues that require further exploration, such as how to design waveforms to balance communication and radar sensing functionalities.

#### A. Related Works

Therefore, more and more scholars have started to work on the waveform design for realizing ISAC systems. Based on the existing works, the literature review on waveform design in ISAC systems can be classified into the following three types.

1) Sensing-Centric Waveform Design: Sensing-centric waveform design aims to fully utilize existing sensing waveforms to simultaneously implement additional communication functions. As sensing waveforms typically do not directly carry modulation information, a common approach is to embed signaling information into the sensing waveforms, thus realizing both communication and sensing functions [14], [15], [16], [17], [18], [19], [20], [21], [22]. Specifically, Xie and Luo [14] proposed a design approach to modulate minimum frequency-shift keying signals onto linear frequency modulation (LFM) pulses. They discussed the relationship between signal power leakage and modulation data when the radar receiver bandwidth approximated the transmission signal bandwidth, and a method was suggested to eliminate power leakage by abandoning a certain channel capacity. However, the use of low-order modulation resulted in a relatively lower communication rate. In addition, modulating communication data into LFM signals using phase-shift keying (PSK) to achieve integrated waveforms is also an area of interest for researchers [15], [16]. Because PSK-LFM exhibits excellent constant-envelope characteristics, enabling efficient utilization of high-power amplifiers to generate integrated signals without causing significant nonlinear distortion. In [17], researchers devised an LFM signal based on continuous phase modulation (CPM) to address the issue of low spectral efficiency caused by the discontinuity in the phase of PSK-LFM. In [18] and [19], low-density parity-check codes and precoding techniques were, respectively, employed to design CPM-LFM waveforms, further enhancing spectral efficiency. However, the above single-carrier waveform design approaches struggle to achieve high data rates and bandwidth utilization while maintaining perceptual performance. Therefore, Han et al. [20] proposed a method based on step frequency (SF). SF signals are easy to generate and can provide large bandwidth and high resolution [21]. Nonetheless, ensuring radar performance remains unaffected by communication data proves challenging. To address these issues, Gaglione et al. [22] introduced pseudorandom sequences to improve spectral efficiency and reduce interdevice interference.

2) Communication-Centric Waveform Design: Orthogonal frequency division multiplexing (OFDM) has gained widespread application in the field of communication due to its advantages, such as resistance to multipath fading, high modulation efficiency, and wide bandwidth. It has also become a significant topic in the research on ISAC shared waveform design [23], [24], [25], [26], [27], [28], [29].

Liu et al. [23] proposed an ISAC system based on OFDM. By compensating and decohering the echoed information, they utilized subspace projection to achieve high-resolution joint estimation of target distance and velocity. Moreover, Yang et al. [24] utilized dynamic constellation expansion to adjust the positions of constellation points, reducing the probability of co-phase occurrence and consequently lowering the peak-to-average power ratio of OFDM. Since random communication information on different subcarriers may affect the ambiguity function, thereby diminishing sensing performance, Watabe et al. [25] proposed using precoding to ensure that communication information between different channels exhibits good autocorrelation and cross-correlation, thus mitigating the impact of communication on sensing. In addition, Hassanien et al. [26] implemented an ISAC system integrating multiple-input multiple-output (MIMO) and OFDM, which utilized the primary lobe of the beam emitted by the MIMO radar for target sensing and the side lobes for communication. Moreover, the authors in [27] and [28] employed diverse weighted vectors for phase modulation. In the aforementioned two ISAC systems, a communication symbol is represented by multiple radar pulses, resulting in a relatively lower communication rate, and only enabling radar-ranging functionality. In [29], an analysis was conducted on the periodogram and multiple signal classification (MUSIC) radar signal processing algorithm, aimed at improving radar resolution accuracy. Simulation results demonstrated that MUSIC is more suitable for high signal-to-interference-plus-noise ratio (SINR) scenarios, whereas the periodogram method is better suited for low SINR scenarios.

3) Joint Waveform Design and Optimization: In communication-centric design and sensing-centric design, the performance of sensing and communication may not be optimal. Therefore, it is essential to explore joint design approaches that are independent of existing radar or communication waveforms, which not only allows for accurate sensing while communicating at high rates but also provides additional freedom and flexibility [30]. To this end, various joint waveform designs have been proposed for ISAC systems [31], [32], [33], [34], [35], [36], [37], [38]. Elbir and Mishra [31] focused on designing a sparse array with hybrid beamforming for ISAC systems, and proposed a modeling and learning-based approach to jointly address the design of sparse arrays and hybrid ISAC beamforming. In comparison to the single communication user model established in [31], Grossi et al. [32] proposed a more complex multiuser multisensing target model, and applied a cognition-based design method, exploring the energy-efficient optimization problem in MIMO radar-communication spectrum sharing scenarios. Through simulation verification, the proposed method maximizes efficiency while ensuring sensing performance, although the beamforming vector is not optimized. Liu et al. [33] studied high-efficiency waveform design for ISAC systems, aiming to enhance system efficiency while guaranteeing target estimation performance. Under power budget and Cramér-Rao lower bound (CRLB) constraints, the efficiency of the transmit waveform has been maximized. To address the highly nonconvex fractionalorder objective function involved in the proposed problem, the Dinkelbach algorithm is introduced in [33]. Liu et al. [34] introduced the successive convex approximation (SCA) algorithm to more efficiently calculate results based on previous work. Simulation results demonstrated a significant improvement in iteration speed and efficiency performance compared with the algorithm proposed in [33]. Chen et al. [35] suggested maximizing sensing accuracy by minimizing the mean square error between the ideal beamforming and the actual beamforming, and derived a closed-form solution for a single communication user scenario. Furthermore, the simulation proves that the shared antenna deployment mode in ISAC systems achieves higher sensing accuracy and overall performance than the separate antenna deployment mode. Liu et al. [36] categorized sensing targets into point targets and extended targets, and guaranteed SINR for each communication user while minimizing CRLB. In addition, Qiu et al. [37] demonstrated the equivalence between CRLB and mean square error in the case of extended targets. In [38], the radar SINR maximization problem was first constructed to jointly optimize the beamforming and transmit signal matrices under power and modulus constraints, using alternating optimization and gradient projection algorithms to solve the problem efficiently.

#### B. Motivations and Contributions

Although joint waveform design brings significant performance improvements to ISAC systems, even exponentially increasing spectral efficiency, achieving perfect channel state information (CSI) estimation remains challenging and impractical in actual communication systems due to diverse factors, such as noise, signal attenuation, and multipath propagation. Therefore, the previous works with perfect CSI [31], [32], [33], [34], [35], [36], [37], [38] may not be effective in actual systems, and they may introduce higher outages or message transmission errors. As a result, to limit the effects of channel uncertainty on the performance of ISAC systems in actual radio environments, it is necessary to consider the robust beamforming design.

Furthermore, the majority of the existing works [14], [15], [16], [17], [18], [19], [20], [21], [22], [23], [24], [25], [26], [27], [28], [29], [30], [31], [32], [33], [34], [35], [36], [37], [38] have concentrated on ISAC waveform design from different aspects. However, the system performance of sensing-centric [14], [15], [16], [17], [18], [19], [20], [21], [22] or communication-centric [23], [24], [25], [26], [27], [28], [29] designs is severely constrained by hardware platforms and signal processing algorithms. Achieving a favorable performance tradeoff between communication and sensing remains elusive. The main contributions are summarized as follows.

 We propose a joint beamforming design framework for downlink multiple-input single-output (MISO) ISAC systems considering imperfect CSI for point target sensing and multiuser communications. The sensing performance is guaranteed while maximizing the system throughput to improve the overall system performance.

- 2) Due to infinite constraints caused by the imperfect CSI, the complex maximization throughput problem is a nonconvex difficult one. First, we transform the original problem into a convex one by applying Schur complementary condition, SCA technique, S-procedure, semidefinite relaxation (SDR) technique, and variable substitution methods. Then, the transformed problem becomes amenable to a solution using the CVX toolbox. Finally, an SCA algorithm is proposed.
- 3) Simulation results demonstrate the convergence and robustness of our proposed SCA algorithm. Specifically, it exhibits better convergence and achieves a 7.3% reduction in outage probability compared with the nonrobust algorithm.

#### C. Organization and Notations

The rest of this article is organized as follows. Section II introduces the downlink MISO-ISAC system model and problem formulation. An iterative-based SCA algorithm is designed in Section III. Section IV gives the simulation results. Finally, Section V concludes this article.

Notations: Vectors and matrices are denoted by boldface lowercase letters and boldface uppercase letters, respectively.  $A^T$ ,  $A^H$ , rank(A), Tr(A), and  $\|A\|_F$  denote the transpose, Hermitian conjugate transpose, rank, trace, and Frobenius norm of matrix A, respectively.  $A \succeq 0$  indicates a positive semidefinite matrix.  $\mathcal{CN}(\mu, \delta^2)$  denotes the Gaussian distributions with mean  $\mu$  and variance  $\delta^2$ .  $\mathbb{E}\{\cdot\}$  denotes the expectation operation.  $\mathbb{C}^{M\times N}$  denotes an  $M\times N$  dimensional complex matrix.  $\|a\|$  and  $\|\cdot\|$  denote the Euclidean norm of a and the absolute operation, respectively.  $\text{Re}\{\cdot\}$  denotes the real part of a complex number. The abbreviations used in this article are given in the Nomenclature.

# II. SYSTEM MODEL AND PROBLEM FORMULATION

As shown in Fig. 1, we consider a multiuser downlink MISO-ISAC system. Specifically, a BS equipped with N antennas serves K single-antenna users while obtaining state information of a point target. Without loss of generality, assuming K < N [39]. Besides, we define L as the communication frame length,  $\forall k \in \mathcal{K} = \{1,2,\ldots,K\}$  and  $\forall l \in \mathcal{L} = \{1,2,\ldots,L\}$  denote the sets of communication users and discrete-time indexes.  $\mathbf{s}(l) = [s_1(l),s_2(l),\ldots,s_K(l)]^T \in \mathbb{C}^{K\times 1}$  denotes the vector of data sent to K users at discrete time l, satisfying  $\frac{1}{L} \sum_{l=1}^L \mathbf{s}(l)\mathbf{s}(l)^H = \mathbf{I}_{K\times K}$ .

Based on the above analysis, the transmitted signal at discrete time l of the BS can be formulated as  $\lceil 10 \rceil$ 

$$x(l) = Ws(l) \tag{1}$$

where  $\boldsymbol{W} = [\boldsymbol{w}_1, \boldsymbol{w}_2, \dots \boldsymbol{w}_K] \in \mathbb{C}^{N \times K}$  denotes the beamforming vector sent by the BS. Therefore, the covariance matrix of  $\boldsymbol{x}(l)$  can be expressed as

$$\mathbf{R}_{x} = \mathbb{E}\left\{\mathbf{x}(l)\mathbf{x}^{H}(l)\right\} = \mathbf{W}\mathbf{W}^{H}.$$
 (2)

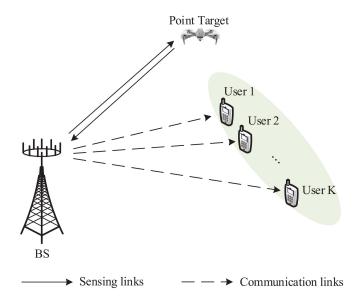


Fig. 1. MISO-ISAC system.

# A. Communication Models and Performance Metrics

The received signal by the communication user k can be expressed as

$$y_k(l) = \boldsymbol{h}_k^H \boldsymbol{w}_k s_k(l) + \sum_{j=1, j \neq k}^K \boldsymbol{h}_k^H \boldsymbol{w}_j s_j(l) + n_k(l)$$
 (3)

where  $h_k \in \mathbb{C}^{N \times 1}$  denotes the channel vector from the BS to the kth user, and  $n_k(l) \sim \mathcal{CN}(0, \sigma_k^2)$  denotes the additive Gaussian white noise at the user k with mean 0 and variance  $\sigma_k^2$ . Based on (3), the SINR of the user k can be formulated by

$$\gamma_k = \frac{\left|\boldsymbol{h}_k^H \boldsymbol{w}_k\right|^2}{\sum_{j=1, j \neq k}^K \left|\boldsymbol{h}_k^H \boldsymbol{w}_j\right|^2 + \sigma_k^2}.$$
 (4)

According to (4), the normalized throughput of the user k can be expressed as

$$R_k = \log_2\left(1 + \gamma_k\right). \tag{5}$$

# B. Sensing Models and Performance Metrics

Motivated by the authors in [41] and [42], it is reasonable for the communication signal sent by the dual-function BS to be used for sensing. Specifically, radar sensing does not require the transmission of valid information to accomplish its task. As long as the transmitted signal can interact with the target, the BS can process the target's echo signals to obtain target information and complete the sensing task. Therefore, by transmitting  $\boldsymbol{x}(l)$ , the echo signal at discrete time l can be expressed as

$$\mathbf{y}_s(l) = \alpha \mathbf{a}(\theta) \mathbf{a}^H(\theta) \mathbf{x}(l) + n_s(l)$$
 (6)

where  $\boldsymbol{a}(\theta) = [1, e^{j2\pi\Delta\sin(\theta)}, \dots, e^{j2\pi(N-1)\Delta\sin(\theta)}]^T \in \mathbb{C}^{N\times 1}$  denotes the steering vector for the transmitting antennas of the BS, and  $\Delta$  denotes the normalized spacing between neighboring antennas. Similarly,  $\boldsymbol{a}^H(\theta)$  denotes the steering vector of the receiving antennas.  $\alpha \in \mathbb{C}$  represents the complex amplitude proportional to the radar cross section of the target and the round-trip path loss.  $n_s(l) \sim \mathcal{CN}(0, \sigma_s^2)$  denotes the additive

Gaussian white noise with mean 0 and variance  $\sigma_s^2$  at the BS receiver.

CRLB can theoretically provide a minimum bound on the variance of the unbiased estimator, making it a valuable performance metric for target estimation. For the point target in an ISAC system, we obtain the position information of the target by estimating its relative angle  $\theta$  with respect to the BS. Defining  $A(\theta) = \mathbf{a}(\theta)\mathbf{a}^H(\theta)$  as the total steering vector, according to work [43], the CRLB of  $\theta$  can be expressed as follows (i.e., at the top of the page 5), where  $\dot{A}(\theta)$  denotes the derivative of  $A(\theta)$  (7) shown at the bottom of the next page.

# C. Robust Problem Formulation

Due to user mobility and the complexity of the electromagnetic environment, it becomes challenging to accurately obtain the CSI between the BS and users. Thus, assuming imperfect channel gains is a reasonable consideration, as motivated by models of bounded CSI errors [46], we have

$$\mathcal{R}_h = \left\{ \Delta \boldsymbol{h}_k \mid \boldsymbol{h}_k = \bar{\boldsymbol{h}}_k + \Delta \boldsymbol{h}_k : \|\Delta \boldsymbol{h}_k\|_2 \le \zeta_k \right\} \tag{8}$$

where  $\mathcal{R}_h$  denotes the set of tightly convex uncertainties,  $\bar{h}_k$  denotes the channel estimation vector,  $\Delta h_k$  denotes the corresponding channel estimation error, and  $\zeta_k \geq 0$  denotes the upper bound,<sup>2</sup> on the parameters of uncertainty.

Therefore, the robust beamforming problem for the ISAC system can be formulated as

$$\begin{aligned} \mathbf{P}_{1} : & \max_{\boldsymbol{w}_{k}} \ R_{\text{sum}}\left(\Delta\boldsymbol{h}_{k}\right) \\ \text{s.t.} & \text{C1} : \text{CRLB}(\theta) \leq \beta \\ & \text{C2} : \|\boldsymbol{W}\|_{F}^{2} \leq P^{\text{max}} \\ & \text{C3} : R_{k}\left(\Delta\boldsymbol{h}_{k}\right) \geq R_{k}^{\text{min}} \\ & \text{C4} : \Delta\boldsymbol{h}_{k} \in \mathcal{R}_{h} \end{aligned} \tag{9}$$

where  $R_{\text{sum}} = \sum_{k=1}^K R_k$  denotes the total throughput of the system,  $\beta$  denotes the threshold of CRLB,  $P^{\text{max}}$  denotes the maximum transmit power threshold of the BS, and  $R_k^{\text{min}}$  denotes the minimum transmission rate threshold of the communication user k, and constraint C1 is to ensure the sensing performance, C2 denotes the maximum transmit power constraint, C3 denotes the minimum transmission rate constraint of the communication user k, and C4 denotes the set of tightly convex uncertaintie.

Obviously, problem  $P_1$  is complicated and difficult to solve due to the following three aspects.

- 1) The total throughput in the objective function is nonconvex and NP-hard.
- 2) The nature of the Fisher information matrix causes constraint C1 to be nonconvex.
- Constraint C3 contains an infinite number of dimensional nonconvex constraints.

<sup>&</sup>lt;sup>1</sup>For the channel estimation phase, we can use the traditional channel estimation method to obtain the estimated channel values [44], [45].

<sup>&</sup>lt;sup>2</sup>In practice, the values of upper bounds depend on the coherence time of the associated channel, the specific channel estimation schemes, and the time between channel estimation and packet transmission [47].

Therefore, we propose the SCA algorithm to solve problem  $\mathbf{P}_1$ .

# III. ROBUST BEAMFORMING PROBLEM OPTIMIZATION

# A. Proposed SCA Algorithm

It is observed that the objective function and constraint C3 in problem  $\mathbf{P}_1$  involve channel errors. In order to deal with it, an auxiliary variable t is introduced, and based on the variable relaxation method, problem  $\mathbf{P}_1$  can be reformulated as

$$\mathbf{P}_{2}: \max_{\boldsymbol{w}_{k},t} t$$
s.t.  $C5: R_{\text{sum}}(\Delta \boldsymbol{h}_{k}) \geq t$ 

$$C1 \sim C4. \tag{10}$$

Problem  $P_2$  remains a challenging nonconvex optimization problem, and to deal with the channel uncertainty as well as the nonconvexity in constraints C3 and C5, the following variational relaxation is considered:

$$\frac{\phi_k}{\gamma_k} \ge 2^{r_k} - 1 \tag{11}$$

$$\phi_k \le \left| \boldsymbol{h}_k^H \boldsymbol{w}_k \right|^2 \tag{12}$$

$$\chi_k \ge \sum_{j=1, j \ne k}^K \left| \boldsymbol{h}_k^H \boldsymbol{w}_j \right|^2 + \sigma_k^2 \tag{13}$$

where  $\phi_k$ ,  $\chi_k$ , and  $r_k$  are the introduced slack variables. However, (11) is still nonconvex, and in order to transform it into a convex one, we apply Taylor series expansion method, then (11) can be approximately linearized as follows:

$$\begin{cases} \phi_k \ge e^{x_k^1}, x_k^1 - x_k^2 \ge x_k^3 \\ \chi_k \le e^{\bar{x}_k^2} \left( x_k^2 - \bar{x}_k^2 + 1 \right) \\ 2^{r_k} - 1 \le e^{\bar{x}_k^3} \left( x_k^3 - \bar{x}_k^3 + 1 \right) \end{cases}$$
(14)

where  $x_k^1$ ,  $x_k^2$ , and  $x_k^3$  are slack variables, respectively, and  $\bar{x}_k^2$  and  $\bar{x}_k^3$  are the values of the last iteration of  $x_k^2$  and  $x_k^3$ , respectively. Defining  $\boldsymbol{W}_k = \boldsymbol{w}_k \boldsymbol{w}_k^H$ , and satisfying  $\boldsymbol{W}_k \succeq \boldsymbol{0}$ , Rank $(\boldsymbol{W}_k) = 1$ . According to (8), (12) can be rewritten as

$$\phi_k \le \Delta \boldsymbol{h}_k^H \boldsymbol{B}_1 \Delta \boldsymbol{h}_k + 2 \operatorname{Re} \left\{ \bar{\boldsymbol{h}}_k^H \boldsymbol{B}_1 \Delta \boldsymbol{h}_k \right\}$$
$$+ \bar{\boldsymbol{h}}_k^H \boldsymbol{B}_1 \bar{\boldsymbol{h}}_k, \ \|\Delta \boldsymbol{h}_k\|_2^2 \le \zeta_k^2.$$
(15)

Similarly, (13) can be rewritten as

$$\chi_k \ge \Delta \boldsymbol{h}_k^H \boldsymbol{B}_2 \Delta \boldsymbol{h}_k + 2 \operatorname{Re} \left\{ \bar{\boldsymbol{h}}_k^H \boldsymbol{B}_2 \Delta \boldsymbol{h}_k \right\}$$
$$+ \bar{\boldsymbol{h}}_k^H \boldsymbol{B}_2 \bar{\boldsymbol{h}}_k + \sigma_k^2, \|\Delta \boldsymbol{h}_k\|_2^2 \le \zeta_k^2$$
(16)

where  $B_1 = W_k$  and  $B_2 = \sum_{j=1, j \neq k}^K W_j$ . To address the channel uncertainties arising from parameter perturbations in (15) and (16), we introduce Lemma 1 to deal with it.

Lemma 1 (S-procedure [48]): Define the quadratic functions  $f_i(\boldsymbol{x}) = \boldsymbol{x}^H \boldsymbol{A}_i \boldsymbol{x} + 2 \mathrm{Re} \{\boldsymbol{b}_i^H \boldsymbol{x}\} + c_i, i = \{1,2\}, \text{ where } \boldsymbol{A}_i \in \mathbb{C}^{N \times N}, \ \boldsymbol{b}_i \in \mathbb{C}^{N \times 1}, \ \boldsymbol{x} \in \mathbb{C}^{N \times 1}, \text{ and } c_i \in \mathbb{R}.$  The condition  $f_1(\boldsymbol{x}) \leq 0 \Rightarrow f_2(\boldsymbol{x}) \leq 0$  holds if and only if there exists  $\lambda \geq 0$  such that

$$\lambda \begin{bmatrix} \boldsymbol{A}_1 & \boldsymbol{b}_1 \\ \boldsymbol{b}_1^H & c_1 \end{bmatrix} - \begin{bmatrix} \boldsymbol{A}_2 & \boldsymbol{b}_2 \\ \boldsymbol{b}_2^H & c_2 \end{bmatrix} \succeq \boldsymbol{0}. \tag{17}$$

Defining an auxiliary variable  $\lambda_1 \geq 0$ , according to Lemma 1, the semiinfinite dimensional constraint (15) can be transformed into the following linear matrix inequality:

$$\begin{bmatrix} \boldsymbol{B}_1 + \lambda_1 \boldsymbol{I}_{N \times N} & \boldsymbol{B}_1 \bar{\boldsymbol{h}}_k \\ \bar{\boldsymbol{h}}_k^H \boldsymbol{B}_1 & \bar{\boldsymbol{h}}_k^H \boldsymbol{B}_1 \bar{\boldsymbol{h}}_k - \boldsymbol{\phi}_k - \lambda_1 \zeta_k^2 \end{bmatrix} \succeq \boldsymbol{0}.$$
 (18)

*Proof:* See Appendix. Similarly, defining  $\lambda_2 \geq 0$  as an auxiliary variable, (16) can be transformed into the following form:

$$\begin{bmatrix} -\boldsymbol{B}_2 + \lambda_2 \boldsymbol{I}_{N \times N} & -\boldsymbol{B}_2 \bar{\boldsymbol{h}}_k \\ -\bar{\boldsymbol{h}}_k^H \boldsymbol{B}_2 & -\bar{\boldsymbol{h}}_k^H \boldsymbol{B}_2 \bar{\boldsymbol{h}}_k - \sigma_k^2 + \chi_k - \lambda_2 \zeta_k^2 \end{bmatrix} \succeq \boldsymbol{0}.$$
(19)

Furthermore, to transform the nonconvex constraint C1 into a convex one, we employ Schur complement condition to convert it into a manageable form [49]. First, it is expressed equivalently as

$$\operatorname{Tr}\left(\dot{\boldsymbol{A}}^{H}(\theta)\dot{\boldsymbol{A}}(\theta)\boldsymbol{R}_{x}\right)-D\geq\frac{\left|\operatorname{Tr}\left(\dot{\boldsymbol{A}}^{H}(\theta)\boldsymbol{A}(\theta)\boldsymbol{R}_{x}\right)\right|^{2}}{\operatorname{Tr}\left(\boldsymbol{A}^{H}(\theta)\boldsymbol{A}(\theta),\boldsymbol{R}_{x}\right)}$$
(20)

where  $D = \sigma_s^2/2\beta |\alpha|^2 L$ . Then, we use the Schur complement condition, (20) can be rewritten as

(14) 
$$\begin{bmatrix} \operatorname{Tr} \left( \dot{\boldsymbol{A}}^{H}(\theta) \dot{\boldsymbol{A}}(\theta) \boldsymbol{R}_{x} \right) - D & \operatorname{Tr} \left( \dot{\boldsymbol{A}}^{H}(\theta) \boldsymbol{A}(\theta) \boldsymbol{R}_{x} \right) \\ \operatorname{Tr} \left( \boldsymbol{A}^{H}(\theta) \dot{\boldsymbol{A}}(\theta) \boldsymbol{R}_{x} \right) & \operatorname{Tr} \left( \boldsymbol{A}^{H}(\theta) \boldsymbol{A}(\theta) \boldsymbol{R}_{x} \right) \end{bmatrix} \succeq \boldsymbol{0}.$$
(21)

Based on the above analysis, the original nonconvex optimization problem  $\mathbf{P}_1$  can be reformulated as follows:

$$\begin{aligned} \mathbf{P}_{3}: & \max_{\boldsymbol{W}_{k},t,\Sigma} t \\ \text{s.t.} & \hat{\mathbf{C}}1: (21) \\ & \hat{\mathbf{C}}2: \sum_{k=1}^{K} \operatorname{Tr}\left(\boldsymbol{W}_{k}\right) \leq P^{\max} \\ & \bar{\mathbf{C}}3: r_{k} \geq R_{k}^{\min} \\ & \mathbf{C}5: (14), (18), (19) \\ & \mathbf{C}6: \boldsymbol{W}_{k} \succeq \mathbf{0} \\ & \mathbf{C}7: \operatorname{Rank}\left(\boldsymbol{W}_{k}\right) = 1 \\ & \mathbf{C}8: \lambda_{1} > 0, \lambda_{2} > 0 \end{aligned} \tag{22}$$

$$CRLB(\theta) = \frac{\sigma_s^2}{2 \mid \alpha \mid^2 L} \times \frac{Tr(\boldsymbol{A}^H(\theta)\boldsymbol{A}(\theta)\boldsymbol{R}_x)}{Tr(\dot{\boldsymbol{A}}^H(\theta)\dot{\boldsymbol{A}}(\theta)\boldsymbol{R}_x)Tr(\boldsymbol{A}^H(\theta)\boldsymbol{A}(\theta)\boldsymbol{R}_x) - \mid Tr(\dot{\boldsymbol{A}}^H(\theta)\boldsymbol{A}(\theta)\boldsymbol{R}_x) \mid^2}.$$
 (7)

# Algorithm 1: Proposed SCA Algorithm.

- 1: Initialize:  $N, K, L, \bar{h}_k, \zeta_k, \beta, P^{\max}, R_k^{\min}, \bar{x}_k^{(0),2}, \bar{x}_k^{(0),3};$
- 2: Set the initial iteration value  $x=1, \eta>0$  as the convergence accuracy, and  $X_{\rm max}$  as the maximum iteration number:
- iteration number; 3: while  $|R_{\text{sum}}^{(x)} R_{\text{sum}}^{(x-1)}| \ge \eta \text{ or } x \le X_{\text{max}}$  do
- 4: Solve  $\mathbf{P}_3$  with given  $\bar{x}_k^{(x-1),2}$ ,  $\bar{x}_k^{(x-1),3}$ , and obtain the optimal solution denoted by  $\bar{x}_k^{(x),2}$ ,  $\bar{x}_k^{(x),3}$ ,  $\{\mathbf{W}_k^{(x)}\}_{k=1}^K$ ;
- 5: until converges;
- 6: **if** Rank( $(\boldsymbol{W}_k^{(x)}) = 1$  **then**
- 7:  $\boldsymbol{w}_{k}^{(x)}$  is obtained via the eigenvalue decomposition method;
- 8: else
- 9:  $w_k^{(x)}$  is obtained by using the singular value decomposition method [50];
- 10: **end if**
- 11: x = x + 1;
- 12: end while
- 13: **out put**:  $w_{h}^{*}$ .

where  $\Sigma = \{\phi_k, \chi_k, r_k, x_k^1, x_k^2, x_k^3, \lambda_1, \lambda_2\}$ . Problem  $\mathbf{P}_3$  is still nonconvex due to  $\mathrm{Rank}(\mathbf{W}_k) = 1$  in C6, we relax it based on the SDR method. Then, problem  $\mathbf{P}_3$  becomes a complex convex one that can be solved directly using the CVX toolbox. Since the solution obtained in problem  $\mathbf{P}_3$  by removing the constraints using the SDR method is only an upper bound on problem  $\mathbf{P}_1$ , a Gaussian randomization method is needed to approximate the near-optimal solution. We assume that the solution of the problem  $\mathbf{P}_3$  is  $\mathbf{W}_k^*$  with  $\mathrm{Rank}(\mathbf{W}_k^*) = 1$ , then  $\mathbf{w}_k^*$  can be obtained by eigenvalue decomposition; otherwise,  $\mathbf{w}_k^*$  can be obtained by singular value decomposition [50]. Finally, the proposed iteration-based SCA algorithm is summarized in Algorithm 1.

# B. Convergence Analysis

To better analysis the convergence of Algorithm 1, we define  $\boldsymbol{W}_k^{(x)}$  as the xth iteration solution of  $\boldsymbol{P}_3$ , x as the iteration number, and  $R_{\text{sum}}(\boldsymbol{W}_k) = \sum_{k=1}^K R_k$  as the total throughput of the system. According to step 3 of Algorithm 1, the following condition is satisfied:

$$R_{\text{sum}}(\boldsymbol{W}_{k}^{(x-1)}) \le R_{\text{sum}}(\boldsymbol{W}_{k}^{(x)})$$
 (23)

it is observed that the final value of  $R_{\mathrm{sum}}(\boldsymbol{W}_k)$  either equals or surpasses the value obtained in the last iteration. Moreover, the cumulative throughput continues to increase within a defined range, thus confirming the convergence of Algorithm 1.

#### C. Complexity Analysis

Based on the method in [51], the complexity of Algorithm 1 can be denoted as  $O = \mathcal{O}(x_1(x_2 + x_3))$  with the following expression:

$$x_1 = \sqrt{K(8+3N)} (24)$$

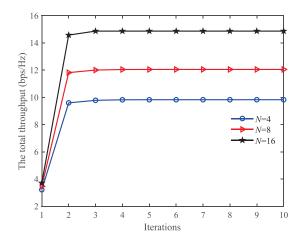


Fig. 2. Convergence of the proposed algorithm.

$$x_2 = n(6K + KN^3 + 2K(N+1)^3)$$
 (25)

$$x_3 = n^2(6K + KN^2 + 2K(N+1)^2)$$
 (26)

where  $n = \mathcal{O}(KN^2)$  denotes the total number of elements to be optimized,  $x_1$  denotes the number of iterations, and  $x_2$  and  $x_3$  denote the complexity of each iteration.

# IV. SIMULATION RESULTS

In this section, the effectiveness of the proposed algorithm is evaluated by numeral simulations. The system channel fading model is assumed to be large-scale fading, and each individual channel fading model is independent, following the distribution:  $Q=\psi d_i^{-\alpha}$ , where  $\psi=-30$  dB represents the path loss,  $d_i$  represents the distance between any two devices, and  $\alpha=3$  denotes the path loss exponent [52]. Furthermore, it is assumed that the point target is at its 0° position with respect to the dual-function BS. Without loss of generality, other parameters are defined as  $\sigma_k=\sigma_s=10^{-7}$  W,  $P^{\max}=5$  W,  $R_k^{\min}=0.1$  bps/Hz [53], L=30, K=2,  $\beta=0.025$  [54],  $X_{\max}=10^5$ , and  $\eta=10^{-5}$ . Define the normalized channel estimation errors as  $\psi_h=\frac{\zeta_k}{\|\overline{h}_{b,k}\|^2}=0.1$ .

Fig. 2 depicts the convergence of the proposed algorithm under different numbers of antennas N at the BS. Clearly, the proposed algorithm tends to consistently converge after approximately five iterations, demonstrating strong convergence. In addition, the total system throughput increases with the growing N. This can be attributed to the larger N, which provides more degrees of freedom, enhancing signal coverage and transmission rates, thereby improving beamforming gain and overall system throughput.

Fig. 3 depicts the total system throughput versus the minimum rate threshold  $R_k^{\min}$  under various channel error upper bounds  $\zeta_k$ . It is clear that for the same  $\zeta_k$ , the total system throughput increases with  $R_k^{\min}$  when  $R_k^{\min}$  is low. This is because the increased  $R_k^{\min}$  compels the system to allocate more power to each user to meet the higher  $R_k^{\min}$  requirements, thereby increasing the throughput per user. Furthermore, at the same  $R_k^{\min}$ , the total system throughput decreases with an increase

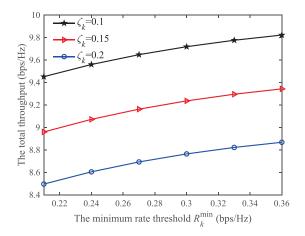


Fig. 3. Total throughput versus  $R_k^{\min}$  under different  $\zeta_k$ .

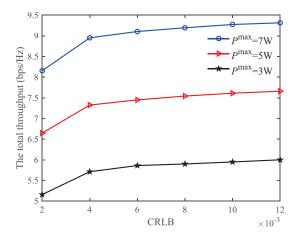


Fig. 4. Total throughput versus the CRLB under different  $P^{\max}$ .

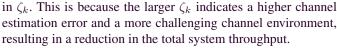


Fig. 4 depicts the total system throughput versus the thresholds of CRLB under various maximum transmit powers  $P^{\max}$ . Obviously, the total system throughput exhibits an increasing trend with rising CRLB thresholds. This can be attributed to the inherent performance tradeoff between communication and sensing, given a specific  $P^{\max}$ . A larger CRLB threshold implies that the system demands less sensing accuracy. Consequently, less power is directed toward the point targets, allowing more power to be allocated to communication data transmission. This leads to an enhancement in communication performance and an overall increase in total throughput. Furthermore, while keeping the CRLB threshold constant, the total system throughput increases with higher  $P^{\max}$ . This is because the increased value of  $P^{\max}$  expands the feasible domain of transmitted power, subsequently boosting the data rate.

Fig. 5 depicts the total system throughput versus the maximum transmit power  $P^{\max}$  under two different algorithms. Evidently, the total system throughput of both algorithms increases with the increasing  $P^{\max}$ . This is because boosting  $P^{\max}$  leads to

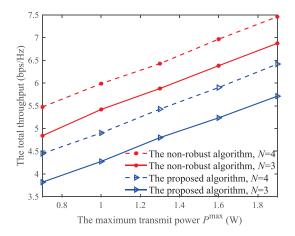


Fig. 5. Total throughput versus  $P^{\max}$  under different algorithms.

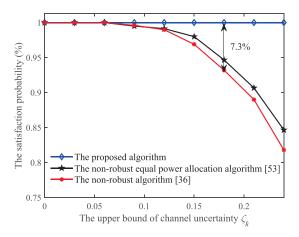


Fig. 6. Satisfaction probability versus  $\zeta_k$  under different algorithms.

stronger signals transmitted by the BS, making them less susceptible to interference or attenuation during transmission. Consequently, the receiving end can more easily decode the received signal, thereby enhancing the overall system throughput. The robust algorithm, as it ensures that the system operates normally in uncertain and noisy environments, typically incurs a cost of reducing the overall throughput to achieve higher stability and reliability. Furthermore, under the same  $P^{\max}$ , when  $\zeta_k$  is small and N is large, the total system throughput is also larger. This is attributed to the improvement in the channel environment and the increased beamforming gain, resulting in an overall increase in system throughput.

Fig. 6 depicts the probability of satisfaction (i.e., 1-outage probability) for various channel error upper bounds  $\zeta_k$  under there distinct algorithms. Clearly, the proposed algorithm demonstrates a remarkable 100% probability of satisfaction, when  $\zeta_k=0.18$ , compared to the nonrobust algorithm, its satisfaction probability is improved by 7.3%. This is because designing with bounded CSI errors ensures that even in the worst-case scenario, the system can still operate smoothly. In contrast, the satisfaction probabilities of nonrobust algorithm and nonrobust equal power allocation algorithms decrease as  $\zeta_k$  increases. This is because CSI errors introduce discrepancies between system

design and actual operation, leading to improper resource allocation and insufficient system robustness, thereby increasing the outage probability. In addition, the satisfaction probability of the nonrobust equal power allocation algorithm is higher than that of the nonrobust algorithm because the nonrobust equal power allocation algorithm is less sensitive to CSI errors, resulting in a higher satisfaction probability.

#### V. CONCLUSION

In this article, we investigated a robust beamforming problem for a MISO-ISAC system with channel uncertainties. A nonconvex robust optimization problem for maximizing the total throughput was formulated by considering the minimum transmission rate constraint of each user, the sensing threshold constraint of the CRLB, and the maximum transmit power constraint. The original problem was transformed into the convex one by applying Schur complementary condition, SCA, S-procedure, SDR, and the variable substitution method. Simulation results demonstrated that the proposed algorithm exhibits better convergence and has a lower outage probability than the nonrobust algorithm.

# APPENDIX PROOF OF LEMMA 1

*Proof:* For Lemma 1 to hold for  $f_1(x) \le 0 \Rightarrow f_2(x) \le 0$  is equivalent to holding for  $f_1(x) \le 0$  if and only if there exists  $\lambda \ge 0$  such that  $\lambda f_1(x) - f_2(x) \ge 0$  holds. This can be written in the following quadratic matrix form:

$$\lambda \begin{bmatrix} \boldsymbol{x}^{H} & \boldsymbol{I} \end{bmatrix} \begin{bmatrix} \boldsymbol{A}_{1} & \boldsymbol{b}_{1} \\ \boldsymbol{b}_{1}^{H} & c_{1} \end{bmatrix} \begin{bmatrix} \boldsymbol{x} \\ \boldsymbol{I} \end{bmatrix} - \begin{bmatrix} \boldsymbol{x}^{H} & \boldsymbol{I} \end{bmatrix} \begin{bmatrix} \boldsymbol{A}_{2} & \boldsymbol{b}_{2} \\ \boldsymbol{b}_{2}^{H} & c_{2} \end{bmatrix} \begin{bmatrix} \boldsymbol{x} \\ \boldsymbol{I} \end{bmatrix} \ge \boldsymbol{0}$$

$$\Leftrightarrow \begin{bmatrix} \boldsymbol{x}^{H} & \boldsymbol{I} \end{bmatrix} \left\{ \lambda \begin{bmatrix} \boldsymbol{A}_{1} & \boldsymbol{b}_{1} \\ \boldsymbol{b}_{1}^{H} & c_{1} \end{bmatrix} - \begin{bmatrix} \boldsymbol{A}_{2} & \boldsymbol{b}_{2} \\ \boldsymbol{b}_{2}^{H} & c_{2} \end{bmatrix} \right\} \begin{bmatrix} \boldsymbol{x} \\ \boldsymbol{I} \end{bmatrix} \ge \boldsymbol{0} \qquad (27)$$

since the quadratic matrix (27) is nonnegative, we have

$$\lambda \begin{bmatrix} \boldsymbol{A}_1 & \boldsymbol{b}_1 \\ \boldsymbol{b}_1^H & c_1 \end{bmatrix} - \begin{bmatrix} \boldsymbol{A}_2 & \boldsymbol{b}_2 \\ \boldsymbol{b}_2^H & c_2 \end{bmatrix} \succeq \boldsymbol{0}. \tag{28}$$

Then, we give a proof for (18) [(19) will not be repeated]. Equations (8) and (15) can be written in quadratic form as follows:

$$\begin{cases} f_1(\boldsymbol{\Delta}\boldsymbol{h}_k) = \Delta\boldsymbol{h}_k^H \Delta\boldsymbol{h}_k - \zeta_k^2 \le 0 \\ f_2(\boldsymbol{\Delta}\boldsymbol{h}_k) = \phi_k - \Delta\boldsymbol{h}_k^H \boldsymbol{B}_1 \Delta\boldsymbol{h}_k - 2\text{Re}\{\bar{\boldsymbol{h}}_k^H \boldsymbol{B}_1 \Delta\boldsymbol{h}_k\} \\ -\bar{\boldsymbol{h}}_k^H \boldsymbol{B}_1 \bar{\boldsymbol{h}}_k \le 0 \end{cases}$$

where  $\boldsymbol{x} = \Delta \boldsymbol{h}_k$ ,  $\boldsymbol{A}_1 = \boldsymbol{I}_{N \times N}$ ,  $\boldsymbol{b}_1 = 0$ ,  $c_1 = -\zeta_k^2$ ,  $\boldsymbol{A}_2 = -\boldsymbol{B}_1$ ,  $\boldsymbol{b}_2 = -\boldsymbol{B}_1\bar{\boldsymbol{h}}_k$ , and  $c_2 = -\bar{\boldsymbol{h}}_k^H\boldsymbol{B}_1\bar{\boldsymbol{h}}_k + \phi_k$ . According to Lemma 1, for  $f_1(x) \leq 0 \Rightarrow f_2(x) \leq 0$  to hold, we have

$$\begin{bmatrix} B_1 + \lambda_1 I_{N \times N} & B_1 \bar{\boldsymbol{h}}_k \\ \bar{\boldsymbol{h}}_k^H B_1 & \bar{\boldsymbol{h}}_k^H B_1 \bar{\boldsymbol{h}}_k - \phi_k - \lambda_1 \zeta_k^2 \end{bmatrix} \succeq \boldsymbol{0}. \quad (30)$$

The proof is complete.

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