

Enigmas, etc.

Solution to Last Month's Quiz

■ Takashi Ohira ^{ID}

The circuit diagram from last month's problem is shown in Figure 1, where the three voltages are related as

$$v_s(t) + v_D(t) + v_L(t) = 48 \quad (1)$$

to meet Kirchhoff's voltage law. The time-domain analysis starts at $t = 0$. The source voltage $v_s(t)$ linearly increases with t up until it reaches the peak, as shown in Figure 2(a). This is simply formulated as

$$v_s(t) = 100t. \quad (2)$$

The very moment $v_s(t)$ crosses 48 V, the diode D turns on. As long as diode D stays on, $v_D(t)$ is kept at zero. Therefore, (1) leads the inductor voltage to

$$v_L(t) = 48 - 100t \quad \text{for } 0.48 < t < 1. \quad (3)$$

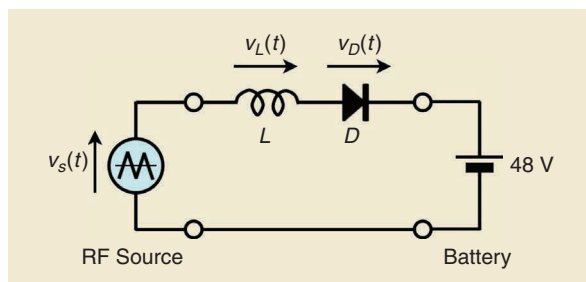


Figure 1. The battery-charging circuit in question.

Takashi Ohira (ohira@tut.jp) is with Toyohashi University of Technology, Aichi 441-8580 Japan. He is a Life Fellow of IEEE.

Digital Object Identifier 10.1109/MMM.2022.3218178
Date of current version: 5 January 2023

After passing the peak, $v_s(t)$ decreases as

$$v_s(t) = 200 - 100t. \quad (4)$$

Because diode D still remains on, (1) leads to

$$v_L(t) = 100t - 152 \quad \text{for } 1 < t < \tau \quad (5)$$

where τ denotes the turn-off moment.

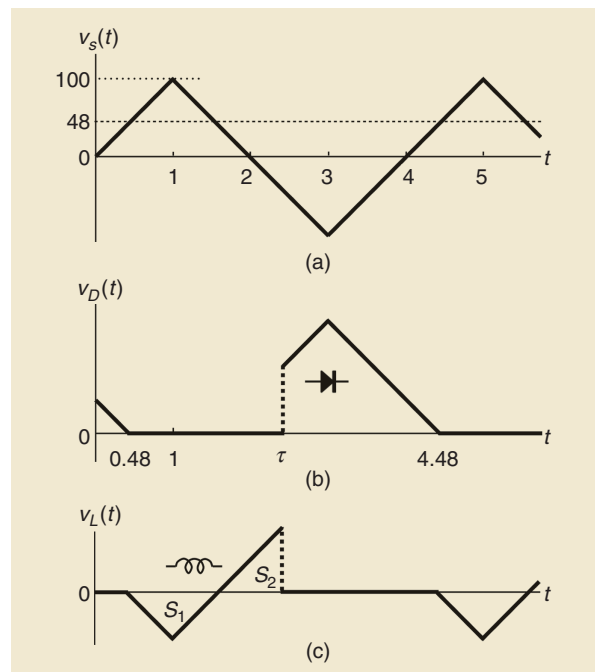


Figure 2. The voltage waveforms of (a) the RF source, (b) the diode, and (c) the inductor.

Looking at the downhill slope of (4), one might have thought that the moment $v_s(t)$ falls across 48 V, it makes diode D turn off. However, that is not true. Because of the inductor's inherent property, it is hard for the current to change quickly. To find where τ is exactly located, we use another inherent property of lossless inductors: the voltage across L contains no dc component. This is formulated as

$$\oint v_L(t)dt = 0 \quad (6)$$


where the circular symbol means an integral for one cycle.

Applying (6) to (3) and (5) gives

$$\int_{0.48}^1 (48 - 100t)dt + \int_1^{\tau} (100t - 152)dt = 0. \quad (7)$$

Note that the integration is performed only when diode D stays on because $v_L(t)$ is kept at zero when

diode D stays off. Solving (7), we find $\tau \approx 2.255$, which is located before the peak. As a result, the pyramid of $v_D(t)$ is truncated, as shown in Figure 2(b). Therefore, the correct answer to last month's quiz is (b). The zero-mean waveform of $v_L(t)$ is also worth viewing from graphics. Focusing on the two triangles indicated by S_1 and S_2 in Figure 2(c), we notice that (7) is translated into the area balance as $S_1 = S_2$.

Paralleling the waveforms of $v_D(t)$ and $v_L(t)$, a simultaneous discontinuity is observed with vertical broken lines. That is to say, the linearly increasing $v_L(t)$ suddenly transfers to $v_D(t)$ at $t = \tau$. By contrast, $v_D(t)$ holds continuity back at $t = 0.48$, which is called *zero-voltage switching (ZVS)*; namely, $v_D(0.48) = 0$. It is a general feature of $L + D$ in series that D turns on in ZVS, whereas it turns off in non-ZVS. This law applies not just to the simple battery charger but also to any other diode-oriented RF power electronics, such as rectennas for wireless power transfer. 

Educator's Corner (continued from page 91)

the 3-dB bandwidth, our simulations showed that, for higher values of k , the frequency response shape was more of a highpass filter, with an overunity gain in the left side, just like overshoot in the step response. Therefore, except for lower values of k , the upper 3-dB point is not meaningful.

Conclusions

It has been shown that a UDRC network is able to achieve a maximum gain of 1.148 for high values of k . This has not been known in the existing literature, and it is hoped that teachers and students of electrical engineering will take notice of this fact. Distributed RC modeling of interconnects is essential in microwave circuits as the energy transmission through them is not instantaneous,

and the transmission delays play an important part in the characteristics of the designed circuit.

Acknowledgment

We thank the editor-in-chief of *IEEE Microwave Magazine* for his valuable suggestions, which helped to improve the manuscript.

References

- [1] W. M. Kaufman, "Theory of a monolithic, null device and some novel circuits," *Proc. IRE*, vol. 48, no. 9, pp. 1540–1545, Sep. 1960, doi: 10.1109/JRPROC.1960.287667.
- [2] W. W. Happ, "Synthesis of distributed-parameter networks," *Proc. IRE*, vol. 50, pp. 483–484, Apr. 1962.
- [3] W. A. Edson, "Tapered distributed RC lines for phase-shift oscillators," *Proc. IRE*, vol. 49, no. 6, pp. 1021–1024, Jun. 1961, doi: 10.1109/JRPROC.1961.287884.
- [4] B. L. H. Wilson and R. B. Wilson, "Shaping of distributed RC networks," *Proc. IRE*, vol. 49, pp. 1021–1031, Aug. 1961.

- [5] M. J. Hellstorm, "Symmetrical RC distributed networks," *Proc. IRE*, vol. 50, pp. 97–98, Jan. 1962.
- [6] S. C. Dutta Roy, "Theory of exponentially tapered RC transmission lines for phase-shift oscillators," *Proc. Inst. Elect. Eng.*, vol. 110, no. 10, pp. 1764–1770, Oct. 1963, doi: 10.1049/ptee.1963.0250.
- [7] S. C. Dutta Roy, "On some three-terminal lumped and distributed RC null networks," *IEEE Trans. Circuit Theory*, vol. 11, no. 1, pp. 98–103, Mar. 1964, doi: 10.1109/TCT.1964.1082239.
- [8] S. C. Dutta Roy, "Revisiting passive RC networks with over unity gain," submitted for publication.
- [9] W. C. Elmore, "The transient response of damped linear networks with particular regard to wideband amplifiers," *J. Appl. Phys.*, vol. 19, no. 1, pp. 55–63, Jan. 1948, doi: 10.1063/1.1697872.
- [10] J. Millman and C. Halkias, *Integrated Electronics: Analog and Digital Circuits and Systems*. New York, NY, USA: McGraw-Hill, 1947.