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# **Stop Oversampling for Class Imbalance Learning: A Review**

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**ABSTRACT** For the last two decades, oversampling has been employed to overcome the challenge of learning from imbalanced datasets. Many approaches to solving this challenge have been offered in the literature. Oversampling, on the other hand, is a concern. That is, models trained on fictitious data may fail spectacularly when put to real-world problems. The fundamental difficulty with oversampling approaches is that, given a real-life population, the synthesized samples may not truly belong to the minority class. As a result, training a classifier on these samples while pretending they represent minority may result in incorrect predictions when the model is used in the real world. We analyzed a large number of oversampling methods in this paper and devised a new oversampling evaluation system based on hiding a number of majority examples and comparing them to those generated by the oversampling process. Based on our evaluation system, we ranked all these methods based on their incorrectly generated examples for comparison. Our experiments using more than 70 oversampling methods and nine imbalanced real-world datasets reveal that all oversampling methods studied generate minority samples that are most likely to be majority. Given data and methods in hand, we argue that oversampling in its current forms and methodologies is unreliable for learning from class imbalanced data and should be avoided in real-world applications.

**INDEX TERMS** Oversampling, SMOTE, imbalanced datasets, machine learning, Hassanat metric.

## I. INTRODUCTION

When training a dataset with examples from one class greatly outnumbering those from the other, a phenomenon known as class imbalance emerges. The majority class is usually referred to as such, whereas the minority class is referred to as such. There may be more than one majority class and more than one minority class in a single dataset. The main cause of class imbalance is that classifiers trained on unequal training sets have a prediction bias, which is linked to poor performance in the minority class(es), Depending on the dataset utilized, the bias could range from a little imbalance to a severe imbalance [1]–[5]. This problem has grown and has become a significant difficulty since the minority class is frequently of critical importance, as it represents favorable examples that are rare in nature or expensive to obtain [6]. This is true when considering contexts such as Big Data analytics [7]–[13],

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Biometrics [14]–[22], gene profiling [23], credit card fraud detection [24], [25], face image retrieval [24], contentbased image retrieval [26], [27], disease detection [28]–[32], internet of things [33]–[43], Natural Language Processing [44], [45], network security [46]–[52], image recognition [53]–[58], Anomaly Detection [59]–[69], etc.

In formal terms, a supervised machine learning dataset *D* with *n* instances belonging to *m* classes C1, C2, C3, ..., Cm is said to be a class imbalanced dataset if and only if for any  $Ci, Cj \exists |Ci| \gg |Cj|$ , where *i* and *j* are indexes 1, 2, 3, ..., m, and  $i \neq j$ .

There are several approaches to solving class imbalance problem before starting classification, such as:

- More samples from the minority class(es) should be acquired from the knowledge domain.
- Changing the loss function to give the failing minority class a higher cost [70].
- Oversampling the minority class.
- Undersampling the majority class.

• Any combination of previous approaches.

Each of the aforementioned approaches has its own set of benefits and drawbacks [71], [72]. Oversampling, on the other hand, is the most often used approach among them, as seen by the multitude of oversampling methods published in the last two decades. However, this does not necessarily imply that the oversampling approach is beneficial. Oversampling approaches boost the quantity of minority-class instances by creating new ones out of thin air based only on their similarity to one or more of the minority's examples. This is troublesome since such methods may raise the likelihood of the learning process being overfitted [73]-[75], [75], [76]. On paper, the overfitted synthetic datasets produce good machine learning results, however this is not always the case in practice. Another more critical problem of oversampling is that the fabricated examples could exist in the real world belonging to a different class, regardless of how similar it is to the minority's examples, as we always have examples from class A that are the closest to examples from a different class B. Therefore, we argue that, even if such synthesizing generates favorable outcomes on paper, negative results can be easily obtained in practice. The major goal of this study, in addition to reviewing a large number of oversampling methods, is to prove our counterclaim on the use of oversampling as a solution to the problem of class imbalance, which is as follows:

Oversampling in its current forms and methodologies is a misleading approach that should be avoided since it feeds the learning process with falsified instances that are pushed to be members of the minority class when they are most likely members of the majority.

To the best of our knowledge, the only methodology for proving an oversampling method's goodness is its classification accuracy metrics after the classification of the oversampled datasets, with no tests for the validity of the synthesized instances and if they are appropriate for training a model for real-world use. Therefore, we find oversampling practitioners are pleased with their machine learning outcomes in the lab, but they should consider how much harm could be done in practice outside of the lab, particularly in medical and other vital applications. The harm is exacerbated when we realize that several of these methods have become integral parts of APIs and machine learning packages, such as Python imbalanced-learn API [77] and Smote-Variants API [78]. We prove our counterclaim in this paper by using a number of typical oversampling methods on several benchmark datasets, concealing some of the majority examples, and then comparing the created examples to the hidden majority examples to determine if they approximately match. Finding such counter examples proves our counterclaim.

The following is the structure of this paper: The literature review of class imbalance problem is presented in the second section. The mythology of proving our counterclaim is illustrated in Section Three. And the experimental results are listed and discussed in section four.



FIGURE 1. The number of publications that have the terms "oversampling" and/or "SMOTE."

### **II. LITERATURE REVIEW OF OVERSAMPLING METHODS**

In the literature, there are various ways to machine learning from class imbalance data. One of the most prevalent ways is oversampling, particularly Synthetic Minority Oversampling Technique approaches (SMOTE). On January 26, 2022, a Google Scholar search for the term "SMOTE" yielded 77,300 results, while a search for "oversampling" yielded 297,000 results. This is merely a foreshadowing of the developing trend of oversampling. Figure 1 depicts the nearly exponential increase in the number of articles that dealt with, employed, or addressed oversampling and/or SMOTE.

The relevance of the well-defined class imbalance problem and the simplicity of oversampling solutions are the reasons for this abnormal surge in oversampling research. Anyone with a rudimentary understanding of machine learning can come up with a novel way to produce fresh similar examples given some minority examples. There could be an infinite number of such solutions.

Several studies, such as [1], [79], [80], have reviewed various oversampling approaches; nevertheless, they are not thorough and have not paid adequate attention to validating the oversampling approach to the problem of class imbalance.

One of the earliest and most extensively utilized approaches for class imbalance is the SMOTE method [81]. It interpolates synthetic examples between nearest neighbors from the training set's collection of minority class cases. As a result, by merging the properties of seed instances with randomly picked k-nearest neighbors, a synthetic sample is generated. The earliest version of the SMOTE algorithm relied solely on synthetic oversampling. They also used a combination of synthetic oversampling and undersampling, which might be useful [82]. SMOTE was tested on nine benchmark datasets and proven to improve classification performance.

SVMSMOTE [83], which is based on SMOTE, focuses on constructing SVM modifications to successfully handle the problem of class imbalance. Oversampling, cost-sensitive learning, and undersampling are some of the heuristics used in SVM modeling. This method produced promising results when compared to other oversampling methods. Borderline-SMOTE [84] is an SMOTE-based minority oversampling method that only oversamples the minority examples around the borderline. In comparison to SMOTE and other random oversampling methods investigated, their findings show that this solution improves classification results for the minority class.

Oversampling by a synthetic inverse minority is used in Reverse-SMOTE (R-SMOTE) [85], a technique based on SMOTE and the inverse near-neighbor idea. R-SMOTE beats other over-sampling methods in terms of precision, F-measurement, and accuracy, according to this study that compared traditional sampling procedures to alternative methods, including SMOTE. In the comparison, eight benchmark datasets were employed.

Constrained Oversampling (CO) [86] is a technique for reducing noise in oversampling. This method is used to extract the overlapping regions in a dataset. Ant Colony Optimization is then used to define the boundaries of minority regions. Most significantly, in order to create a balanced dataset, fresh samples are synthesized via oversampling under constraints. This method varies from others in that it includes noise-reduction constraints in the oversampling process. CO outperforms a range of oversampling benchmarks, according to their results.

In addition, the Majority Weighted Minority Oversampling Technique (MWMOTE) [87] was offered as a solution to the problem of class-imbalance learning. MWMOTE finds and weights difficult-to-learn informative minority class samples based on their distance from nearby majority class samples. It then creates synthetic samples from the weighted informative minority class samples using a clustering algorithm. The primary premise of MWMOTE is that all generated samples must belong to one of the minority class clusters. In terms of numerous assessment measures, the provided results suggest that MWMOTE is superior than or similar to some other existing approaches.

Adaptive synthetic (ADASYN) [88] was given with the goal of eliminating bias and moving the classification decision boundary in the direction of the hard examples. The primary idea behind ADASYN is to use a weighted distribution for different minority class examples based on their learning difficulty, with more synthetic data created for more difficult minority class examples than for easier minority class examples. The efficacy of this method is proved by the results of experiments conducted on a variety of datasets using five different evaluation measures.

Synthetic Minority Over-Sampling Technique Based on Furthest Neighbor Algorithm (SOMTEFUNA) [6] is another exciting and recent method for machine learning from imbalanced datasets. To produce fresh synthetic minority examples, this method employs the farthest neighbor examples. SOMTEFUNA has a number of advantages over some other approaches, one of which being the lack of tuning parameters, which makes it easier to be used in real-world scenarios. Using Naive Bayes and Support Vector Machine classifiers, the method compared the benefits of resampling to common methods such as SMOTE and ADASYN. The reported findings show that SOMTEFUNA is a viable alternative to the other oversampling methods, according to its reported results.

Sampling WIth the Majority (SWIM) [89] is a synthetic oversampling method that is robust in cases of significant class imbalance. SWIM's fundamental feature is that it uses the density of the well-sampled majority class to direct the creation process. SWIM's model was built using both the radial basis function and the Mahalanobis distance. SWIM was put to the test on 25 benchmark datasets, and the findings show that it beats some of the most common oversampling methods.

Other ways of oversampling include, but are not limited to, the work of [78], [90]–[118].

The validation process is what all oversampling methods have in common, which is basically the evaluation of the classifier's performance employed to classify the oversampled datasets using one or more accuracy measures such as Accuracy, Precision, Recall, F-measure, G-mean, Specificity, Kappa, Matthews correlation coefficient (MCC), Area under the ROC Curve (AUC), True positive rate, False negative (FN), False positive (FP), True positive rate, False negative (FN), and ROC curve. Table 1 lists 72 oversampling methods, including their known names, references, the number of datasets utilized, the number of classes in these datasets, the classifiers employed, and the performance metrics used to validate the classification results after oversampling.

As can be seen from the previous discussion and Table 1, all the aforementioned oversampling methods use the classification accuracy measures of the synthesized data to verify their goodness, assuming that the synthesised examples belong to the minority class. On paper, however, the accuracy measures appear to be good if the data is over-fitted, which is common when using Oversampling methods [71]–[76].

Another critical problem with the oversampling approach is the assumption that the synthetic examples belong to the minority class; do they truly belong to the minority class?

None of the previous literature has answered this critical question. This study aims to provide a validation system for oversampling methods, in order to determine to what degree these methods synthesize unrealistic examples; assuming they are belonging to the minority when they are not.

## **III. METHOD AND DATA**

The proposed validation system for oversampling methods works by hiding a subset of the majority's examples, which is referred to as the hidden subset. Although the hidden majority examples are part of the population, we excluded them from the training dataset since we assumed they were not obtained from the real-world knowledge domain. Because all oversampling approaches do not access the entire realworld population, this assumption is correct.

It is important to make sure that the class imbalance problem still exists after concealing the hidden subset. \_

TABLE 1. Summary of the methods used in this study. In this table, C4.5 is Decision Tree C4.5, LR is Logistic Regression, LDA is linear discriminate	
analysis, NB is naive bayes, RF is random forest and ANN is artificial neural network.	

ID	Method Name	Reference	No. Datasets	No. Classes	Classifiers	Performance measures		
					C4.5	ROC curve		
M1	SMOTE	[81]	6	Binary	Ripper NB	AUC		
M2	SMOTE TomekLinks	[119]	13	Binary	C4.5	AUC		
M3	SMOTE ENN	[119]	13	Binary	C4.5	AUC		
М4	Bordarlina SMOTE1	[8/]	4	Binory	C4.5	TP rate		
1914	Dordennie SwiOTET	[04]	4	Billal y	C4.5	F-values		
M5	Borderline SMOTE2	[8/1]	4	Binary	C4.5	TP rate		
1115	bolderinie Swi0122	[0+]	-	Dinary	C <del>1</del> .5	F-values		
						Accuracy, Precision		
M6	ADASYN	[89]	5	Binary	C4.5	Recall, F-measure		
						G-mean		
					C4.5	Recall, Specificity		
M7	AHC	[121]	1	Binary	KNN, SVM	Accuracy		
		[]	-	j	NB	ROC, G-mean		
					AdaBoost	weighted accuracy		
		[100]	10	D		Precision		
<b>M8</b>	distance SMOTE	[122]	10	Binary	Linear Regression	Recall		
MO		[100]	1	D	CVD /	F-measure		
M9	polynom fit SMOTE	[123]	1	Binary	SVM	IP rate, IN rate		
M10	Stafanowski	[124]	0	Dinom	C4.5	Specificity		
WIIU	Steranowski	[124]	9	Dillary	MODLEM	Beenll		
M11	ADOMS	[125]	12	Binary	ANN	G mean		
19111	ADOMS	[123]	12	Dillary		Precision Recall		
M12	Safe Level SMOTE	[126]	2	Binary	NB, SVM	F-values AUC		
					C4.5	Precision, Recall		
M13	MSMOTE	[127]	3	Binary	AdaBoost	F-values		
M14	DE oversampling	[128]	10	Binary	SVM	F-measure, AUC		
M15	SMOBD	[129]	9	Binary	SVM	G-mean, AUC		
M16	SUNDO	[120]	4	Dinomy	CADT SVM	Accuracy, TP		
WI10	SUNDO	[130]	4	ыпагу	CARI, SVM	TN, FP, FN		
M17	MSYN	[131]	10	Binary	C4.5	AUC, F-measure		
					ANN	Accuracy Recall		
M18	SVM balance	[132]	1	Binary	RF	Specificity AUC		
					LR	specificity, nee		
M19	TRIM SMOTE	[133]	11	Binary	C4.5	AUC, F-measure		
M20	SMOTE RSB	[134]	44	Binary	C4.5	AUC		
M21	ProWSvn	[135]	10	Binary	ANN	F-measure		
	,			5	C4.5	G-mean, AUC		
MAAA		[126]	0	D	KNN, RIPPER			
<b>NIZZ</b>	SL graph SMOTE	[130]	8	Binary	C4.5	F-measure, AUC		
					IND Logistic Trees			
					A NIN	Decell		
м23	I VO SMOTE	[137]	8	Binary	NR	Specificity		
1123	LIQSMOLE	[137]	0	Billal y	ND RE	G mean		
					SVM OLVO3	J-moan		
						Precision Recall		
M24	SOI CJ	[138]	20	Binary	C4.5	F-measure, AUC		
			• •		C4.5			
M25	ROSE	[139]	20	Binary	LR	AUC		

# TABLE 1. (Continued.) Summary of the methods used in this study. In this table, C4.5 is Decision Tree C4.5, LR is Logistic Regression, LDA is linear discriminate analysis, NB is naive bayes, RF is random forest and ANN is artificial neural network.

M26	SMOTE OUT	[140]	18	Binary	SVM	F-measure
M27	SMOTE Cosine	[140]	18	Binary	SVM	F-measure
W128	Selected SMOTE	[140]	18	Binary	5 V IVI	F-measure
M29	LN SMOTE	[141]	15	Binary	C4.5	G-mean
		[]		5	NB	Recall
					C4.5	
M30	MWMOTE	[88]	20	Binary	AdaBoost, KNN ANN	G-mean, AUC
M31	PDFOS	[142]	6	Binary	RBF	F-measure G-mean, AUC
M32	RWO sampling	[143]				
M33	NEATER	[144]	22	Binary	C4.5 RF. SVM	G-mean, AUC
M34	DEAGO	[145]	2	Binary	ANN	AUC
M35	Gazzah	[146]	2	Multi	SVM	True Negative Rate True Positive Rate
					C4.5	
M36	MCT	[147]	14	Binary	KNN, SVM NB	FN, FP
M37	SMOTE IPF	[148]	9	Binary	C4.5	AUC Presiden
						Recall
M38	KernelADASYN	[149]	7	Binary	C4.5	F-measure
						G-Mean
M39	MOT2LD	[150]	15	Binary	CART	G-mean
	-				-	F-measure
						Recall
M40	V SYNTH	[151]	6	Binary	LR	Specificity
				2	LDA	Accuracy
						FPR, FNR
					SVM KNN	Recall
M41	OUPS	[152]	45	Binary	LDA	Specificity
					LR	G-mean
M42	SMOTE D	[153]	66	Binary	C4.5	F-measure
3.6.42		[155]	10		KNN, SVM	
M43	SMOLE PSO	[154]	18	Multi	SVM	AUC and G-mean
M44	CURE SMOTE	[155]	12	Multi	CART	G-mean
					RF	AUC
M45	CE SMOTE	[156]	10	Binary	C4.5	F-measure
		[]		)		G-mean
M46	Edge Det SMOTE	[157]	9	Binary	SVM	F-measure G-mean
						accuracy
M47	CBSO	[158]	8	Binary	ANN C4.5	F-measure
			_		C4.J	G-mean
M48	ASMOBD	[129]	9	Binary	SVM	G-mean and AUC
						Precision Recall
M49	Assembled SMOTE	[159]	4	Binary	SVM	F-score
						Accuracy

M50	SDSMOTE	[160]	4	Binary	C4.5 AdaBoost Bagging	AUC F-measure
M51	DSMOTE	[161]	11	Binary	Naïve Bayes KNN, SVM	Accuracy Recall Precision F-measure
M52 M53	G SMOTE NT SMOTE	[162] [163]	4 3	Binary Binary	1NN and SVM SVM and C4.5	G-mean AUC Accuracy
M54	Lee	[164]	8	Binary	SVM	Precision Recall
M55	SMOTE PSOBAT	[165]	30	Binary	ANN C4.5	Kappa Accuracy AUC
M56	MDO	[166, 167]	20	Multi	C4.5, KNN RIPPER	G-mean Precision Recall
M57	Random SMOTE	[168]	10	Multi	KNN	F-measure G-mean Accuracy
M58	VIS RST	[169]	6	Binary	AdaBoost C4.5	True positive rate true negatives rate F-measure, and AUC
M59	GASMOTE	[170]	10	Binary	C4.5	F-measure, G-mean
M60	SMOTE FRST 2T	[171]	1	Binary	C4.5	AUC, FP, FN
M61	AND SMOTE	[172]	12	Binary	CART	AUC
				2	ANN	Recall
M62	NRAS	[173]	41	Binary	SVM, LDA	Specificity
					LR	G-mean
						Precision
M63	AMSCO	[174]	30	Binary	ANN	Recall
1105	AMBCO	[1/+]	50	Dinary		F-measure
						G-mean
M64	SSO	[175]	6	Binary	ANN	F-measure
		[]	-		I.D.	G-mean
M65	NDO sampling	[176]	1	Binary	LR Decision Tree C5 ANN, SVM	F-measure, Recall
M66	DSRBF	[177]	13	Multi	ANN	Accuracy
						Accuracy
M67	Gaussian SMOTE	[104]	1	Binary	SVM	Recall Specificity
M68	Supervised SMOTE	[178]	2	Binary	SVM	Recall Specificity MCC, AUC
M69	SN SMOTE	[179]	39	Binary	KNN, ANN C4.5	Accuracy Recall Specificity, AUC
M70	CCR	[180]	32	Binary	CART, KNN NB, SVM	F-measure G-mean, AUC
M71	ANS	[181]	14	Binary	ANN, KNN NB, SVM C4.5	F-measure, AUC
M72	cluster SMOTE	[182]	2	Binary	RIPPER	AUC

# TABLE 1. (Continued.) Summary of the methods used in this study. In this table, C4.5 is Decision Tree C4.5, LR is Logistic Regression, LDA is linear discriminate analysis, NB is naive bayes, RF is random forest and ANN is artificial neural network.



FIGURE 2. Flow diagram of the proposed validation system.

After that, we apply the oversampling method that needs to be validated on the remaining dataset in order to generate new examples, which is referred to as the synthetic subset. The hidden subset is then returned to the training set.

The generated examples in the synthetic subset are claimed to belong to the minority class by all oversampling methods. We compare the similarity between these examples (the synthetic subset) and all examples in the original training set before oversampling to see if these synthesized examples belong to the minority or the majority.

Figure 2 illustrates the proposed validation system.

In order to determine the degree of similarity, we need a similarity measure such as Euclidean distance (ED), Manhattan distance (MD), Hassanat distance (HD) [182], etc. In this paper, we opt for HD as being invariant to noise, outliers and data scale, since the nature of this metric prevents each feature from having a distance greater than one, regardless of the scale of the features in the targeted dataset. Furthermore, HD had been shown to outperform a wide range of machine learning similarity measures, including the most common ones like ED and MD [183]–[187].

HD can be expressed mathematically as in equation1.

$$D(p_i, q_i) = \begin{cases} 1 - \frac{1 + \min(p_i, q_i)}{1 + \max(p_i, q_i)}, & \min(p_i, q_i) \ge 0\\ 1 - \frac{1 + \min(p_i, q_i) + |\min(p_i, q_i)|}{1 + \max(p_i, q_i) + |\min(p_i, q_i)|}, & \min(p_i, q_i) < 0 \end{cases}$$
(1)

and for the total distance between two examples is

$$HD(\mathbf{p}, \mathbf{q}) = \sum_{i=1}^{N} D(p_i, q_i)$$
(2)

where p and q are feature vectors and N is the number of features in each vector.

It is worth mentioning that we are proposing a validation system, not an evaluation system, the similarity measure using HD is meant to find the number of examples taken from the synthetic subset that are similar to the minority as the core of our validation system. i.e. HD is calculated between the generated examples and the original examples. Those generated examples, which are more similar/nearest to the majority indicate the error of the oversampling method validated. This error is calculated according to equation 3.

$$Error = \frac{CM}{SS} \tag{3}$$

where CM is the number of synthetic examples that are more similar to majority examples using HD and SS is the total number of examples in the synthetic subset. The number of incorrectly synthesized examples, CM, and the total number of synthesized examples, SS, are used to determine the oversampling error, i.e., each example belonging to CM is closer to one of the instances belonging to the Majority class than any example belonging to the Minority class, despite the fact that it should be the other way around.

TABLE 2.	Description	of the	datasets	used in	this	study.
----------	-------------	--------	----------	---------	------	--------

ID	Name	No. Attributes	No. Classes	No. Minor	No. Major
1	Yeast4	10	2	51	1433
2	Yeast5	10	2	44	1440
3	Yeast6	10	2	35	1449
4	pima	8	2	268	500
5	car_good	6	2	69	1659
6	oil_spell	49	2	41	896
7	wisconsin	10	2	239	444
8	abalone-21_vs_8	8	2	14	567
9	Vehicle3	19	2	212	634

# **IV. DATASETS**

We employ nine real-life datasets to put our validation system to the test, such as Yeast4, Yeast5, and Yeast6, which are routinely used by many oversampling methods. On [188], all of the datasets are freely available. Table 2 contains information about these datasets.

Table 2 shows that the datasets have different minority and majority distributions, despite the fact that the number classes is the same. It is not necessary to address the problem with multi-class datasets to prove our counter claim, as most oversampling approaches only use binary class datasets, as shown in Table 1.

#### V. EXPERIMENTS AND RESULTS

In our experiments, we used all of the oversampling methods listed in Table 1 on each of the datasets listed in Table 2, after eliminating some majority examples at random. We employed varied numbers of hidden examples, namely 10%, 25%, and 50% of the majority examples of each dataset examined, to see the effect of the number of hidden examples on the validation process. Furthermore, each experiment is repeated five times, with the average of the results for each hidden ratio for each oversampling method on each dataset being reported. Table 3 shows the number of erroneous synthetic examples (NE), which are ones that are generated as minority examples but appear to be more comparable to majority examples, as the proposed validation system suggests. It also shows the number of synthetic examples (SE) generated by each oversampling method, in addition to the error rate (ER) which is calculated using Equation 3. All the result reported in Table 3 were obtained by hiding only 10% of the majority examples. Table 4 continues the results of Table 3 on the rest of the datasets.

The averages of five trials on each dataset for each approach are provided in Table 3 and Table 4. In addition, for each approach, the average error is calculated for the error rates the eight datasets mentioned in Tables 3 and 4. The last column in Table 4 shows the average rank of each method based on the eight used datasets; the lower the rank, the better the oversampling performance; for example, rank 1 shall be awarded to the method with the smallest error rate.







(c) 50%

FIGURE 3. Box plot of the average error rates of all oversampling methods on different datasets with varied hidden percentages.

The thorough examination of Tables 3 and 4 demonstrates that all oversampling methods result in errors in the synthesized examples. That is, they generate examples that are

# TABLE 3. Oversampling methods' validation results on the used datasets using 10% hidden percent.

Method         NE         SE         ER         NE         SE         ER         NE         SE         ER         NE         NA         ER           M1         463.2         1239         0.37         108         1252         0.09         294         1270         0.23         53         1425         0.00           M2         470         1235         0.38         117         1252         0.09         279         1270         0.22         46         1425         0.00           M3         414.2         1130.2         0.37         91         1222         0.07         266         1187         0.22         47         1406         0.0           M4         270.6         1239         0.38         597         1252         0.48         757         1270         0.60         368         1425         0.0           M6         568.8         1239         0.46         219         1252         0.17         534         1270         0.20         11         1425         0.0           M7         50         50         1.00         42         43         0.98         34         34         1.00         66         68         <			Yeast4			Yeast5		Yeast6			car_good			
MI         463.2         1239         0.37         108         1252         0.09         294         1270         0.23         53         1425         0.0           M2         470         1235         0.38         117         1252         0.09         279         1270         0.22         46         1425         0.0           M3         414.2         1130.2         0.37         91         1222         0.07         266         1187         0.22         47         1406         0.0           M4         270.6         1239         0.22         277         1252         0.42         391         1270         0.40         60         1425         0.0           M5         471         1239         0.38         597         1252         0.48         757         1270         0.60         688         1425         0.0           M7         50         50         1.00         42         43         0.98         34         34         1.00         66         68         0.99           M8         482.6         1239         0.39         145         1252         0.12         258         1270         0.20         11         1425 </th <th>Method</th> <th>NE</th> <th>SE</th> <th>ER</th> <th>NE</th> <th>SE</th> <th>ER</th> <th>NE</th> <th>SE</th> <th>ER</th> <th>NE</th> <th>NA</th> <th>ER</th>	Method	NE	SE	ER	NE	SE	ER	NE	SE	ER	NE	NA	ER	
M2       470       1235       0.38       117       1252       0.09       279       1270       0.22       46       1425       0.0         M3       414.2       1130.2       0.37       91       1222       0.07       266       1187       0.22       47       1406       0.0         M4       270.6       1239       0.22       277       1252       0.22       391       1270       0.60       368       1425       0.0         M5       471       1239       0.38       597       1252       0.48       757       1270       0.42       53       1425       0.0         M6       568.8       1239       0.46       219       1252       0.17       534       1270       0.42       53       1425       0.0         M7       50       50       1.00       42       43       0.98       34       34       1.00       66       68       0.99         M8       482.6       1239       0.39       145       1252       0.12       258       1270       0.20       11       1425       0.0         M10       53       59       0.90       9       11       0.82 <th>M1</th> <th>463.2</th> <th>1239</th> <th>0.37</th> <th>108</th> <th>1252</th> <th>0.09</th> <th>294</th> <th>1270</th> <th>0.23</th> <th>53</th> <th>1425</th> <th>0.04</th>	M1	463.2	1239	0.37	108	1252	0.09	294	1270	0.23	53	1425	0.04	
M3       414.2       1130.2       0.37       91       1222       0.07       266       1187       0.22       47       1406       0.0         M4       270.6       1239       0.22       277       1252       0.22       391       1270       0.31       60       1425       0.0         M5       471       1239       0.38       597       1252       0.48       757       1270       0.60       368       1425       0.0         M6       568.8       1239       0.46       219       1252       0.17       534       1270       0.42       53       1425       0.0         M7       50       50       1.00       42       43       0.98       34       34       1.00       66       68       0.9         M8       482.6       1239       0.39       145       1252       0.12       258       1270       0.20       11       1425       0.0         M10       53       59       0.90       9       11       0.82       17       17       1.00       36       204       0.1         M11       523.4       1239       0.42       165       1252       0.13	M2	470	1235	0.38	117	1252	0.09	279	1270	0.22	46	1425	0.03	
M4       270.6       1239       0.22       277       1252       0.22       391       1270       0.31       60       1425       0.0         M5       471       1239       0.38       597       1252       0.48       757       1270       0.60       368       1425       0.2         M6       568.8       1239       0.46       219       1252       0.17       534       1270       0.42       53       1425       0.0         M7       50       50       1.00       42       43       0.98       34       34       1.00       66       68       0.99         M8       482.6       1239       0.39       145       1252       0.12       258       1270       0.20       11       1425       0.0         M9       765       1224       0.63       204       1232       0.17       744       1260       0.19       873       1449       0.6         M10       53       59       0.90       9       11       0.82       17       17       1.00       36       204       0.11         M11       523.4       1239       0.42       165       1252       0.13	M3	414.2	1130.2	0.37	91	1222	0.07	266	1187	0.22	47	1406	0.03	
M5       471       1239       0.38       597       1252       0.48       757       1270       0.60       368       1425       0.2         M6       568.8       1239       0.46       219       1252       0.17       534       1270       0.42       53       1425       0.0         M7       50       50       1.00       42       43       0.98       34       120       0.42       53       1425       0.0         M8       482.6       1239       0.39       145       1252       0.12       258       1270       0.20       11       1425       0.0         M9       765       1224       0.63       204       1232       0.17       244       1260       0.19       873       1449       0.60         M10       53       59       0.90       9       11       0.82       17       17       1.00       36       204       0.13         M11       523.4       1239       0.42       165       1252       0.13       372       1270       0.24       884       1425       0.6         M14       425.8       771.4       0.55       -       -       -	M4	270.6	1239	0.22	277	1252	0.22	391	1270	0.31	60	1425	0.04	
M6       568.8       1239       0.46       219       1252       0.17       534       1270       0.42       53       1425       0.0         M7       50       50       1.00       42       43       0.98       34       34       1.00       66       68       0.99         M8       482.6       1239       0.39       145       1252       0.12       258       1270       0.20       11       1425       0.0         M9       765       1224       0.63       204       1232       0.17       244       1260       0.19       873       1449       0.60         M10       53       59       0.90       9       11       0.82       17       17       1.00       36       204       0.13         M11       523.4       1239       0.42       165       1252       0.13       372       1270       0.24       884       1425       0.13         M12       109.8       125.2       0.88       -       -       -       250       648       0.39       237       992       0.22         M15       479       1239       0.39       116       1252       0.09	M5	471	1239	0.38	597	1252	0.48	757	1270	0.60	368	1425	0.26	
M7         50         50         1.00         42         43         0.98         34         34         1.00         66         68         0.99           M8         482.6         1239         0.39         145         1252         0.12         258         1270         0.20         11         1425         0.0           M9         765         1224         0.63         204         1232         0.17         244         1260         0.19         873         1449         0.66           M10         53         59         0.90         9         11         0.82         17         17         1.00         36         204         0.13           M11         523.4         1239         0.42         165         1252         0.13         372         1270         0.29         190         1425         0.13           M11         523.4         1239         0.42         165         1252         0.21         308         1270         0.24         884         1425         0.66           M13         363         1239         0.39         116         1252         0.09         357         1270         0.28         57         1425	M6	568.8	1239	0.46	219	1252	0.17	534	1270	0.42	53	1425	0.04	
M8       482.6       1239       0.39       145       1252       0.12       258       1270       0.20       11       1425       0.00         M9       765       1224       0.63       204       1232       0.17       244       1260       0.19       873       1449       0.66         M10       53       59       0.90       9       11       0.82       17       17       1.00       36       204       0.13         M11       523.4       1239       0.42       165       1252       0.13       372       1270       0.29       190       1425       0.13         M11       523.4       1239       0.29       261       1252       0.21       308       1270       0.24       884       1425       0.66         M14       425.8       771.4       0.55       -       -       -       250       648       0.39       237       992       0.22         M15       479       1239       0.39       116       1252       0.09       357       1270       0.28       57       1425       0.0         M16       285       286       1.00       289       292	M7	50	50	1.00	42	43	0.98	34	34	1.00	66	68	0.97	
M9       765       1224       0.63       204       1232       0.17       244       1260       0.19       873       1449       0.66         M10       53       59       0.90       9       11       0.82       17       17       1.00       36       204       0.13         M11       523.4       1239       0.42       165       1252       0.13       372       1270       0.29       190       1425       0.13         M12       109.8       125.2       0.88       -       -       -       55       55       1.00       -       -       -       -       -       -       -       55       55       1.00       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -	M8	482.6	1239	0.39	145	1252	0.12	258	1270	0.20	11	1425	0.01	
M10       53       59       0.90       9       11       0.82       17       17       1.00       36       204       0.13         M11       523.4       1239       0.42       165       1252       0.13       372       1270       0.29       190       1425       0.13         M12       109.8       125.2       0.88       -       -       -       55       55       1.00       -       -       -       -         M13       363       1239       0.29       261       1252       0.21       308       1270       0.24       884       1425       0.6         M14       425.8       771.4       0.55       -       -       -       250       648       0.39       237       992       0.2         M16       285       286       1.00       289       292       0.99       298       300       0.99       304       306       0.99         M17       309.8       1239       0.25       45       1252       0.04       79       1270       0.06       23       1425       0.00         M18       478.8       1239       0.39       103       1252       0	M9	765	1224	0.63	204	1232	0.17	244	1260	0.19	873	1449	0.60	
M11       523.4       1239       0.42       165       1252       0.13       372       1270       0.29       190       1425       0.11         M12       109.8       125.2       0.88       -       -       -       55       55       1.00       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       1425       0.00       111       111       111       111	M10	53	59	0.90	9	11	0.82	17	17	1.00	36	204	0.18	
M12       109.8       125.2       0.88       -       -       -       55       55       1.00       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -	MII M12	523.4	1239	0.42	165	1252	0.13	372	1270	0.29	190	1425	0.13	
M13       365       1239       0.29       261       1252       0.21       308       1270       0.24       884       1425       0.6         M14       425.8       771.4       0.55       -       -       -       250       648       0.39       237       992       0.2         M15       479       1239       0.39       116       1252       0.09       357       1270       0.28       57       1425       0.0         M16       285       286       1.00       289       292       0.99       298       300       0.99       304       306       0.99         M17       309.8       1239       0.25       45       1252       0.04       79       1270       0.06       23       1425       0.0         M18       478.8       1239       0.39       103       1252       0.08       269       1270       0.10       64       1425       0.0         M19       329       1239       0.27       26       1252       0.02       124       1270       0.10       64       1425       0.0         M20       938.8       2478       0.38       0       43       0.	M12 M12	109.8	125.2	0.88	-	-	-	<b>33</b>	33 1270	1.00	-	-	-	
M14       425.8       771.4       0.55       -       -       250       648       0.59       257       992       0.22         M15       479       1239       0.39       116       1252       0.09       357       1270       0.28       57       1425       0.0         M16       285       286       1.00       289       292       0.99       298       300       0.99       304       306       0.99         M17       309.8       1239       0.25       45       1252       0.04       79       1270       0.06       23       1425       0.0         M18       478.8       1239       0.39       103       1252       0.08       269       1270       0.21       59       1425       0.0         M19       329       1239       0.27       26       1252       0.02       124       1270       0.10       64       1425       0.0         M20       938.8       2478       0.38       0       43       0.00       575       2540       0.23       0       359       0.0         M21       729.4       1239       0.59       221       1252       0.18 <td< th=""><th>M13 M14</th><th>303</th><th>1239</th><th>0.29</th><th>261</th><th>1252</th><th>0.21</th><th>308</th><th>1270</th><th>0.24</th><th>884</th><th>1425</th><th>0.62</th></td<>	M13 M14	303	1239	0.29	261	1252	0.21	308	1270	0.24	884	1425	0.62	
M15       479       1239       0.39       116       1232       0.09       337       1270       0.28       37       1425       0.00         M16       285       286       1.00       289       292       0.99       298       300       0.99       304       306       0.99         M17       309.8       1239       0.25       45       1252       0.04       79       1270       0.06       23       1425       0.00         M18       478.8       1239       0.39       103       1252       0.08       269       1270       0.21       59       1425       0.00         M19       329       1239       0.27       26       1252       0.02       124       1270       0.10       64       1425       0.00         M20       938.8       2478       0.38       0       43       0.00       575       2540       0.23       0       359       0.00         M21       729.4       1239       0.59       221       1252       0.18       385       1270       0.30       513       1425       0.30         M22       282.6       1239       0.63       330       1252 <th>M14 M15</th> <th>425.8</th> <th>//1.4</th> <th>0.55</th> <th>-</th> <th>-</th> <th>-</th> <th>250</th> <th>048</th> <th>0.39</th> <th>237</th> <th>992</th> <th>0.24</th>	M14 M15	425.8	//1.4	0.55	-	-	-	250	048	0.39	237	992	0.24	
M16       283       286       1.00       289       292       0.99       298       300       0.99       304       306       0.99         M17       309.8       1239       0.25       45       1252       0.04       79       1270       0.06       23       1425       0.0         M18       478.8       1239       0.39       103       1252       0.08       269       1270       0.21       59       1425       0.0         M19       329       1239       0.27       26       1252       0.02       124       1270       0.10       64       1425       0.0         M20       938.8       2478       0.38       0       43       0.00       575       2540       0.23       0       359       0.0         M21       729.4       1239       0.59       221       1252       0.18       385       1270       0.30       513       1425       0.30         M22       282.6       1239       0.63       330       1252       0.26       621       1270       0.32       54       1425       0.0         M23       775.8       1239       0.63       330       1252	M15 M16	4/9	1239	0.39	110	1252	0.09	202	1270	0.28	37 204	1423	0.04	
M17       309.8       1239       0.23       43       1232       0.04       79       1270       0.06       23       1423       0.0         M18       478.8       1239       0.39       103       1252       0.08       269       1270       0.21       59       1425       0.0         M19       329       1239       0.27       26       1252       0.02       124       1270       0.10       64       1425       0.0         M20       938.8       2478       0.38       0       43       0.00       575       2540       0.23       0       359       0.0         M21       729.4       1239       0.59       221       1252       0.18       385       1270       0.30       513       1425       0.33         M22       282.6       1239       0.63       330       1252       0.26       621       1270       0.32       54       1425       0.0         M23       775.8       1239       0.63       330       1252       0.26       621       1270       0.33       48       1425       0.0         M24       52       1239       0.04       120       1252	M17	283	280	1.00	289 45	1252	0.99	298 70	300 1270	0.99	304 22	300	0.99	
M16       478.8       1239       0.39       103       1232       0.08       209       1270       0.21       39       1423       0.00         M19       329       1239       0.27       26       1252       0.02       124       1270       0.10       64       1425       0.00         M20       938.8       2478       0.38       0       43       0.00       575       2540       0.23       0       359       0.00         M21       729.4       1239       0.59       221       1252       0.18       385       1270       0.30       513       1425       0.30         M22       282.6       1239       0.23       -       -       -       406       1270       0.32       54       1425       0.00         M23       775.8       1239       0.63       330       1252       0.26       621       1270       0.49       290       1425       0.24         M24       52       1239       0.04       120       1252       0.10       41       1270       0.03       48       1425       0.0         M25       867       1239       0.36       76       1252	M117 M18	309.8 178.8	1239	0.23	43	1252	0.04	79 260	1270	0.00	25 50	1425	0.02	
M15       325       1239       0.27       26       1252       0.02       124       1270       0.10       04       1425       0.00         M20       938.8       2478       0.38       0       43       0.00       575       2540       0.23       0       359       0.00         M21       729.4       1239       0.59       221       1252       0.18       385       1270       0.30       513       1425       0.33         M22       282.6       1239       0.59       221       1252       0.18       385       1270       0.30       513       1425       0.33         M22       282.6       1239       0.63       330       1252       0.26       621       1270       0.32       54       1425       0.04         M23       775.8       1239       0.63       330       1252       0.26       621       1270       0.32       54       1425       0.04         M24       52       1239       0.63       330       1252       0.10       41       1270       0.33       48       1425       0.03         M26       442       1239       0.36       76       1252<	M10	4/0.0	1239	0.39	105	1252	0.08	124	1270	0.21	59 64	1425	0.04	
M20       J38.3       L478       0.38       0       43       0.00       J73       L340       0.23       0       J35       0.00         M21       729.4       1239       0.59       221       1252       0.18       385       1270       0.30       513       1425       0.30         M22       282.6       1239       0.23       -       -       -       406       1270       0.32       54       1425       0.30         M23       775.8       1239       0.63       330       1252       0.26       621       1270       0.32       54       1425       0.20         M24       52       1239       0.63       330       1252       0.26       621       1270       0.32       54       1425       0.20         M24       52       1239       0.63       330       1252       0.10       41       1270       0.03       48       1425       0.00         M25       867       1239       0.36       76       1252       0.06       246       1270       0.19       41       1425       0.00         M26       442       1239       0.38       86       1252       <	M20	038.8	2478	0.27	20	1252	0.02	575	2540	0.10	04	350	0.04	
M21       1257       1257       1257       1252       0.16       565       1270       0.56       515       1425       0.57         M22       282.6       1239       0.23       -       -       -       406       1270       0.32       54       1425       0.04         M23       775.8       1239       0.63       330       1252       0.26       621       1270       0.49       290       1425       0.2         M24       52       1239       0.04       120       1252       0.10       41       1270       0.03       48       1425       0.0         M25       867       1239       0.70       456       1252       0.36       707       1270       0.56       744       1425       0.57         M26       442       1239       0.36       76       1252       0.06       246       1270       0.19       41       1425       0.0         M27       475.4       1239       0.38       86       1252       0.07       265       1270       0.21       60       1425       0.0         M28       470.2       1239       0.38       121       1252       0.10	M21	729.4	1239	0.50	221	1252	0.00	385	1270	0.25	513	1425	0.00	
M22       262.6       1239       0.23       1252       126       1270       0.32       54       1125       0.60         M23       775.8       1239       0.63       330       1252       0.26       621       1270       0.49       290       1425       0.24         M24       52       1239       0.04       120       1252       0.10       41       1270       0.03       48       1425       0.0         M25       867       1239       0.70       456       1252       0.36       707       1270       0.56       744       1425       0.55         M26       442       1239       0.36       76       1252       0.06       246       1270       0.19       41       1425       0.0         M27       475.4       1239       0.38       86       1252       0.07       265       1270       0.21       60       1425       0.0         M28       470.2       1239       0.38       121       1252       0.10       303       1270       0.24       49       1425       0.0         M29       413.8       1239       0.33       167       1252       0.13       27	M22	722.4 282.6	1239	0.32	-	-	-	406	1270	0.30	54	1425	0.04	
M24       52       1239       0.04       120       1252       0.10       41       1270       0.03       48       1425       0.0         M24       52       1239       0.04       120       1252       0.10       41       1270       0.03       48       1425       0.0         M25       867       1239       0.70       456       1252       0.36       707       1270       0.56       744       1425       0.5         M26       442       1239       0.36       76       1252       0.06       246       1270       0.19       41       1425       0.0         M27       475.4       1239       0.38       86       1252       0.07       265       1270       0.21       60       1425       0.0         M28       470.2       1239       0.38       121       1252       0.10       303       1270       0.24       49       1425       0.0         M29       413.8       1239       0.33       167       1252       0.13       272       1270       0.21       163       1425       0.1	M23	775.8	1239	0.63	330	1252	0.26	621	1270	0.32 0.49	290	1425	0.20	
M25       867       1239       0.70       456       1252       0.36       707       1270       0.56       744       1425       0.55         M26       442       1239       0.36       76       1252       0.06       246       1270       0.19       41       1425       0.55         M26       442       1239       0.36       76       1252       0.06       246       1270       0.19       41       1425       0.00         M27       475.4       1239       0.38       86       1252       0.07       265       1270       0.21       60       1425       0.00         M28       470.2       1239       0.38       121       1252       0.10       303       1270       0.24       49       1425       0.00         M29       413.8       1239       0.33       167       1252       0.13       272       1270       0.21       163       1425       0.11	M24	52	1239	0.04	120	1252	0.10	41	1270	0.03	48	1425	0.03	
M2644212390.367612520.0624612700.194114250.06M27475.412390.388612520.0726512700.216014250.06M28470.212390.3812112520.1030312700.244914250.06M29413.812390.3316712520.1327212700.2116314250.1	M25	867	1239	0.70	456	1252	0.36	707	1270	0.56	744	1425	0.52	
M27         475.4         1239         0.38         86         1252         0.07         265         1270         0.21         60         1425         0.04           M28         470.2         1239         0.38         121         1252         0.10         303         1270         0.24         49         1425         0.04           M29         413.8         1239         0.33         167         1252         0.13         272         1270         0.21         163         1425         0.11	M26	442	1239	0.36	76	1252	0.06	246	1270	0.19	41	1425	0.03	
M28         470.2         1239         0.38         121         1252         0.10         303         1270         0.24         49         1425         0.0           M29         413.8         1239         0.33         167         1252         0.13         272         1270         0.21         163         1425         0.1	M27	475.4	1239	0.38	86	1252	0.07	265	1270	0.21	60	1425	0.04	
<b>M29</b> 413.8 1239 0.33 167 1252 0.13 272 1270 0.21 163 1425 0.1	M28	470.2	1239	0.38	121	1252	0.10	303	1270	0.24	49	1425	0.03	
	M29	413.8	1239	0.33	167	1252	0.13	272	1270	0.21	163	1425	0.11	
<b>M30</b> 644.8 1239 0.52 223 1252 0.18 369 1270 0.29 81 1425 0.00	M30	644.8	1239	0.52	223	1252	0.18	369	1270	0.29	81	1425	0.06	
<b>M31</b> 872.2 1239 0.70 395 1252 0.32 599 1270 0.47 791 1425 0.50	M31	872.2	1239	0.70	395	1252	0.32	599	1270	0.47	791	1425	0.56	
<b>M32</b> 927.8 1239 0.75 698 1252 0.56 987 1270 0.78 467 1425 0.33	M32	927.8	1239	0.75	698	1252	0.56	987	1270	0.78	467	1425	0.33	
<b>M33</b> 1041.6 2478 0.42 315 2504 0.13 813 2540 0.32 96 2850 0.0	M33	1041.6	2478	0.42	315	2504	0.13	813	2540	0.32	96	2850	0.03	
<b>M34</b> 1236 1239 1.00 523 1252 0.42 36 1270 0.03 1425 1425 1.00	M34	1236	1239	1.00	523	1252	0.42	36	1270	0.03	1425	1425	1.00	
<b>M35</b> 504 791 0.64 148 807 0.18 159 841 0.19 369 668 0.5	M35	504	791	0.64	148	807	0.18	159	841	0.19	369	668	0.55	
<b>M36</b> 602 1239 0.49 191 1252 0.15 414 1270 0.33 248 1425 0.1	M36	602	1239	0.49	191	1252	0.15	414	1270	0.33	248	1425	0.17	
<b>M37</b> 518 1239 0.42 110 1252 0.09 292 1270 0.23 54 1425 0.0	M37	518	1239	0.42	110	1252	0.09	292	1270	0.23	54	1425	0.04	
<b>M38</b> 1200 1239 0.97 855 1252 0.68 1264 1270 1.00 1283 1425 0.90	M38	1200	1239	0.97	855	1252	0.68	1264	1270	1.00	1283	1425	0.90	
<b>M39</b> 307 1226 0.25 129 1248 0.10 93 1262 0.07 467 1409 0.33	M39	307	1226	0.25	129	1248	0.10	93	1262	0.07	467	1409	0.33	
<b>M40</b> 1199 1239 0.97 639 1252 0.51 1262 1270 0.99	M40	1199	1239	0.97	639	1252	0.51	1262	1270	0.99	-	-	-	
<b>M41</b> 938 1264 0.74 547 1268 0.43 711 1272 0.56 713 1430 0.59	M41	938	1264	0.74	547	1268	0.43	711	1272	0.56	713	1430	0.50	
<b>M42</b> 1239 1239 1.00 1010 1251 0.81 12/1 12/1 1.00 1424 1424 1.00 <b>M42</b> 78 152 0.51 22 122 0.24 47 105 0.45 72 207 0.2	M42	1239	1239	1.00	1010	1251	0.81	12/1	12/1	1.00	1424	1424	1.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	IV145 M44	18	155	0.51	32 199	132	0.24	47	105	0.45	12	207	0.35	
<b>M44</b> 288 1239 0.25 188 1232 0.15 89 1270 0.07 14 1425 0.0 <b>M45</b> 710 1230 0.57 72 1252 0.06 130 1270 0.11 70 1425 0.0	IV144 M45	200 710	1239	0.23	100	1252	0.15	89 120	1270	0.07	14 70	1425	0.01	
<b>M45</b> 710 1239 $0.57$ 72 1252 $0.00$ 139 1270 $0.11$ 70 1425 $0.0$	IV145 M46	/10	1239	0.37	12	1252	0.00	139	1270	0.11	/U 69	1425	0.05	
<b>M47</b> 753 1230 0.61 363 1252 0.00 623 1270 0.50 120 1425 0.00 $\mathbf{M47}$	1914U M47	440 752	1239	0.30	0J 362	1252	0.07	∠10 633	1270	0.22	120	1423	0.03	
<b>M48</b> $302$ 1239 0.01 303 1232 0.27 0.35 1270 0.30 120 1423 0.0 <b>M48</b> 302 1230 0.24 35 1252 0.03 32 1270 0.03 22 1425 0.0	M48	302	1239	0.01	303	1252	0.29	32	1270	0.00	22	1425	0.00	
<b>M49</b> $476$ 1239 0.38 123 1252 0.03 52 1270 0.05 25 1425 0.0	M49	476	1239	0.24	123	1252	0.05	308	1270	0.05	23 49	1425	0.02	
<b>M50</b> 451 1239 0.36 85 1252 0.07 256 1270 0.24 49 1425 0.0	M50	451	1239	0.36	85	1252	0.10	256	1270	0.24	49	1425	0.03	
$\mathbf{M51}  14  1239  0.01  2  1252  0.07  230  1270  0.20  49  1423  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01  0.01 $	M51	14	1239	0.01	2	1252	0.07	0	1270	0.00	0	1425	0.00	

M52	524	1220	0.42	85	1252	0.07	206	1270	0.22	15	1425	0.01
N152	554	1239	0.45	05	1252	0.07	290	1270	0.23	15	1425	0.01
M53	413	1239	0.33	18	1252	0.01	285	1270	0.22	12	1425	0.01
M54	452	1239	0.36	103	1252	0.08	320	1270	0.25	55	1425	0.04
M55	225	592	0.38	76	869	0.09	169	724	0.23	26	979	0.03
M56	592	1239	0.48	453	1252	0.36	441	1270	0.35	211	1425	0.15
M57	470	1239	0.38	116	1252	0.09	304	1270	0.24	48	1425	0.03
M58	232	411	0.56	69	224	0.31	95	148	0.64	85	346	0.25
M59	64	165	0.39	12	133	0.09	18	116	0.16	5	234	0.02
M60	552	1482	0.37	115	1500	0.08	279	1270	0.22	59	1425	0.04
M61	212	1239	0.17	73	1252	0.06	128	1270	0.10	28	1425	0.02
M62	140	1239	0.11	84	1252	0.07	28	1270	0.02	241	1425	0.17
M63	275	805	0.34	97	1101	0.09	182	789	0.23	282	5700	0.05
M64	579	1235	0.47	236	1250	0.19	257	1270	0.20	1373	1425	0.96
M65	558	1239	0.45	143	1252	0.11	307	1270	0.24	413	1425	0.29
M66	521	1239	0.42	101	1252	0.08	275	1270	0.22	58	1425	0.04
M67	918	1239	0.74	727	1252	0.58	1025	1270	0.81	1260	1425	0.88
M68	365	1239	0.29	140	1252	0.11	100	1270	0.08	238	1425	0.17
M69	496	1239	0.40	104	1252	0.08	326	1270	0.26	67	1425	0.05
M70	1048	1240	0.85	898	1253	0.72	1076	1270	0.85	851	1449	0.59
M71	381	1239	0.31	-	-	-	105	1270	0.08	18	1425	0.01
M72	411	1239	0.33	46	1252	0.04	498	1270	0.39	22	1425	0.02

TABLE 3. (Continued.) Oversampling methods' validation results on the used datasets using 10% hidden percent.



FIGURE 4. Methods ranking based on their average error rates on the datasets mentioned in Tables 3 and 4.

meant to be minority, yet are similar to the majority or fall within the majority class's decision boundary. Despite the fact that all methods generate such examples, the quantity of fake examples generated differs from one method to another. On the Yeast4 dataset, for example, the oversampling method (M51) generates 14 incorrect examples, whereas other methods, such as M70, generate more than 1K incorrect examples. That is why M51 is ranked first, whereas M70 is ranked much higher. Similar findings were achieved when 25% and 50% of the majority examples were used as hidden examples, thus there is no need to include them in tables; however, we show them in Figure 3.

The average error rate of all oversampling methods increases somewhat as the hidden percent increases, as seen

# TABLE 4. Oversampling methods' validation results on the used datasets using 10% hidden percent.

		oil		W	viscons	in	abal	one-21	_vs_8		pima			
Method	NE	NA	ER	NE	NA	ER	NE	NA	ER	NE	NA	ER	Avg. ER	Rank
M1	601	766	0.78	4	161	0.02	250	497	0.50	40	182	0.22	0.28	26
M2	512	668	0.77	6	157	0.04	239	493	0.48	34	120	0.28	0.29	32
M3	446	584	0.76	5	139	0.04	230	478	0.48	-	-	-	0.28	27
M4	443	766	0.58	7	161	0.04	164	497	0.33	57	182	0.31	0.26	14
M5	437	766	0.57	59	161	0.37	250	497	0.50	63	182	0.35	0.44	54
M6	632	766	0.83	16	161	0.10	277	497	0.56	57	182	0.31	0.36	45
M7	40	40	1.00	235	238	0.99	13	13	1.00	247	267	0.93	0.98	71
<b>M8</b>	578	766	0.75	3	161	0.02	271	497	0.55	47	182	0.26	0.29	31
M9	758	779	0.97	12	239	0.05	326	504	0.65	201	268	0.75	0.50	57
M10	66	71	0.93	23	35	0.66	24	26	0.92	26	44	0.59	0.75	67
M11	591	766	0.77	3	161	0.02	238	497	0.48	48	182	0.26	0.31	41
M12	79	79	1.00	16	23	0.70	-	-	-	110	127	0.87	0.89	70
M13	449	766	0.59	4	161	0.02	164	497	0.33	43	182	0.24	0.32	42
M14	557	714	0.78	8	103	0.08	209	293	0.71	35	164	0.21	0.42	52
M15	578	766	0.75	3	161	0.02	252	497	0.51	48	182	0.26	0.29	38
M16	199	199	1.00	23	23	1.00	116	116	1.00	22	24	0.92	0.99	72
M17	513	766	0.67	0	161	0.00	144	497	0.29	25	182	0.14	0.18	5
M18	592	766	0.77	1	161	0.01	239	497	0.48	49	182	0.27	0.28	24
M19	568	766	0.74	6	161	0.04	155	497	0.31	40	182	0.22	0.22	8
M20	116	160	0.73	2	263	0.01	5	160	0.03	0	3	0.00	0.17	4
M21	673	766	0.88	18	161	0.11	269	497	0.54	68	182	0.37	0.42	50
M22	489	766	0.64	13	17	0.76	153	497	0.31	104	132	0.79	0.44	55
M23	631	766	0.82	16	161	0.10	321	497	0.65	47	182	0.26	0.43	53
M24	103	766	0.13	11	161	0.07	19	497	0.04	40	182	0.22	0.08	1
M25	734	766	0.96	41	161	0.25	284	497	0.57	93	182	0.51	0.55	61
M26	582	766	0.76	2	161	0.01	252	497	0.51	37	182	0.20	0.27	17
M27	585	766	0.76	3	161	0.02	263	497	0.53	53	182	0.29	0.29	33
M28	585	766	0.76	8	161	0.05	242	497	0.49	44	182	0.24	0.29	30
M29	458	766	0.60	5	161	0.03	121	497	0.24	49	182	0.27	0.24	11
M30	636	766	0.83	14	161	0.09	272	497	0.55	75	182	0.41	0.37	46
M31	730	766	0.95	57	161	0.35	336	497	0.68	94	182	0.52	0.57	62 50
M32	559	766	0.73	8	161	0.05	322	497	0.65	51	182	0.28	0.51	58
M33	1238	1532	0.81	9	322	0.03	502	994	0.51	98	364	0.27	0.31	40
M34	733	766	0.96	0	161	0.00	497	497	1.00	136	182	0.75	0.64	65
M35	/06	724	0.98	-	-	-	152	235	0.65	-	-	-	0.53	60
M36 M27	564	/66	0.74	11 ~	161	0.07	291	497	0.59	33	182	0.29	0.35	44
M3/	582	/66	0.76	2	161	0.03	236	497	0.47	40	182	0.22	0.28	25
N138 M20	-	- 749	-	4	101	0.02	389	497	0.78	0	182	0.00	0.62	04 7
N139 M40	554 614	748	0.47	14 74	159	0.09	42	491	0.09	39	100	0.25	0.21	1
IVI4U M 4 1	014 701	/00 769	0.80	/4	101	0.46	443 201	497 510	0.90	121	182	0.00	0.70	00 50
N141 M42	701	763	0.91	0 40	162	0.00	391 407	310 407	0.77	30 71	103	0.31	0.35	59 60
N142 M42	494	/05	0.03	40 70	103	0.23	497	497	1.00	/1	192	0.57	0.70	09 56
N145 M44	107	125	0.87	16	120	0.38	10	42	0.50	20	120	0.01	0.30	50 16
1V144 M/45	000 524	700	0.90	10	101	0.10	210 200	491 407	0.43	20 10	102	0.21	0.20	10 20
IV143 M46	505	700	0.08	Q Q	101	0.04	209 วาว	471 407	0.42	40 44	102 192	0.20	0.27	20 22
IV140 M 47	373 616	700	0.78	0 16	101	0.05	222	497 107	0.43	44 71	182	0.24	0.28	22 40
1V147 M49	040	700	0.04	20	101	0.10	240 125	471 107	0.40	71 22	102	0.39	0.41	47 )
1V140 M40	- 508	- 766	- 0.79	32 2	101 161	0.20	123 242	471 107	0.23	22 21	102	0.12	0.15	4 22
M50	590 604	700	0.70	5 11	101 161	0.02	243 246	471 107	0.49	24 22	102	0.19	0.20	25 21
M51	765	766	1.00	11 0	101 161	0.07	240 256	+71 107	0.49	55 25	102	0.10	0.20	41 10
14131	105	/00	1.00	U	101	0.00	550	47/	0.12	<i>2</i> 3	102	0.14	0.23	10

M52	572	766	0.75	5	161	0.03	287	497	0.58	46	182	0.25	0.29	39
M53	542	766	0.71	0	161	0.00	129	497	0.26	43	182	0.24	0.22	9
M54	608	766	0.79	4	161	0.02	257	497	0.52	39	182	0.21	0.29	28
M55	514	688	0.75	2	72	0.03	71	129	0.55	75	319	0.24	0.29	29
M56	719	766	0.94	82	161	0.51	88	497	0.18	74	182	0.41	0.42	51
M57	597	766	0.78	5	161	0.03	259	497	0.52	44	182	0.24	0.29	35
M58	123	151	0.81	5	148	0.03	3	26	0.12	46	111	0.41	0.39	48
M59	125	162	0.77	13	639	0.02	27	42	0.64	179	750	0.24	0.29	37
M60	650	805	0.81	12	168	0.07	281	571	0.49	53	216	0.25	0.29	36
M61	423	766	0.55	5	161	0.03	55	497	0.11	37	182	0.20	0.16	3
M62	546	766	0.71	10	161	0.06	119	497	0.24	31	182	0.17	0.19	6
M63	2492	3064	0.81	9	491	0.02	-	-	-	148	678	0.22	0.25	13
M64	-	-	-	14	160	0.09	256	495	0.52	54	180	0.30	0.39	47
M65	535	766	0.70	13	161	0.08	247	497	0.50	46	182	0.25	0.33	43
M66	618	766	0.81	9	161	0.06	225	497	0.45	44	182	0.24	0.29	34
M67	739	766	0.96	60	161	0.37	315	497	0.63	92	182	0.51	0.69	66
M68	604	766	0.79	22	161	0.14	109	497	0.22	68	182	0.37	0.27	19
M69	506	766	0.66	4	161	0.02	206	497	0.41	32	182	0.18	0.26	15
M70	570	779	0.73	14	239	0.06	389	497	0.78	74	268	0.28	0.61	63
M71	624	766	0.81	6	161	0.04	24	497	0.05	83	182	0.46	0.25	12
M72	511	766	0.67	6	161	0.04	243	497	0.49	35	182	0.19	0.27	18

TABLE 4. (Continued.) Oversampling methods' validation results on the used datasets using 10% hidden percent.

in Figure 3. This is logical since when oversampling methods synthesize their minority examples, they become unaware of some majority examples; in fact, we expected a significant error rise as the size of the hidden subset grew larger. In terms of the effect of the dataset on the average oversampling error, we can observe in the same figure that some datasets, such as (Yeast5), are easier to be oversampled than others, such as (Yeast6) and (Yeast4). However, the difference is not substantial, and more importantly, as the Box plots show, the standard deviation of the error rates produced by all oversampling methods on each dataset is extremely high.

In order to compare oversampling methods, we ranked them according to their average error across eight datasets. The average ranks of the methods are plotted against the average errors they produced on all used datasets as shown in Figure 4.

Despite the fact that all of the methods discussed generate false examples, Figure 4 indicates that certain methods do better than others in avoiding the formation of false examples. As a result, if oversampling is unavoidable, the method's reliability should be verified using a validation tools such as ours. Methods like M24, for example, have error rates close to 0%, whereas others like M7 and M16 have error rates near to 99%.

As a result, all Oversampling methods validated produce misleading examples, regardless of the hidden percentage or dataset used. Figure 5 visualizes the Oversampling results on eight datasets using M1, displaying various sorts of examples, including hidden, minority, majority, and synthesized examples while hiding 10% of the majority examples. For the sake of illustration, we limited the data to only two features. As seen in Figure 5, many synthetic examples are created on the basis of or near hidden examples, producing almost identical feature values. Even in higher dimensional feature space, such a situation has the potential to occur. The common mistake that all oversampling methods make is to feed such data to a classifier, assuming that all of the examples are realistic and labeled based on reality. The classifier has no other knowledge and learns based on the false assumption, which produces excellent results in labs but unexpected behavior in real-world scenarios.

The results shown thus far do not necessarily imply that incorrect example synthesis occurs just when the majority examples are hidden from the oversampling method. Even though the majority examples are completely visible to the methods, some methods generate false examples. The published findings of all of the oversampling methods demonstrate this, as none of them claimed to be an accurate method with no errors.

We validated some of the best performers on a ninth machine learning dataset, Vehicle3, because some oversampling approaches passed our validation test by presenting a relatively small number of unrealistic examples, and to further support our counterclaim against the validity of the oversampling approach in general. The validation results some of the good performers are shown in Table 5.

As can be seen in Table 5, when we changed the dataset, the errors of the "best" oversampling methods increased significantly, demonstrating once again that these oversampling methods fill in the features space gap without considering whether the generated examples are truly belong to the minority, and falsely consider them as such. This makes the training



FIGURE 5. Visualization of validating the SMOTE method on three datasets. When the figure is scaled up, more information is obtained.

 TABLE 5.
 ER on vehicle3 dataset using 25% hidden data and some of the methods with the least ER.

Method	NE	SE	ER
M51	168	264	0.64
M24	88	264	0.33
M62	122	264	0.46
M61	61	264	0.23
M19	91	264	0.34
M39	102	236	0.43
M44	194	264	0.73
M68	149	264	0.56

of these examples deceptive, and it could lead to the classifier being overfitted on incorrect data if robust generalization techniques are not used. As a result, when applied to realworld tasks, it is possible that the entire machine learning system fails spectacularly, particularly in critical applications such as security, autonomous driving, aviation safety and medical applications, where even one unrealistic false synthesized example could do catastrophic harm.

#### **VI. CONCLUSION**

Oversampling methods have been used and developed for decades to handle the problem of class imbalance learning, and there is a near exponential growing trend for such type of research. The main question of this research is oversampling approach in its current form and methods provide applicable and viable solution for learning from class imbalance data? We claim that the current oversampling approach is deceptive and could lead to severe failures in real-world applications. In order to answer the main question and to prove our counterclaim, we reviewed a large number of oversampling methods and analyzed their performance in terms of providing unrealistic examples, for this purpose we propose a new validation system for oversampling methods, which we utilized to validate over 70 different oversampling methods. Our validation results on nine real-world common datasets reveal that all of the oversampling methods investigated generate false examples, assuming that they are minorities when they are not, causing classifiers to perform well in labs but more likely fail in practice.

The Oversampling methods investigated in this paper are ranked according to how many incorrect examples they generate. When used to solve real-life problems, the ranking shows that some methods are less harmful than others. When the datasets were changed, however, they were found to produce intolerable number of errors. Therefore, we recommend avoiding such methods when dealing with sensitive applications such as security, autonomous driving, aviation safety, and medical applications that use machine learning from class imbalanced data. Instead, we seriously encourage using ensemble approaches to problems of class imbalance, such as Easy Ensemble [189], Random Data Partitioning [71], etc. Because these methods do not create data out of thin air and do not, as the Undersampling approach suggests, deny the learning process from critical data.

More research should be done in the future to confirm the validity or invalidity of oversampling approach, investigating more methods and incorporating more data. Furthermore, we recommend that additional research be conducted on real-world applications, including measurements of incorrect predictions made with and without the use of oversampling methods, as well as comparisons with ensemble methods.

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