

Direct-Splitting-Based CN-FDTD for Modeling 2D Material Nanostructure Problems

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ABSTRACT Incorporating a truncation of the complex-frequency-shifted perfectly matched layer (CFS-PML), the direct-splitting-based Crank-Nicolson finite-difference time-domain (CNDS-FDTD) is developed and applied to the infrared two-dimensional layered material (2DLM) black phosphorous (BP) metasurface implementations on the all-dielectric nanostructure. To improve extremely low efficiencies in solving infrared terahertz (THz) problems with the few-atomic-layer thickness of 2DLMs, the CFS-CNDS-FDTD is proposed in demand due to the fact that it possesses capabilities of implicit FDTD method and unsplit-field CFS-PML truncation, respectively, in completely conquering the Courant-Friedrich-Levy condition (CFL) limit and holding good performance. The temporal incremental in the CFS-CNDS-FDTD can reach 1000 times larger than that in the regular FDTD for infrared nanoscale problems centered at the 2.5 THz and then keep accurate. Three-dimensional (3D) numerical cases have been carried out to corroborate the proposed method. The CFS-CNDS-FDTD can not only achieve high accuracies and then saves several dozen times of CPU time as compared to the regular FDTD, but also pave the way for designing all-dielectric nanostructures with other 2DLM metasurfaces.

INDEX TERMS Black phosphorous (BP), Crank-Nicolson finite-difference time-domain (CN-FDTD), complex-frequency-shifted perfectly matched layer (CFS-PML), direct-splitting (DS), metasurface, two-dimensional layered material (2DLM).

I. INTRODUCTION

THE METALLIC or dielectric metasurfaces [1]–[7] are composed of arrays of subwavelength-spaced optical scatters distributed atop the interface whose prime function is to allow for locally altering the phase of incident light, which have very recently drawn considerable attention due to the fact that a unique method can be provided to guide electromagnetic waves at will, and then possess advanced optical technology adopted for implementing versatile functionalities in a planar structure [8]–[14]. Therefore, the significant loss and fabrication difficulty of volumetric metamaterials can be effectively avoided [2], [15]–[16].

However, as far as we know, most previously elaborated metasurface designs encounter low coupling efficiency and are based on metallic resonators, which leads to ohmic loss.

To overcome drawbacks of plasmonic metasurfaces, one can replace metals with all-dielectric resonators [17], [18]. Dielectric metasurfaces consist of interfaces patterned with a distribution of high-index dielectric light scattering particles of size comparable to the wavelength of light [3]. Their scattering properties were first studied by Faraday [19] and the effect is also known as Faraday-Tyndall scattering.

Very recently, an efficient design of all-dielectric photonic structure has been implemented for modeling graphene-based

optoelectronics devices, which provide a promising method applied to enhancing light-matter interaction in sub-nanometer two-dimensional layered materials (2DLMs) [20]. Furthermore, black phosphorus (BP), as another emerging member of the 2DLMs, has exhibited high carrier mobility, strong light-matter interaction in the infrared spectrum, and high degree of band anisotropy [21]–[25]. Besides, fully different from graphene with in-plane isotropy, the BP shows in-plane anisotropic properties. Therefore, the monolayer 2D BP with/without subwavelength patterning will be added into 3D all-dielectric nanostructures in this study.

However, the monolayer BP is few-atomic-layer thickness in size, and hence relatively thin as compared with the regular 3D geometrical nanostructures, leading to requirements of massive CPU time and computer memory for regular finite-difference time-domain (FDTD) simulations [26]–[34] because of resulting from the Courant-Friedrich-Levy condition (CFL) limit. The challenge lies in a quite large number of time steps required by the regular FDTD method for infrared sub-nanometer problems where high spatial and temporal sampling densities are required. For example, at the central frequency of 1 terahertz (THz) in the all-dielectric nanostructure application, spatial and temporal sampling densities in air can be approximately 0.1 million points per wavelength (PPW) and 0.3 million points per period (PPP), separately. To circumvent this problem, implicit FDTD methods [35]–[38] can be well used, which encounter no limit on time intervals arising from stability considerations.

The Crank-Nicolson FDTD (CN-FDTD) methods, as one of the most popular implicit formulations, are characterized with pretty high numerical accuracies and exhibit extremely small numerical anisotropy, but their full implicit discretization leads to a huge sparse matrix that needs to be inverted [39].

Very recently, to avoid solving very huge sparse matrix so that the CPU time and memory can be dramatically decreased, the cycle-sweep-uniform CN-FDTD (CNCSU-FDTD) is used to solve 3D low frequency subsurface sensing problems [40], which can be also used for modeling 3D infrared all-dielectric nanostructures with a 2D BP with the design of metasurface. However, it should be noted that the ADE-based CFS-CNCSU-FDTD method is indicated in [40], [41] to be only conditionally stable in certain situations. Recently, however, the BT-based CNDS-FDTD method is proposed and applied to solve FDTD problems in the microwave range, and then further prove that the CNCSU-FDTD exists the instability in certain cases [42].

In this systematic study, the efficient direct-splitting-based CN-FDTD (CNDS-FDTD) method with the CFS-PML scheme is proposed based on the auxiliary differential equation (ADE) method to model 3D all-dielectric photonic nanostructures with monolayer BP metasurfaces in the infrared Terahertz range. The CFS-CNDS-FDTD not only possess higher efficiency than the alternating-direction-implicit FDTD (ADI-FDTD) method [43]–[46] due to owning fewer loops at each time step, but is suitable for

parallel computation [47]–[49] which can be used to further reduce CPU time [39].

In view of the CFL limit of regular FDTD method needing higher PPW and PPP sampling, the CFS-CNDS-FDTD method is adopted to overcome extremely low computational efficiency by using large CFL number (CFLN). For example, the CFLN = 1000 can be set, and hence several dozen times of CPU time as compared with the regular FDTD method can be saved. Besides, to further corroborate the performance of CFS-CNDS-FDTD, we design the 3D all-dielectric nanostructures adding the single layer BP with/without subwavelength patterning for validation. As a result, 3D numerical simulations have been carried out to prove that the proposed CFS-CNDS-FDTD not only saves a large amount of CPU time and then reaches good accuracies as compared with the conventional FDTD simulation, but paves the way for fabricating the all-dielectric nanostructures with BP and other 2DLM metasurfaces.

The main contributions of this work include following: (1) The unconditionally-stable CNDS-based FDTD formulations is developed, different from the CNCSU-based FDTD which is conditionally stable in certain cases; (2) The 3D all-dielectric nanostructures with BP metasurfaces in the infrared range are implemented using the CFS-CNDS-FDTD.

II. FORMULATION

In a 3D CFS-PML region, the frequency domain modified Maxwell's curl equations can be written as

$$j\omega\varepsilon_0\varepsilon_r(\omega)E(\omega) + \sigma E(\omega) = \nabla_s \times H(\omega) \quad (1)$$

$$j\omega\mu_0H(\omega) = -\nabla_s \times E(\omega) \quad (2)$$

where $\varepsilon_r(\omega)$ and $\mu_r(\omega)$ are the relative permittivity and permeability of an inhomogeneous medium, respectively, and σ is the electrical conductivity. For the CFS-PML region, the operator ∇_s is expressed as

$$\nabla_s = \sum_{\eta=x,y,z} \hat{\eta} S_\eta^{-1} \partial_\eta \quad (3)$$

where ∂_x , ∂_y and ∂_z are partial derivatives with respect to x , y and z , and S_η is complex stretching coordinate metric with the CFS scheme, defined as

$$S_\eta = \kappa_\eta + \sigma_\eta / (\alpha_\eta + j\omega), \quad (\eta = x, y, z) \quad (4)$$

where κ_η is a scaling factor, and imaginary part σ_η represents a loss in PML regions, and α_η is assumed to be positive real.

As an example, we now are considering discretization of the x component of E field in all corners and edges of PML regions that is parallel to the x direction

$$j\omega\varepsilon_0\varepsilon_r E_x + \sigma E_x = S_y^{-1} \frac{\partial H_z}{\partial y} - S_z^{-1} \frac{\partial H_y}{\partial z} \quad (5)$$

$$-j\omega\mu_0 H_y = S_z^{-1} \frac{\partial E_x}{\partial z} - S_x^{-1} \frac{\partial E_z}{\partial x} \quad (6)$$

$$-j\omega\mu_0 H_z = S_x^{-1} \frac{\partial E_y}{\partial x} - S_y^{-1} \frac{\partial E_x}{\partial y} \quad (7)$$

Rewrite S_{η}^{-1} , ($\eta = x, y, z$) as

$$S_{\eta}^{-1} = (\kappa_{\eta})^{-1} - \frac{\sigma_{\eta}/(\kappa_{\eta}^2 \varepsilon_0)}{j\omega + (\alpha_{\eta} + \sigma_{\eta}/\kappa_{\eta})/\varepsilon_0} \quad (8)$$

Incorporating (8) into (5-7), and we have

$$j\omega \varepsilon_0 \varepsilon_r E_x + \sigma E_x = (\kappa_y)^{-1} \frac{\partial H_z}{\partial y} - (\kappa_z)^{-1} \frac{\partial H_y}{\partial z} - \frac{\sigma_y/(\kappa_y^2 \varepsilon_0)}{j\omega + (\alpha_y + \sigma_y/\kappa_y)/\varepsilon_0} \frac{\partial H_z}{\partial y} + \frac{\sigma_z/(\kappa_z^2 \varepsilon_0)}{j\omega + (\alpha_z + \sigma_z/\kappa_z)/\varepsilon_0} \frac{\partial H_y}{\partial z} \quad (9)$$

$$j\omega \mu_0 H_y = (\kappa_x)^{-1} \frac{\partial E_z}{\partial x} - (\kappa_z)^{-1} \frac{\partial E_x}{\partial z} - \frac{\sigma_x/(\kappa_x^2 \varepsilon_0)}{j\omega + (\alpha_x + \sigma_x/\kappa_x)/\varepsilon_0} \frac{\partial E_z}{\partial x} + \frac{\sigma_z/(\kappa_z^2 \varepsilon_0)}{j\omega + (\alpha_z + \sigma_z/\kappa_z)/\varepsilon_0} \frac{\partial E_x}{\partial z} \quad (10)$$

$$j\omega \mu_0 H_z = (\kappa_y)^{-1} \frac{\partial E_x}{\partial y} - (\kappa_x)^{-1} \frac{\partial E_y}{\partial x} - \frac{\sigma_y/(\kappa_y^2 \varepsilon_0)}{j\omega + (\alpha_y + \sigma_y/\kappa_y)/\varepsilon_0} \frac{\partial E_x}{\partial y} + \frac{\sigma_x/(\kappa_x^2 \varepsilon_0)}{j\omega + (\alpha_x + \sigma_x/\kappa_x)/\varepsilon_0} \frac{\partial E_y}{\partial x} \quad (11)$$

To simplify (9-11), $f_{xy}, f_{xz}, g_{yx}, g_{yz}, g_{zx}, g_{zy}$ are introduced as auxiliary variables, shown below

$$f_{xy} = \frac{\sigma_y/(\kappa_y^2 \varepsilon_0)}{j\omega + (\alpha_y + \sigma_y/\kappa_y)/\varepsilon_0} \frac{\partial H_z}{\partial y} \quad (12)$$

$$f_{xz} = \frac{\sigma_z/(\kappa_z^2 \varepsilon_0)}{j\omega + (\alpha_z + \sigma_z/\kappa_z)/\varepsilon_0} \frac{\partial H_y}{\partial z} \quad (13)$$

$$g_{yx} = \frac{\sigma_x/(\kappa_x^2 \varepsilon_0)}{j\omega + (\alpha_x + \sigma_x/\kappa_x)/\varepsilon_0} \frac{\partial E_z}{\partial x} \quad (14)$$

$$g_{yz} = \frac{\sigma_z/(\kappa_z^2 \varepsilon_0)}{j\omega + (\alpha_z + \sigma_z/\kappa_z)/\varepsilon_0} \frac{\partial E_x}{\partial z} \quad (15)$$

$$g_{zy} = \frac{\sigma_y/(\kappa_y^2 \varepsilon_0)}{j\omega + (\alpha_y + \sigma_y/\kappa_y)/\varepsilon_0} \frac{\partial E_x}{\partial y} \quad (16)$$

$$g_{zx} = \frac{\sigma_x/(\kappa_x^2 \varepsilon_0)}{j\omega + (\alpha_x + \sigma_x/\kappa_x)/\varepsilon_0} \frac{\partial E_y}{\partial x} \quad (17)$$

Substituting (12-17) into (9-11), and then adopting the auxiliary differential equation (ADE) technique, we obtain

$$\varepsilon_0 \varepsilon_r \frac{\partial E_x}{\partial t} + \sigma E_x = (\kappa_y)^{-1} \frac{\partial H_z}{\partial y} - (\kappa_z)^{-1} \frac{\partial H_y}{\partial z} - f_{xy} + f_{xz} \quad (18)$$

$$\mu_0 \frac{\partial H_y}{\partial t} = (\kappa_x)^{-1} \frac{\partial E_z}{\partial x} - (\kappa_z)^{-1} \frac{\partial E_x}{\partial z} - g_{yx} + g_{yz} \quad (19)$$

$$\mu_0 \frac{\partial H_z}{\partial t} = (\kappa_y)^{-1} \frac{\partial E_x}{\partial y} - (\kappa_x)^{-1} \frac{\partial E_y}{\partial x} - g_{zy} + g_{zx} \quad (20)$$

$$\frac{\partial f_{xy}}{\partial t} + \frac{\alpha_y + \sigma_y/\kappa_y}{\varepsilon_0} f_{xy} = \frac{\sigma_y}{\kappa_y^2 \varepsilon_0} \frac{\partial H_z}{\partial y} \quad (21)$$

$$\frac{\partial f_{xz}}{\partial t} + \frac{\alpha_z + \sigma_z/\kappa_z}{\varepsilon_0} f_{xz} = \frac{\sigma_z}{\kappa_z^2 \varepsilon_0} \frac{\partial H_y}{\partial z} \quad (22)$$

$$\frac{\partial g_{yx}}{\partial t} + \frac{\alpha_x + \sigma_x/\kappa_x}{\varepsilon_0} g_{yx} = \frac{\sigma_x}{\kappa_x^2 \varepsilon_0} \frac{\partial E_z}{\partial x} \quad (23)$$

$$\frac{\partial g_{yz}}{\partial t} + \frac{\alpha_z + \sigma_z/\kappa_z}{\varepsilon_0} g_{yz} = \frac{\sigma_z}{\kappa_z^2 \varepsilon_0} \frac{\partial E_x}{\partial z} \quad (24)$$

$$\frac{\partial g_{zy}}{\partial t} + \frac{\alpha_y + \sigma_y/\kappa_y}{g_{zy}} g_{zy} = \frac{\sigma_y}{\kappa_y^2 \varepsilon_0} \frac{\partial E_x}{\partial y} \quad (25)$$

$$\frac{\partial g_{zx}}{\partial t} + \frac{\alpha_x + \sigma_x/\kappa_x}{\varepsilon_0} g_{zx} = \frac{\sigma_x}{\kappa_x^2 \varepsilon_0} \frac{\partial E_y}{\partial x} \quad (26)$$

Subsequently, applying the Crank-Nicolson method to (18)-(26), and then tidy them up, as in (27), shown at the bottom of the page, and (28)–(35), shown at the bottom of the next page.

$$\begin{aligned} & E_x^{n+1} \left(i + \frac{1}{2}, j, k \right) \\ & = C_{exe} E_x^n \left(i + \frac{1}{2}, j, k \right) \\ & + C_{exhz}(j) \frac{1}{\Delta y} \left[H_z^{n+1} \left(i + \frac{1}{2}, j + \frac{1}{2}, k \right) - H_z^{n+1} \left(i + \frac{1}{2}, j - \frac{1}{2}, k \right) + H_z^n \left(i + \frac{1}{2}, j + \frac{1}{2}, k \right) - H_z^n \left(i + \frac{1}{2}, j - \frac{1}{2}, k \right) \right] \\ & - C_{exhy}(k) \frac{1}{\Delta z} \left[H_y^{n+1} \left(i + \frac{1}{2}, j, k + \frac{1}{2} \right) - H_y^{n+1} \left(i + \frac{1}{2}, j, k - \frac{1}{2} \right) + H_y^n \left(i + \frac{1}{2}, j, k + \frac{1}{2} \right) - H_y^n \left(i + \frac{1}{2}, j, k - \frac{1}{2} \right) \right] \\ & - C_{exf} \left[f_{xy}^{n+1} \left(i + \frac{1}{2}, j, k \right) + f_{xy}^n \left(i + \frac{1}{2}, j, k \right) \right] + C_{exf} \left[f_{xz}^{n+1} \left(i + \frac{1}{2}, j, k \right) + f_{xz}^n \left(i + \frac{1}{2}, j, k \right) \right] \quad (27) \end{aligned}$$

Next, substituting (30)–(35) into (27)–(29), we have (36)–(38), as shown at the bottom of the next page, where D_η , ($\eta = x, y$, and z) are central difference derivative approximations [13], and then temporary variables are shown below

$$C_{exe} = \frac{1 - \frac{\sigma \Delta t}{2\epsilon_0 \epsilon_r}}{1 + \frac{\sigma \Delta t}{2\epsilon_0 \epsilon_r}},$$

$$C_{exhz}(j) = \frac{\frac{\Delta t}{2\epsilon_0 \epsilon_r}}{1 + \frac{\sigma \Delta t}{2\epsilon_0 \epsilon_r}} [\kappa_{pml_y}(j)]^{-1},$$

$$C_{exhy}(k) = \frac{\frac{\Delta t}{2\epsilon_0 \epsilon_r}}{1 + \frac{\sigma \Delta t}{2\epsilon_0 \epsilon_r}} [\kappa_{pml_z}(k)]^{-1},$$

$$C_{exf} = \frac{\frac{\Delta t}{2\epsilon_0 \epsilon_r}}{1 + \frac{\sigma \Delta t}{2\epsilon_0 \epsilon_r}},$$

$$C_{hyez}\left(i + \frac{1}{2}\right) = \frac{\Delta t}{2\mu_0 \mu_r} \left[\kappa_{pml_x}^*\left(i + \frac{1}{2}\right) \right]^{-1},$$

$$C_{hyex}\left(k + \frac{1}{2}\right) = \frac{\Delta t}{2\mu_0 \mu_r} \left[\kappa_{pml_z}^*\left(k + \frac{1}{2}\right) \right]^{-1},$$

$$H_y^{n+1}\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) = H_y^n\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right)$$

$$+ C_{hyez}\left(i + \frac{1}{2}\right) \frac{1}{\Delta x} \left[E_z^{n+1}\left(i + 1, j, k + \frac{1}{2}\right) - E_z^{n+1}\left(i, j, k + \frac{1}{2}\right) + E_z^n\left(i + 1, j, k + \frac{1}{2}\right) - E_z^n\left(i, j, k + \frac{1}{2}\right) \right]$$

$$- C_{hyex}\left(k + \frac{1}{2}\right) \frac{1}{\Delta z} \left[E_x^{n+1}\left(i + \frac{1}{2}, j, k + 1\right) - E_x^{n+1}\left(i + \frac{1}{2}, j, k\right) + E_x^n\left(i + \frac{1}{2}, j, k + 1\right) - E_x^n\left(i + \frac{1}{2}, j, k\right) \right]$$

$$- C_{hyg} \left[g_{yx}^{n+1}\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) + g_{yx}^n\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) \right] + C_{hyg} \left[g_{yz}^{n+1}\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) + g_{yz}^n\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) \right] \quad (28)$$

$$H_z^{n+1}\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) = H_z^n\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right)$$

$$+ C_{hzex}\left(j + \frac{1}{2}\right) \frac{1}{\Delta y} \left[E_x^{n+1}\left(i + \frac{1}{2}, j + 1, k\right) - E_x^{n+1}\left(i + \frac{1}{2}, j, k\right) + E_x^n\left(i + \frac{1}{2}, j + 1, k\right) - E_x^n\left(i + \frac{1}{2}, j, k\right) \right]$$

$$- C_{hzey}\left(i + \frac{1}{2}\right) \frac{1}{\Delta x} \left[E_y^{n+1}\left(i + 1, j + \frac{1}{2}, k\right) - E_y^{n+1}\left(i, j + \frac{1}{2}, k\right) + E_y^n\left(i + 1, j + \frac{1}{2}, k\right) - E_y^n\left(i, j + \frac{1}{2}, k\right) \right]$$

$$- C_{hzg} \left[g_{zy}^{n+1}\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) + g_{zy}^{n+1}\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) \right] + C_{hzg} \left[g_{zx}^{n+1}\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) + g_{zx}^{n+1}\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) \right] \quad (29)$$

$$f_{xy}^{n+1}\left(i + \frac{1}{2}, j, k\right) = C_{fxyf}(j) f_{xy}^n\left(i + \frac{1}{2}, j, k\right)$$

$$+ C_{fxyhz}(j) \frac{1}{\Delta y} \left[H_z^{n+1}\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) - H_z^{n+1}\left(i + \frac{1}{2}, j - \frac{1}{2}, k\right) + H_z^n\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) - H_z^n\left(i + \frac{1}{2}, j - \frac{1}{2}, k\right) \right] \quad (30)$$

$$f_{xz}^{n+1}\left(i + \frac{1}{2}, j, k\right) = C_{fxzf}(k) f_{xz}^n\left(i + \frac{1}{2}, j, k\right)$$

$$+ C_{fxzhy}(k) \frac{1}{\Delta z} \left[H_y^{n+1}\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) - H_y^{n+1}\left(i + \frac{1}{2}, j, k - \frac{1}{2}\right) + H_y^n\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) - H_y^n\left(i + \frac{1}{2}, j, k - \frac{1}{2}\right) \right] \quad (31)$$

$$g_{yx}^{n+1}\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) = C_{gyxg}\left(i + \frac{1}{2}\right) g_{yx}^n\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right)$$

$$+ C_{gyxex}\left(i + \frac{1}{2}\right) \frac{1}{\Delta x} \left[E_z^{n+1}\left(i + 1, j, k + \frac{1}{2}\right) - E_z^{n+1}\left(i, j, k + \frac{1}{2}\right) + E_z^n\left(i + 1, j, k + \frac{1}{2}\right) - E_z^n\left(i, j, k + \frac{1}{2}\right) \right] \quad (32)$$

$$g_{yz}^{n+1}\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) = C_{gyzg}\left(k + \frac{1}{2}\right) g_{yz}^n\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right)$$

$$+ C_{gyzex}\left(k + \frac{1}{2}\right) \frac{1}{\Delta z} \left[E_x^{n+1}\left(i + \frac{1}{2}, j, k + 1\right) - E_x^{n+1}\left(i + \frac{1}{2}, j, k\right) + E_x^n\left(i + \frac{1}{2}, j, k + 1\right) - E_x^n\left(i + \frac{1}{2}, j, k\right) \right] \quad (33)$$

$$g_{zy}^{n+1}\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) = C_{gzyg}\left(j + \frac{1}{2}\right) g_{zy}^n\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right)$$

$$+ C_{gzyex}\left(j + \frac{1}{2}\right) \frac{1}{\Delta y} \left[E_x^{n+1}\left(i + \frac{1}{2}, j + 1, k\right) - E_x^{n+1}\left(i + \frac{1}{2}, j, k\right) + E_x^n\left(i + \frac{1}{2}, j + 1, k\right) - E_x^n\left(i + \frac{1}{2}, j, k\right) \right] \quad (34)$$

$$g_{zx}^{n+1}\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) = C_{gzxg}\left(i + \frac{1}{2}\right) g_{zx}^n\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right)$$

$$+ C_{gzxey}\left(i + \frac{1}{2}\right) \frac{1}{\Delta x} \left[E_y^{n+1}\left(i + 1, j + \frac{1}{2}, k\right) - E_y^{n+1}\left(i, j + \frac{1}{2}, k\right) + E_y^n\left(i + 1, j + \frac{1}{2}, k\right) - E_y^n\left(i, j + \frac{1}{2}, k\right) \right] \quad (35)$$

$$C_{hyg} = \frac{\Delta t}{2\mu_0\mu_r},$$

$$C_{hzex}\left(j + \frac{1}{2}\right) = \frac{\Delta t}{2\mu_0\mu_r} \left[k_{pml_y}^* \left(j + \frac{1}{2} \right) \right]^{-1},$$

$$C_{hzey}\left(i + \frac{1}{2}\right) = \frac{\Delta t}{2\mu_0\mu_r} \left[k_{pml_x}^* \left(i + \frac{1}{2} \right) \right]^{-1},$$

$$C_{hzg} = \frac{\Delta t}{2\mu_0\mu_r},$$

Similarly, same operations can be applied to other field components. Therefore, these all equations can be written compactly as

$$(I - D_1 - D_2)W^{n+1} = (U + D_1 + D_2)W^n + V \quad (39)$$

Eq. (39) can be factorized and split as

$$(I - D_1)W^* = (U + D_1 + 2D_2)W^n + V \quad (40)$$

$$(I - D_2)W^{n+1} = W^* - D_2W^n \quad (41)$$

It can be seen that (40)-(41) solve tri-diagonal matrices at each time step to obtain electric field components, while all magnetic field components can be found explicitly.

III. NUMERICAL RESULTS

As mentioned above, we have demonstrated and derived the CFS-CNDS-FDTD formulations, which can be efficiently and accurately utilized to model BP metasurface implementations in the infrared range. To further elaborate and corroborate advantages and applications of the CFS-CNDS-FDTD versus the regular FDTD in solving all-dielectric nanostructures, 3D numerical simulations are carried out to compare the accuracy and the efficiency and accuracy between both the CFS-CNDS-FDTD and the conventional FDTD.

As known to all, the numerical stability of the conventional FDTD method is determined by the CFL condition, which requires that the temporal incremental Δt has a specific bound relative to the lattice 3D-space size $\{\Delta x, \Delta y, \Delta z\}$. Therefore, the CFL factor can be defined in the w -direction as

$$s_w = \frac{c_0 \Delta t}{\sqrt{3} \Delta w} \quad (w = x, y, z) \quad (42)$$

where Δw is the grid scale for FDTD. c_0 is the light speed in vacuum. The CFL factor must satisfy $s_w \leq 1$ in the

$$E_x^{n+1}\left(i + \frac{1}{2}, j, k\right) + [C_{exhy}(k) - C_{exf}C_{fxzhy}(k)]D_z H_y^{n+1}\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) - [C_{exhz}(j) - C_{exf}C_{fxyhz}(j)]D_y H_z^{n+1}\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right)$$

$$= C_{exe}E_x^n\left(i + \frac{1}{2}, j, k\right) - [C_{exhy}(k) - C_{exf}C_{fxzhy}(k)]D_z H_y^n\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right)$$

$$+ [C_{exhz}(j) - C_{exf}C_{fxyhz}(j)]D_y H_z^n\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right)$$

$$- C_{exf} \left[[1 + C_{fxyf}(j)]f_{xy}^n\left(i + \frac{1}{2}, j, k\right) \right] + C_{exf} \left[[1 + C_{fxzf}(k)]f_{xz}^n\left(i + \frac{1}{2}, j, k\right) \right] \quad (36)$$

$$H_y^{n+1}\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) + [C_{hyex}\left(k + \frac{1}{2}\right) - C_{hyg}C_{gyzex}\left(k + \frac{1}{2}\right)]D_z E_x^{n+1}\left(i + \frac{1}{2}, j, k\right)$$

$$- [C_{hyez}\left(i + \frac{1}{2}\right) - C_{hyg}C_{gyxex}\left(i + \frac{1}{2}\right)]D_x E_z^{n+1}\left(i, j, k + \frac{1}{2}\right)$$

$$= H_y^n\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) - [C_{hyex}\left(k + \frac{1}{2}\right) - C_{hyg}C_{gyzex}\left(k + \frac{1}{2}\right)]D_z E_x^n\left(i + \frac{1}{2}, j, k\right)$$

$$+ [C_{hyez}\left(i + \frac{1}{2}\right) - C_{hyg}C_{gyxex}\left(i + \frac{1}{2}\right)]D_x E_z^n\left(i, j, k + \frac{1}{2}\right)$$

$$- C_{hyg} \left[[1 + C_{gyxg}\left(i + \frac{1}{2}\right)]g_{yx}^n\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) + C_{hyg} \left[[1 + C_{gyzg}\left(k + \frac{1}{2}\right)]g_{yz}^n\left(i + \frac{1}{2}, j, k + \frac{1}{2}\right) \right] \right] \quad (37)$$

$$H_z^{n+1}\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) - [C_{hzex}\left(j + \frac{1}{2}\right) - C_{hzg}C_{gzyex}\left(j + \frac{1}{2}\right)]D_y E_x^{n+1}\left(i + \frac{1}{2}, j, k\right)$$

$$+ [C_{hzey}\left(i + \frac{1}{2}\right) - C_{hzg}C_{gzxey}\left(i + \frac{1}{2}\right)]D_x E_y^{n+1}\left(i, j + \frac{1}{2}, k\right)$$

$$= H_z^n\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) + [C_{hzex}\left(j + \frac{1}{2}\right) - C_{hzg}C_{gzyex}\left(j + \frac{1}{2}\right)]D_y E_x^n\left(i + \frac{1}{2}, j, k\right)$$

$$- [C_{hzey}\left(i + \frac{1}{2}\right) - C_{hzg}C_{gzxey}\left(i + \frac{1}{2}\right)]D_x E_y^n\left(i, j + \frac{1}{2}, k\right)$$

$$- C_{hzg} \left[[1 + C_{gzyg}\left(j + \frac{1}{2}\right)]g_{zy}^n\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) + C_{hzg} \left[[1 + C_{gzxg}\left(i + \frac{1}{2}\right)]g_{zx}^n\left(i + \frac{1}{2}, j + \frac{1}{2}, k\right) \right] \right] \quad (38)$$

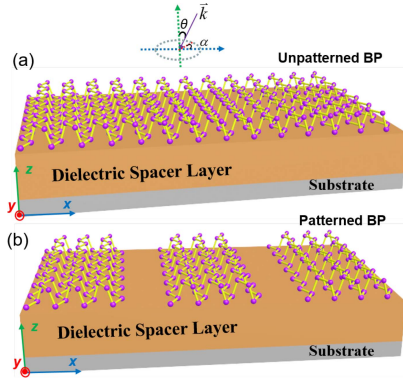


FIGURE 1. (a) Proposed nanostructure with unpatterned BP, where armchair and zigzag directions are along the x axis and y axis, respectively. (b) Patterned BP. The symbols α and θ represent the azimuth and elevation angles of incident light, respectively.

conventional FDTD method, whereas the implicit FDTD can break through the CFL factor s_w due to its unconditional stability. However, how to choose maximum CFL factor s will be a vital problem.

In general, FDTD results are affected by spatial sampling and temporal sampling densities. The spatial sampling density refers to the number of points per wavelength (PPW) at the highest frequency in the interested frequency band, while the temporal sampling density represents the number of points per period (PPP) at the highest frequency. The spatial sampling and temporal sampling densities are respectively expressed by

$$Q_{s,w}(\text{PPW}) = \frac{\lambda_{\min}}{\Delta w} = \frac{c_0}{f_{\max} \Delta w} \quad (43)$$

$$Q_t(\text{PPP}) = \frac{T_{\min}}{\Delta t} = \frac{1}{f_{\max} \Delta t} \quad (44)$$

where minimum wavelength λ_{\min} and period T_{\min} are restricted by the maximum frequency f_{\max} of input impulse.

The design of proposed photonic nanostructures based on the monolayer BP with/without patterning is shown in Fig. 1. The structure consists of an alumina (Al_2O_3), a substrate, and a monolayer BP with/without patterning, respectively, shown in Fig. 1(a, b). The whole nanostructure in size is finished with a $67 \text{ nm} \times 67 \text{ nm} \times 50.25 \text{ nm}$ FDTD domain, and its space is discretized with a uniform grid with $\Delta x = \Delta y = \Delta z = 0.67 \text{ nm}$. The receiver is placed at $(40.2, 40.2, 44.89) \text{ nm}$ for all cases.

In our design, the dielectric layers of Al_2O_3 ($= 33.5 \text{ nm}$ of thickness) and substrate ($= 6.7 \text{ nm}$ thickness) are assumed to be nonmagnetic ($\mu = \mu_0$), and optically lossless with the refractive index of 1.7 and 1.48, respectively. In addition, the monolayer BP ($= 2.68 \text{ nm}$ thickness), shown in Fig. 1(a, b), is depicted by adopting a simple semi-classical Drude model [21], [22], for both x and y cases, respectively, defined as

$$\sigma_i = jD_i / \left(\pi \left(\omega + \frac{j\eta}{\hbar} \right) \right) \quad (45)$$

where i denotes the direction concerned, and D_i is the Drude weight, written below

$$D_i = \pi e^2 n / m_i \quad (46)$$

where m_i ($i = x, y$) are the electron effective mass along x and y directions, and denoted by adopting $m_{cx} = \hbar^2 / (2\gamma^2 / \varsigma + \eta_c)$ and $m_{cy} = \hbar^2 / (2\nu_c)$. Both $\epsilon_x(\omega)$ and $\epsilon_y(\omega)$ are the dielectric constants of the monolayer BP for both x and y directions, respectively, written below

$$\epsilon_i = \epsilon_r + \frac{j\sigma_i}{\epsilon_0 \omega a} \quad (47)$$

Via a series of manipulations of σ_i and ϵ_i ($i = x, y$), we obtain

$$\sigma_i = \frac{A_i}{B_i + j\omega} \quad (48)$$

$$\epsilon_i = \epsilon_r - \frac{Q_i}{j\omega} + \frac{Q_i}{B_i + j\omega} \quad (49)$$

where $A_i = -D_i / \pi$, $B_i = -\eta / \hbar$, and $Q_i = A_i / (\epsilon_0 a B_i)$. As depicted in [22], the parameters of BP are determined by fitting the known anisotropic mass for x - and y -direction. For BP, we have

$$\gamma = \frac{4a}{\pi} eV, \varsigma = 2eV, \eta_c = \frac{\hbar^2}{0.4m_0}, \nu_c = \frac{\hbar^2}{1.4m_0}$$

In additions, the relaxation rate can be described via choosing the electronic doping $n = 10^{13} \text{ cm}^{-2}$ and $\eta = 10 \text{ meV}$. a is the scale length of the BP, and π/a is the width of the Brillouin Zone in [21], [22].

As shown in Fig. 1, the source is excited by a bipolar square wave pulse with the repetition frequency of 2.5 THz. we here set the window time of 0.16 ps in the horizontal axis to observe the stability of electric field component in the x - and y - direction at the receiver point.

We test first case on the 3D nanostructures with monolayer BP without patterning with the proposed CFS-CNDS-FDTD method with different temporal discretization density and use the results by the conventional explicit FDTD method and the CFS-ADI-FDTD in [46] as the reference.

The Fig. 2 plots simulation results for a receiver for these three different schemes as obtained with different temporal sampling densities in terms of number of PPP. Corresponding to this sampling density, the CFL number is defined as $CFLN = \Delta t / \Delta t_{\max}^{FDTD}$, where Δt_{\max}^{FDTD} is the maximum time interval under the stability condition of the regular FDTD algorithm. It should be noted in Fig. 2 that even at such large $CFLN$ values simulation results of the proposed CFS-CNDS-FDTD are just as good as those of both the conventional explicit FDTD and the CFS-ADI-FDTD in [46].

Besides, it is clearly reflected in Table 1 that the proposed CFS-CNDS-FDTD can save massive CPU time as compared with that of the conventional FDTD.

Similarly, it can be also observed that the good agreement can be achieved for the 3D nanostructures with monolayer BP with patterning among these FDTD methods, shown in Fig. 3.

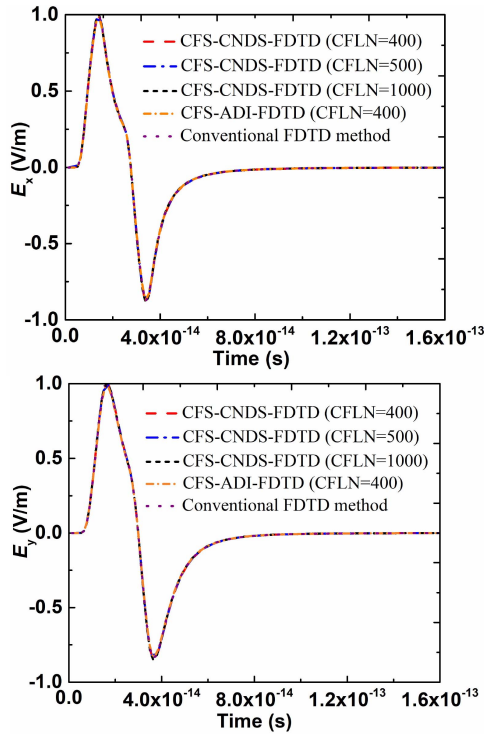


FIGURE 2. Electrical field E_x and E_y evaluated by the conventional FDTD, the CFS-CNDS-FDTD, and the CFS-ADI-FDTD.

TABLE 1. Computational Time for Different CFLNs

FDTD methods with CFLNs	CPU Time (s)	P (%)
Conventional FDTD method	118000	100
CFS-CNDS-FDTD (CFLN=400)	5462.95	4.6
CFS-CNDS-FDTD (CFLN=500)	4573.83	3.8
CFS-CNDS-FDTD (CFLN=1000)	2232.08	1.8
CFS-ADI-FDTD (CFLN=400)	6612.42	5.6

To show absorption abilities of the proposed CNDS-FDTD, conventional FDTD, and ADI-FDTD based on CFS-PML. We here provide reflective reflection errors of these three methods to compare their absorption accuracies for the case of Fig. 1(a).

It is shown in the above numerical result that the maximum relative reflection errors of Conventional FDTD, CFS-CNDS-FDTD, CFS-ADI-FDTD, are -75.5233 dB, -64.5135 dB, and -54.9536 dB, respectively. As reflected in Fig. 4, therefore, the proposed CNDS-FDTD can obtain better absorption accuracy than the ADI-FDTD.

To further validate the robustness and performance of the CFS-CNDS-FDTD, we next build up and implement the 3D all-dielectric nanostructures with a monolayer BP, which can consist of a BP monolayer (= 2.68 nm of thickness), a Calcium Fluoride (CaF_2) layer (=4.02 nm of thickness), a transparent substrate (=2.01 nm of thickness), the mirror with a stack of dielectric layers of alternate Zirconia (ZrO_2) (=2.01 nm of thickness) and Cryolite (Na_3AlF_6) (=6.03 nm of thickness), and periodic silica (SiO_2) nanoribbons (=3.35 nm of thickness), shown in Fig. 5.

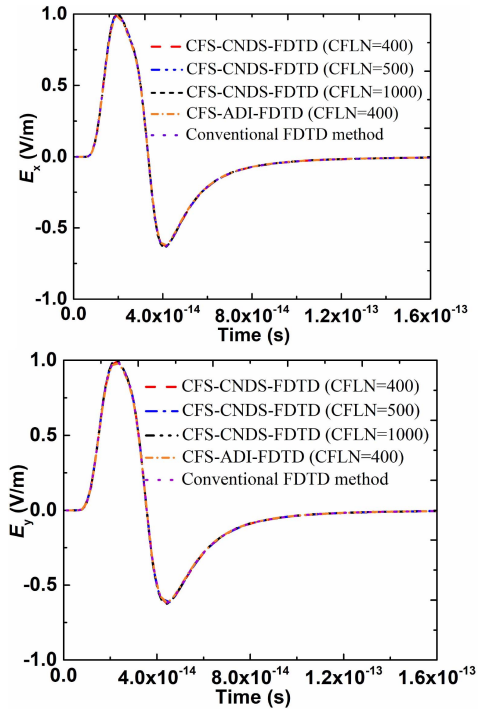


FIGURE 3. Electrical field (a) E_x and (b) E_y evaluated by the conventional FDTD, the CFS-CNDS-FDTD, and the CFS-ADI-FDTD.

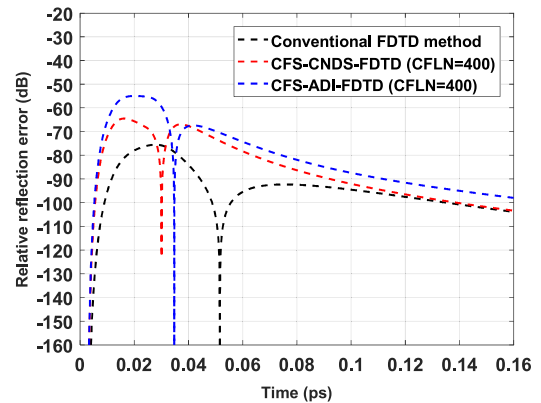


FIGURE 4. Relative reflection error versus time for Conventional FDTD method, CFS-CNDS-FDTD (CFLN = 400), CFS-ADI-FDTD (CFLN = 400).

The whole nanostructure domain is done with a $67 \text{ nm} \times 67 \text{ nm} \times 50.25 \text{ nm}$ FDTD domain, and its space is discretized with a uniform grid with $\Delta x = \Delta y = \Delta z = 0.67 \text{ nm}$. In our design, the dielectric layers of CaF_2 , ZrO_2 , SiO_2 , Na_3AlF_6 and substrate are assumed to be nonmagnetic, and optically lossless with the refractive index of 1.45, 2.6, 1.48, 1.33, and 1.48, respectively.

In the same way, we here adopt identical source and window time to observe and validate the stability and performance of the CFS-CNDS-FDTD method. The 3D nanostructures adding a monolayer BP without periodic SiO_2 nanoribbons is studied using the proposed CFS-CNDS-FDTD method with different PPP, and then compares the results by the conventional explicit FDTD and CFS-ADI-FDTD methods in [46], shown in Fig. 5(a).

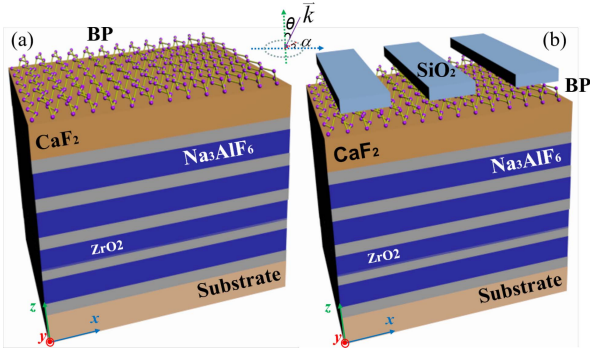


FIGURE 5. (a) Proposed nanostructure adding unpatterned BP without a periodic SiO_2 , where armchair and zigzag directions are along the x axis and y axis, respectively. (b) with a periodic SiO_2 . The symbols α and θ represent the azimuth and elevation angles of incident light, respectively.

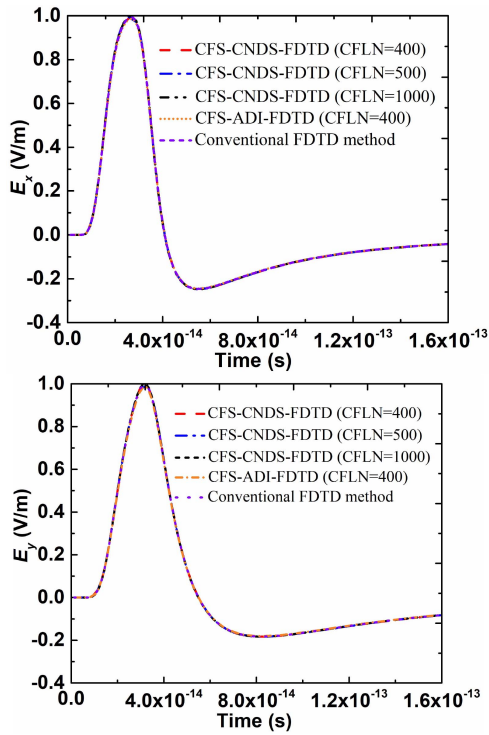


FIGURE 6. Electrical field (a) E_x and (b) E_y evaluated by the conventional FDTD, the CFS-CNDS-FDTD, and the CFS-ADI-FDTD.

TABLE 2. Computational Time for Different CFLNs

FDTD methods with CFLNs	CPU Time (s)	P (%)
Conventional FDTD method	118066	100
CFS-CNDS-FDTD (CFLN=400)	5476.65	4.63
CFS-CNDS-FDTD (CFLN=500)	4598.43	3.89
CFS-CNDS-FDTD (CFLN=1000)	2259.28	1.91
CFS-ADI-FDTD (CFLN=400)	6632.12	5.6

As shown in Fig. 6, the good agreement is obtained among the conventional explicit FDTD, the CFS-ADI- and the CFS- CNDS-FDTDs with different CFLNs. Furthermore, the Table 2 indicates that the proposed CFS-CNDS-FDTD can occupy substantially less CPU time than that of the regular FDTD.

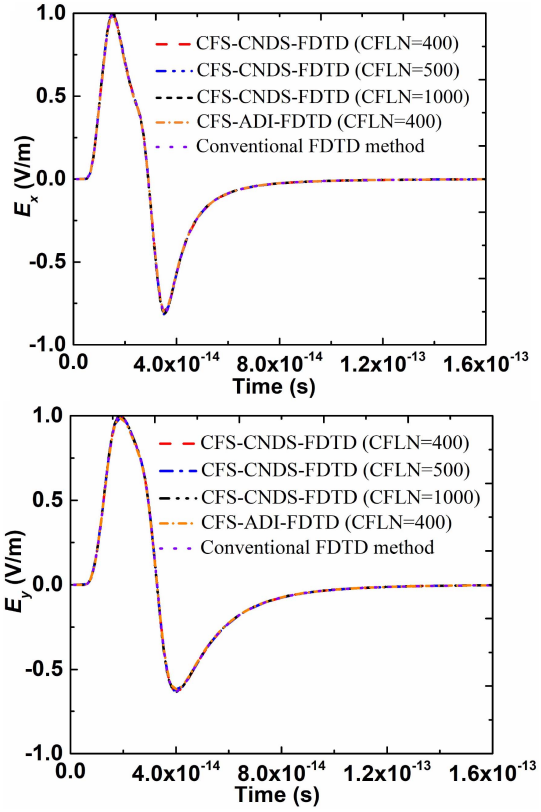


FIGURE 7. Electrical field (a) E_x and (b) E_y evaluated by the conventional FDTD, the CFS-CNDS-FDTD, and the CFS-ADI-FDTD.

Recently, the design of a 3D all-dielectric nanostructure is presented with periodic SiO_2 nanoribbons and 2D graphene in [18], which can obviously enhance light-matter interaction. To further analyze and unveil the physics of periodic structures subsequently, now the periodic SiO_2 is put atop the monolayer BP for validating the accuracy of CFS-CNDS-FDTD method, shown in Fig. 5(b).

As reflected in Fig. 7, we can again observe good agreement among the implicit CN-FDTD and the explicit FDTD methods, therefore, the good performance of the CFS-CNDS-FDTD for modeling all-dielectric nanostructures with BP metasurface is corroborated.

To show absorption abilities of the proposed CNDS-FDTD, conventional FDTD, and ADI-FDTD based on CFS-PML. We here provide reflective reflection errors of these three methods to compare their absorption accuracies for the case of Fig. 5(a).

It is shown in the above numerical result that the maximum relative reflection errors of Conventional FDTD, CFS-CNDS- FDTD, CFS-ADI-FDTD, are -70.0159 dB, -65.0919 dB, and -55.4651 dB, respectively. As reflected in Fig. 8, therefore, the proposed CNDS-FDTD can obtain better absorption accuracy than the ADI-FDTD.

As a result, it will become more practical and efficient if the proposed CFS-CNDS-FDTD method is adopted to solve the 3D all-dielectric nanostructures with the 2DLM

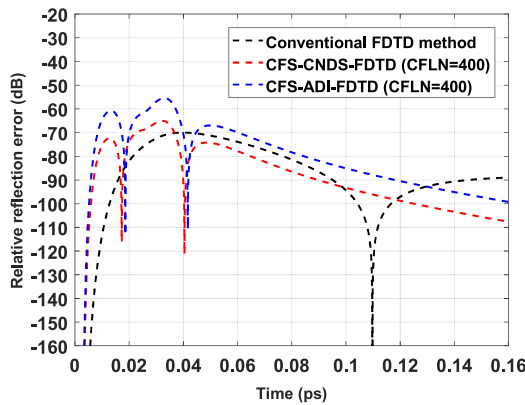


FIGURE 8. Relative reflection error versus time for Conventional FDTD method, CFS-CNDS-FDTD (CFLN = 400), CFS-ADI-FDTD (CFLN = 400).

material in the infrared range instead of the conventional FDTD method.

IV. CONCLUSION

A CFS-CNDS-FDTD has been developed and presented for infrared 2DLM metasurface implementation on all-dielectric nanostructures. The proposed CFS-CNDS-FDTD can greatly improve the computational efficiency when solving infrared terahertz problems with few-atomic-layer thickness of 2DLMs due to possessing capabilities of implicit FDTD method and unsplit-field CFS-PML. As shown in 3D numerical cases, the temporal incremental in CFS-CNDS-FDTD method can reach 1000 times larger than that in the regular FDTD for infrared problems while keeping pinpoint. As a consequence, the CFS-CNDS-FDTD can not only achieve high accuracies and saves several dozen times of CPU time as compared to the regular FDTD, but also pave the road for high-efficient designs of 3D all-dielectric nanostructures with 2DLM metasurfaces.

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