

Received September 9, 2021, accepted September 22, 2021, date of publication September 29, 2021, date of current version October 7, 2021.

Digital Object Identifier 10.1109/ACCESS.2021.3116193

# Perturbative Approach for the Analysis of Charge Distribution on Arbitrarily Shaped Conductors

MAURO BOLOGNA<sup>1</sup>, GIANLUCA CAPOSCIUTTI<sup>2</sup>,  
KRISTOPHER J. CHANDÍA<sup>1</sup>, (Member, IEEE),  
AND BERNARDO TELLINI<sup>2</sup>, (Senior Member, IEEE)

<sup>1</sup>Departamento de Ingeniería Eléctrica-Electrónica, Universidad de Tarapacá, Arica 1010069, Chile

<sup>2</sup>Dipartimento di Ingegneria dell'Energia, dei Sistemi, del Territorio e delle Costruzioni, Università di Pisa, 56122 Pisa, Italy

Corresponding author: Mauro Bologna (mauroh69@gmail.com)

The work of Kristopher J. Chandía was supported by UTA Mayor Project 8736-20.

**ABSTRACT** In this paper, we analyze the electrostatic charge distribution on arbitrarily shaped conductor surfaces. Following a perturbative approach, we derive an approximate analytical formulation of the problem. We start from the known case of a conducting ellipsoid, we adopt a deformed ellipsoidal coordinate system, and we search for the zero-order approximated solution of the problem. We also focus on arbitrary-shaped thin foils, showing that the charge density is divergent on their borders. We then define the applicability range of the proposed approach expressing the contour equation as the Fourier series. Finally, we present a detailed error analysis for several polygonal contours, comparing the analytical results with those obtained via a numerical analysis based on the Finite Element Methods (FEM).

**INDEX TERMS** Charge distribution, conductors, electrostatic analysis.

## I. INTRODUCTION

The problem of finding the electrostatic charge distribution on a charged conductor is a fascinating problem that many classical electrodynamics textbooks solve in several analytical cases [1]–[3]. Still today it is attracting the attention of the researchers. In [4], [5] the authors study the relationships between the electrostatic field near the conducting surface and curvature radius of the surface itself. In [6], [7] the authors perform a numerical analysis of electrostatic problems. In [8], [9] the authors, respectively, study analytically and numerically the capacitance of different arbitrarily shaped conductors. Several practical problems are related to the identification of the charge distribution and possibly its optimization, on thin surface domains, for instance, in energy harvesting and designing devices [10], [11], semiconductors [12], photovoltaics, and optoelectronics [13], [14]. In electrical accumulators, such as lithium batteries, the study of the charge density distribution has a crucial role in developing new techniques to reduce dendrite growth [15], [16]. Many devices used in electrical and electronic engineering are sketched with an ideal geometrical

shape. The knowledge of the charge distribution of a generic geometry of the conductor can allow for a better designing the conductor geometries and for reducing the possibility of occurrence of electrostatic discharge [17]–[19]

A typical example is a capacitor considered as two infinite metallic foils separated by a distance  $d$ . This idealization of a capacitor does not take into account the intense electric field generated near the edges of the conducting surfaces. The problem of electrostatic forces between two finite-size conductors of different geometries has been investigated in several works [20]–[24]. Recently, in [25], the authors consider a battery with finite-size electrodes, making the conjecture that the border effect can be relevant in the dendrite formation. Being of finite size and assumed as two two-dimensional disks, the electrodes have a not uniform charge density taking infinite values at the border of each disk. More generally, any device has a finite size, and the knowledge of the charge density distribution is crucial. The proposed model has been supported by experiments [26], so confirming that the density charge distribution on the battery electrodes plays an important role in dendrite formation. While uniformly charged two-dimensional shapes are studied in the literature, iso-potential surfaces with non-uniform charge distribution are a hard task, and closed formulas for the distribution are

The associate editor coordinating the review of this manuscript and approving it for publication was Jenny Mahoney<sup>1</sup>.

known in a few cases [1]–[3]. In [27]–[30] the authors present interesting methods based on series development. The series method may be difficult to apply when in the solutions, there are divergent quantities. Typically, to reproduce divergent quantities, an increasing number of series terms is necessary. Similar difficulties can arise in numerical approaches such as, for example, the Finite Element Method (FEM). It is an intrinsic limitation for a numerical simulation to reproduce a divergence. The approach that we propose can overcome the difficulty of dealing with divergent quantities since the leading term, zero-order term, in thin foils, is divergent on the foil border. In the present work, we propose a general approach to the problem of an analytical expression of the potential, the electrical field, and the electrical charge density of a metallic surface with an arbitrary shape. In particular, we will focus on thin foil surfaces.

The paper is organized as follows: In Sec. II, we will show the analytical approach to the full problem, i.e., the evaluation of the electric potential and the charge density on an arbitrarily shaped conductor. In Sec. III, we will apply the results of the previous section to thin foils. In Sec. IV, we will show the applicability of our approach. In Sec. V, we will perform a numerical analysis and check on the analytical formulas for thin foils with polygonal shapes, comparing the results with the simulations performed by the software Ansys. In Sec. VI we will discuss the numerical results. Finally, in Sec. VII, we will summarize the paper results.

## II. ELECTRICAL POTENTIAL GENERATED BY A CONDUCTOR SURFACE

Our goal is to find an analytical (approximate) solution of

$$\nabla^2\phi = 0, \quad \phi|_S = \phi_0 \quad (1)$$

where  $S$  is the conductor surface and  $\phi_0$  is the value of the potential at the surface. Since we are considering an arbitrary shape for the conductor surface, we need to adopt a convenient set of coordinates. For this purpose, we consider the coordinate system generated by the following equation [2]

$$\frac{r^2}{a^2(1 + \varepsilon f(\theta))^2 + u} + \frac{z^2}{c^2 + u} = 1 \quad (2)$$

where  $r^2 = x^2 + y^2$ . It is straightforward to check that  $u = 0$  describes the deformed ellipsoid where its section has an arbitrary shape given by  $a(1 + \varepsilon f(\theta))$  (see the example of Fig. 1). Keeping in mind thin foils, we may focus on the confocal oblate spheroids coordinates, i.e.,  $a(1 + \varepsilon f(\theta)) > c$  so we may take the limit  $c \rightarrow 0$  and end up into the two-dimensional thin foil case. Solving for  $u$  we have

$$u_{1,2} = \frac{1}{2} \left( R^2 - a(\theta)^2 - c^2 \pm w \right) \quad (3)$$

where  $R^2 = r^2 + z^2$ ,  $a(\theta) = a(1 + \varepsilon f(\theta))$  and

$$w = \left[ \left( R^2 - a(\theta)^2 - c^2 \right)^2 + 4 \left( z^2 a(\theta)^2 + c^2 r^2 - c^2 a(\theta)^2 \right) \right]^{\frac{1}{2}}.$$

We can choose as third coordinate the polar angle  $\theta$ . Without ambiguity from now on we set  $u = u_1$  and  $u_2 = v$ . The inverse relationships are

$$r = \frac{\sqrt{a^2(\theta)^2 + u}\sqrt{a^2(\theta)^2 + v}}{\sqrt{a^2(\theta)^2 - c^2}} \quad (4)$$

$$z = \frac{\sqrt{c^2 + u}\sqrt{c^2 + v}}{\sqrt{c^2 - a(\theta)^2}} \quad (5)$$

To evaluate the laplacian of the potential in the  $u, v, \theta$  coordinates, we may use the general formula given by [31]

$$\nabla^2\phi = \frac{1}{\sqrt{g}} \frac{\partial}{\partial u^i} \left( \sqrt{g} g^{ik} \frac{\partial \phi}{\partial u^i} \right) = 0, \quad (6)$$

where  $u^1 = u$ ,  $u^2 = v$ ,  $u^3 = \theta$ ,  $g = \text{Det}[g_{ik}]$  is the determinant of the metric tensor,  $g_{ik}$ , and  $g^{ik}$  are the inverse matrix elements of  $g_{ik}$ . Also, according to Einstein's summation convention, repeated suffix implies summation. To find the metric tensor associated with these coordinates, we write the infinitesimal distance between two points

$$dr = \frac{\partial r}{\partial u} du + \frac{\partial r}{\partial v} dv + \frac{\partial r}{\partial \theta} d\theta \quad (7)$$

$$dz = \frac{\partial z}{\partial u} du + \frac{\partial z}{\partial v} dv + \frac{\partial z}{\partial \theta} d\theta \quad (8)$$

$$ds^2 = dr^2 + dz^2 + r^2 d\theta^2 = g_{ik} du^i du^k, \quad (9)$$

with  $g_{ik} = g_{ki}$ ,  $u^1 = u$ ,  $u^2 = v$ ,  $u^3 = \theta$ . Plugging Eqs. (4) and (5) into Eqs. (7) and (8). We obtain the metric tensor elements writing the square of the infinitesimal length of a curve in the  $u, v, \theta$  coordinates

$$\begin{aligned} ds^2 = & \frac{u - v}{4(a^2[1 + \varepsilon f(\theta)]^2 + u)(c^2 + u)} du^2 \\ & + \frac{v - u}{4(a^2[1 + \varepsilon f(\theta)]^2 + v)(c^2 + v)} dv^2 \\ & + \frac{[a^2(1 + \varepsilon f(\theta))^2 + u][a^2(1 + \varepsilon f(\theta))^2 + v]}{a^2[1 + \varepsilon f(\theta)]^2 - c^2} d\theta^2 \\ & + \delta g_{ik} du^i du^k, \quad \delta g_{ik} = \delta g_{ki}, \quad i, k = u, v, \theta, \quad i \neq k \end{aligned} \quad (10)$$

where for the sake of compactness, we did not explicitly write the off-diagonal terms,  $\delta g_{ik}$ . From Eq. (10), we deduce the elements of the metric tensor

$$g_{uu} \equiv h_1^2 = \frac{u - v}{4(a(\theta)^2 + u)(c^2 + u)}, \quad (11)$$

$$g_{vv} \equiv h_2^2 = \frac{v - u}{4(a(\theta)^2 + v)(c^2 + v)}, \quad (12)$$

$$g_{\theta\theta} \equiv h_3^2 = \frac{[a(\theta)^2 + u][a(\theta)^2 + v]}{a(\theta)^2 - c^2}, \quad (13)$$

$$\begin{aligned} \delta g_{u\theta} = & \varepsilon a(\theta) a f'(\theta) (a(\theta)^2 + v) \\ & \times \frac{[a(\theta)^2 (a(\theta)^2 - 2c^2) - c^2(u + v) - uv]}{(c^2 - a(\theta)^2)^2}, \end{aligned} \quad (14)$$

$$\delta g_{v\theta} = \varepsilon a(\theta) a f'(\theta) \left( a(\theta)^2 + u \right) \times \frac{[a(\theta)^2 (a(\theta)^2 - 2c^2) - c^2(u + v) - uv]}{(a(\theta)^2 - c^2)^2}. \quad (15)$$

From here on, the parameter  $\varepsilon$  will be considered a perturbative parameter, i.e.,  $\varepsilon \ll 1$ . To zero  $\varepsilon$  order, we seek a solution that is a function of the coordinate  $u$ , namely the coordinate that vanishes at the surface of the conductor. The Laplace equation for the electric potential  $\phi(u, v, \theta)$  is given by

$$\begin{aligned} \nabla^2 \phi &= \frac{1}{\sqrt{g}} \frac{\partial}{\partial u^i} \left( \sqrt{g} g^{ik} \frac{\partial \phi}{\partial u^k} \right) \\ &= \frac{1}{h_1 h_2 h_3} \frac{\partial}{\partial u} \left( \frac{h_2 h_3}{h_1} \frac{\partial \phi}{\partial u} \right) = 0. \end{aligned} \quad (16)$$

While the coordinates  $u, v$  do not have crossed terms,  $g_{uv} = 0$ , in principle we should consider the fact that  $g_{\theta k} \neq 0$ . But the contribution of these terms and the  $\theta$  derivative is of the  $\varepsilon$  order (see Eqs. (14) and (15)). We also stress that we cannot neglect  $\varepsilon$  in the function  $a(\theta)$  in the denominator of  $h_1$  because the variable  $u$  can take the zero value since  $u = 0$  is the surface of the conductor. Therefore, in the denominator, the term containing  $\varepsilon$  cannot be neglected. Solving Eq. (16) with the boundary condition  $\phi \rightarrow 0$  for  $u \rightarrow \infty$  and  $\phi = \text{constant}$  for  $u = 0$ , we have

$$\phi_0 = A \frac{\arctan \left[ \frac{\sqrt{a(\theta)^2 - c^2}}{\sqrt{c^2 + u}} \right]}{\arctan \left[ \frac{\sqrt{a(\theta)^2 - c^2}}{c} \right]} \quad (17)$$

and the charge density on the surface of the conductor, to zero-order, is

$$\begin{aligned} \sigma_0 &= -\frac{\varepsilon_0}{h_1} \frac{\partial}{\partial u} \phi_0 \Big|_{u=0} \\ &= \frac{\varepsilon_0 A \sqrt{a(\theta)^2 - c^2}}{\sqrt{a(\theta)^4 - r^2} [a(\theta)^2 - c^2] \arctan \left[ \frac{\sqrt{a(\theta)^2 - c^2}}{c} \right]}, \end{aligned} \quad (18)$$

where  $\varepsilon_0$  is the vacuum permittivity.

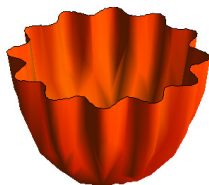


FIGURE 1. Ellipsoid with a section given by  $a(1 + \varepsilon f(\theta)) = 1 + 0.1 \cos(12\theta)$ .

### III. CHARGE DENSITY ON THIN FOILS

In this section, we will focus now on the case of a thin foil with an arbitrary border. The foil's electric potential is obtained taking the limit  $c \rightarrow 0$  of Eq. (17). The surface density is obtained taking the limits  $c \rightarrow 0, u \rightarrow 0$  and

$z \rightarrow 0$  of Eq. (18). Adopting the more visualizable cylindrical coordinate system  $r, \theta, z$ , for the potential we have

$$\phi_0 = A \arctan \left[ \frac{a(\theta)}{\sqrt{u}} \right] = A \arctan [\Phi(r, z, \theta)], \quad (19)$$

where

$$\Phi(r, z, \theta) = \left[ \frac{2 a(\theta)^2}{R^2 - a(\theta)^2 + \sqrt{(R^2 - a(\theta)^2)^2 + 4 z^2 a(\theta)^2}} \right]^{\frac{1}{2}}$$

and  $R^2 = r^2 + z^2$ . For the density we have

$$\sigma_0 = -\frac{\varepsilon_0}{h_1} \frac{\partial}{\partial u} \phi_0 \Big|_{u=0} = \frac{\varepsilon_0 A}{\sqrt{a(\theta)^2 - r^2}}. \quad (20)$$

We infer that at the border of the conductor,  $r = a(\theta)$ , the density is divergent. When  $\varepsilon = 0$  then  $a(\theta) = a[+\varepsilon f(\theta)] = a$  and we recover the exact result of a disk of radius  $a$ . As we will see in Sec. V, for  $\varepsilon \ll 1$  the zero approximation is already satisfactory.

We now evaluate the first correction to the potential, and consequently, to the charge density. To further simplify our calculation, we use cylindrical coordinates. We focus on solving the Laplace equation near the surface, i.e., at  $z = 0$ , so finding the correction to the charge density. We may write

$$\nabla^2 \phi = \nabla^2 \phi_0 + \nabla^2 \phi_1 = 0, \quad (21)$$

where  $\phi_1$  is of  $\varepsilon$  order. The potential  $\phi_0$  satisfy the Laplace equation in the  $r, z$  variables while the derivative respect to  $\theta$  generates a  $\varepsilon$  order term. Developing  $\phi_0$  and  $\phi_1$  near  $z = 0$

$$\phi_0 \approx \text{const} + z \frac{\partial}{\partial z} \phi_0 \Big|_{z=0} = \text{const} - z \frac{\sigma_0}{\varepsilon_0}, \quad \phi_1 \approx z \varrho(r, \theta) \quad (22)$$

we have

$$\nabla^2 \phi_1 = z \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} \sigma_0. \quad (23)$$

We stress that the problem is symmetric with respect to the  $z$  coordinate, and the potential is an odd function of  $z$ . In principle, we should also consider the term proportional to  $z^3$  but, for the moment, we assume that it is negligible with respect  $\phi_1$ . Assuming a Taylor expansion in  $r$  for the function  $\varrho(r, \theta)$ , we write

$$\phi_1 = z \sum_{n=0}^{\infty} r^{2n} y_n(\theta), \quad (24)$$

and plugging it into Eq. (23) we have

$$\begin{aligned} \sum_{n=0}^{\infty} 4n^2 r^{2n} y_n(\theta) + r^{2n} \frac{\partial^2}{\partial \theta^2} y_n(\theta) \\ = A \sum_{n=0}^{\infty} \binom{-\frac{1}{2}}{n} r^{2n} \frac{\partial^2}{\partial \theta^2} h_n(\theta), \end{aligned} \quad (25)$$

where we defined  $h_n(\theta) \equiv a(\theta)^{-2n-1}$ . Solving for  $n = 0$  we have

$$y_0(\theta) = A \left( \frac{1}{a(\theta)} - \frac{1}{a(0)} \right), \quad (26)$$

while for  $n \neq 0$  we have

$$y_n(\theta) = A \left( \frac{-\frac{1}{2}}{n} \right) \left[ -\cos(2n\theta) \left( \int_0^\theta \frac{h_n''(u) \sin(2nu)}{2n} du \right) + \sin(2n\theta) \left( \int_0^\theta \frac{h_n''(u) \cos(2nu)}{2n} du \right) \right] \quad (27)$$

where  $h''(\theta)$  means second derivative with respect to  $\theta$  and the integration constants have been selected in such way that  $y_n(\theta) \rightarrow 0$  for  $\varepsilon \rightarrow 0$ . After long but straightforward algebra we obtain

$$y_n(\theta) = A \left( \frac{-\frac{1}{2}}{n} \right) \left[ h_n(\theta) - h_n(0) \cos(2n\theta) - \frac{h_n'(0) \sin(2n\theta)}{2n} - 2n \int_0^\theta h_n(u) \sin [2n(\theta - u)] du \right]. \quad (28)$$

For sake of simplicity, we assume  $f'(0) = 0$  which, in turn, implies  $h'(0) = 0$ . The condition  $f'(0) = 0$  is satisfied by all polygons with an even number of sides. Performing the sum we have

$$\sum_{n=0}^{\infty} r^{2n} y_n(\theta) = A \left[ \frac{1}{\sqrt{a(\theta)^2 - r^2}} + \text{Re} \left[ \frac{1}{\sqrt{a(0)^2 - r^2 e^{2i\theta}}} \right] + \text{Im} \left[ \int_0^\theta \frac{r^2 e^{2i(\theta-u)} U(a(u) - r)}{[a(u)^2 - r^2 e^{2i(\theta-u)}]^{3/2}} du \right] \right] \quad (29)$$

where  $U(x)$  is the step function. Remembering that the correction to the potential near  $z = 0$  is  $\phi_1 = z \sum_n r^{2n} y_n(\theta)$  we obtain for the density correction

$$\sigma^{(1)}(r, \theta) = \epsilon_0 A \left[ -\frac{1}{\sqrt{a(\theta)^2 - r^2}} + \text{Re} \left[ \frac{1}{\sqrt{a(0)^2 - r^2 e^{2i\theta}}} \right] + \text{Im} \left[ \int_0^\theta \frac{r^2 e^{2i(\theta-u)} U(a(u) - r)}{[a(u)^2 - r^2 e^{2i(\theta-u)}]^{3/2}} du \right] \right]. \quad (30)$$

By direct inspection of Eq. (30), we may verify that for  $\varepsilon \rightarrow 0$  then  $\sigma^{(1)}(r, \theta) \rightarrow 0$ . To take into account the term proportional to  $z^3$ , previously neglected, we introduce

the effective constant  $B$ , instead of the constant  $A$  multiplying  $\sigma^{(1)}(r, \theta)$ . Once the density correction has been determined, we can write for the electric potential

$$\begin{aligned} \phi(x, y, z) &= \frac{2}{4\pi\epsilon_0} \\ &\times \int_0^{2\pi} \int_0^{a(\theta)} \frac{\sigma(r, \theta)}{\sqrt{r^2 - 2r(x \cos \theta + y \sin \theta) + R^2}} r dr d\theta \\ &= \int_0^{2\pi} \int_0^{a(\theta)} \frac{\sigma^{(0)}(r, \theta)}{\sqrt{r^2 - 2r(x \cos \theta + y \sin \theta) + R^2}} r dr d\theta \\ &+ \int_0^{2\pi} \int_0^{a(\theta)} \frac{\sigma^{(1)}(r, \theta)}{\sqrt{r^2 - 2r(x \cos \theta + y \sin \theta) + R^2}} r dr d\theta, \end{aligned} \quad (31)$$

where  $R^2 = x^2 + y^2 + z^2$ , the extra factor 2 takes into account the contribution of the upper and lower conductor surface, and with

$$\sigma^{(0)}(r, \theta) = \frac{A}{\sqrt{a(\theta)^2 - r^2}} \quad (32)$$

$$\begin{aligned} \sigma^{(1)}(r, \theta) = B \left[ -\frac{1}{\sqrt{a(\theta)^2 - r^2}} + \text{Re} \left[ \frac{1}{\sqrt{a(0)^2 - r^2 e^{2i\theta}}} \right] + \text{Im} \left[ \int_0^\theta \frac{r^2 e^{2i(\theta-u)} U(a(u) - r)}{[a(u)^2 - r^2 e^{2i(\theta-u)}]^{3/2}} du \right] \right], \end{aligned} \quad (33)$$

where, as previously stated, the effective constant  $B$  multiplies  $\sigma^{(1)}(r, \theta)$  instead of the constant  $A$ . Also  $A$  and  $B$  have been redefined in such a way to include the constant  $\frac{2}{4\pi\epsilon_0}$ . By construction,  $\phi(x, y, z)$  given by Eq. (31) satisfies the Laplace equation and  $\partial_z \phi(x, y, z)|_{z=0}$  gives the charge density at the surface of the conductor, i. e.  $\sigma(r, \theta) = \sigma^{(0)}(r, \theta) + \sigma^{(1)}(r, \theta)$ . In Sec. V we will numerically check that  $\phi(x, y, z)$ , at  $z = 0$  and in the region  $r \leq a(\theta)$ , is, with good approximation, constant.

#### IV. APPLICABILITY OF THE APPROXIMATION

So far, we have not given details on the applicability of the approximation in the presence of thin foils with arbitrary border. It is important to note that, despite a shape that visually appears relatively far from a circular shape, what is relevant in our calculation is the first non-constant term of  $a(\theta) = a(1 + \varepsilon f(\theta))$ , i.e.  $\varepsilon f(\theta)$ . If  $\varepsilon \ll 1$ , then our approach applies. In general, the border is described by a function where not necessarily identifying the  $\varepsilon$  parameter is straightforward. We can give a criterion to identify the parameter using the Fourier series of the border. To do that, we write

$$a(\theta) = \sum_{k=0}^{\infty} c_k \frac{\exp[ik\theta]}{\sqrt{2\pi}} + \sum_{k=1}^{\infty} c_k^* \frac{\exp[-ik\theta]}{\sqrt{2\pi}}, \quad (34)$$

where  $c_k^*$  is the complex conjugate of  $c_k$ . Let us define  $\bar{k}$  the index of the first Fourier coefficient that does not vanish.

Then, as a first approximation, we may write  $a(\theta)$  as the sum of the first two non-vanishing terms

$$a(\theta) \approx c_0 \left( 1 + \frac{2|c_{\bar{k}}|}{c_0} \cos[\bar{k}\theta + \phi_{\bar{k}}] \right), \quad c_{\bar{k}} = |c_{\bar{k}}| \exp[i\phi_{\bar{k}}], \quad (35)$$

where we use the polar representation of the Fourier coefficients  $c_{\bar{k}} = |c_{\bar{k}}| \exp[i\phi_{\bar{k}}]$ . Our approach applies if  $2|c_{\bar{k}}|/c_0 \ll 1$ . Indeed, being  $c_k$  the coefficient of a convergent series, then in general we have that  $c_k < c_{\bar{k}}$  for  $k > \bar{k}$ .

To better clarify this point, let us consider the case of a square. Its border is described by

$$a(\theta) = \cos\left(\frac{\pi}{4}\right) \sec\left[\theta - \frac{\pi}{2} \left\lfloor \frac{4\theta + \pi}{2\pi} \right\rfloor\right], \quad (36)$$

that represents a square of side  $a = \sqrt{2}$ . The first non-vanishing terms are given by  $c_0 \approx 0.79$ ,  $c_4 = c_4^* \approx -0.055$  and we can write

$$a(\theta) \approx c_0 \left[ 1 + \frac{2c_4}{c_0} \cos(4\theta) \right]. \quad (37)$$

Consequently we may set  $\varepsilon = 2c_4/c_0 \approx 0.14$ . We deduce that a square can be considered a deformed circle, even if the first-order perturbative approach is not accurate. We will return to the square conductor study in the next section to perform numerical analysis on surfaces with a polygonal border.

### V. NUMERICAL ANALYSIS

In this section, we will check our result by performing a numerical analysis on a thin foil with a polygonal edge with  $n$  sides. The function that describes a  $n$ -sided polygon is

$$a(\theta) = \cos\left(\frac{\pi}{n}\right) \sec\left[\theta - \frac{2\pi}{n} \left\lfloor \frac{n\theta + \pi}{2\pi} \right\rfloor\right]. \quad (38)$$

The main goal of this section is the numerical evaluation of the percent error defined as  $E = 100(\phi - \phi_S)/\phi_S$  at  $z = 0$  in the region  $r \leq a(\theta)$  where the potential  $\phi$  takes the constant value  $\phi_S$ . Without loss of generality we may set  $\phi_S = 1$ . In order to perform the numerical analysis, the coefficients  $A$  and  $B$  of Eqs. (32) and (33) need to be evaluated. We calculate the function  $\phi$  in a D-elements computational domain  $(x_i, y_i)$  belonging to the polygon. We define  $M_1(x_i, y_i)$  and  $M_2(x_i, y_i)$  as

$$M_1(x_i, y_i) = \frac{1}{A} \int_0^{2\pi} \int_0^{a(\theta)} \frac{\sigma^{(0)}(r, \theta)r}{\sqrt{r^2 - 2r(x \cos \theta + y \sin \theta) + r_i^2}} dr d\theta, \quad (39)$$

$$M_2(x_i, y_i) = \frac{1}{B} \int_0^{2\pi} \int_0^{a(\theta)} \frac{\sigma^{(1)}(r, \theta)r}{\sqrt{r^2 - 2r(x \cos \theta + y \sin \theta) + r_i^2}} dr d\theta, \quad (40)$$

where  $r_i^2 \equiv x_i^2 + y_i^2$  and  $A$  and  $B$  are determined by solving the system

$$\begin{bmatrix} M_1(x_1, y_1) & M_2(x_1, y_1) \\ M_1(x_2, y_2) & M_2(x_2, y_2) \\ \vdots & \vdots \\ M_1(x_D, y_D) & M_2(x_D, y_D) \end{bmatrix} \begin{bmatrix} A \\ B \end{bmatrix} = \begin{bmatrix} 1 \\ 1 \\ \vdots \\ 1 \end{bmatrix}. \quad (41)$$

The linear system of Eq. (41) is over-determined, and  $A$  and  $B$  are calculated by minimizing the 2-norm  $N^{(2)}$  given by

$$N^{(2)} = \sqrt{\sum_{i=1}^D (AM_1(x_i, y_i) + BM_2(x_i, y_i))^2 - 1}. \quad (42)$$

To evaluate  $M_1(x_i, y_i)$  and  $M_2(x_i, y_i)$  we perform a numerical integration by means of Matlab<sup>®</sup> [32]–[34]. First of all, we generate a two-dimensional numerical domain, according to Eq. (38). Since the numerical values of the integrals defining  $M_1$  and  $M_2$  are divergent along the border of the domains, the distribution of the couples  $(x_i, y_i)$  inside the polygonal domain is crucial for the evaluation of  $A$  and  $B$ . Therefore, we randomly selected  $6 \times 10^3$  couples for each case to provide a uniform point distribution and a minor bias in the  $A$  and  $B$  estimation. Also, we adopted a minimum distance between the points to increase the uniformity of their distribution. The adopted number of coordinates, at which  $M_1$  and  $M_2$  are evaluated, is a balance between the accuracy calculating  $A$  and  $B$  and the computational resources availability. In Fig. 2 we show, as example, the domain for  $n = 4$  (i.e. square domain) resulting from the aforementioned discretization. Being the surface an electrical conductor, the domain  $r \leq a(\theta)$  is expected to be at the same potential  $\phi_0 = 1$ , and, ideally,  $A$  and  $B$  are expected to satisfy  $AM_1(x_i, y_i) + BM_2(x_i, y_i) - 1 = 0 \forall i$ . In the practical case, the analytical approximation and the numerical errors, mainly due to the adopted integral algorithm tolerance [33], [34], lead to different values from the expected one. With the choice  $\phi_S = 1$ , the percent error  $E$  for each domain position is given by

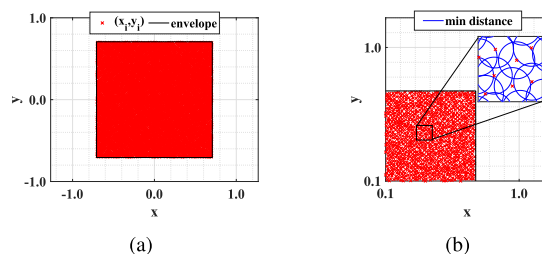


FIGURE 2. Plot (a): Representation of a square domain. Plot (b): Particular for  $x > 0$  and  $y > 0$ .

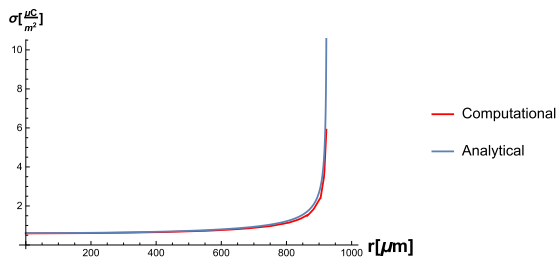
$$E = [AM_1(x_i, y_i) + BM_2(x_i, y_i) - 1] 100. \quad (43)$$

The  $A$  and  $B$  coefficients are calculated for a polygon with  $n$  sides and  $n$  ranging in  $n \in [4, 14]$  and minimizing  $N^{(2)}$  given by Eq. (42). Average, median, maximum positive

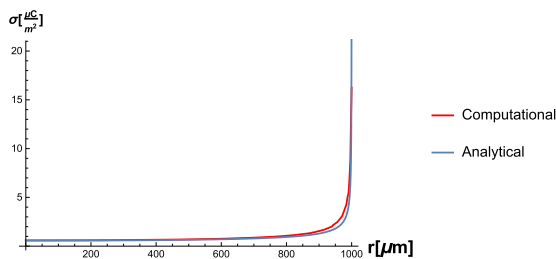
and negative errors based on  $E$  are further compared for all the tested cases. Finally, we compare the analytical results with the numerical simulation performed using the software Ansys. More precisely, we compare the numerical simulation with the zero-order of the perturbative approach given by

$$\sigma^{(0)}(r, \theta) = \frac{2\phi_S}{\pi} \frac{\epsilon_0}{\sqrt{a(\theta)^2 - r^2}}, \quad (44)$$

where the surface potential  $\phi_S$ , for numerical reasons, has been set 100 volts instead of the unit. The thickness of the thin octagonal foil is 0.01 mm, and the radius of the circumscribed circumference, i.e., the distance center-vertex of the octagon, is 1 mm. The agreement between the analytical formula (44) and the numerical analysis is very good, as shown in Figs. 3 and 4. It is worthy of stressing that, being the charge density divergent on the octagon border, the agreement between analytical formulation and numerical calculations ceases to hold in the vicinity of the border.



**FIGURE 3.** Charge density: Blu line the analytical result given by (32). Red line the numerical evaluation. We compared the results along the line  $\theta = 0$ , i.e., the  $x$  axis. For numerical reason the potential on the surface  $\phi_S$  has been set 100 volts. The thickness of the foil is 0.01 mm, and the radius of the circumscribed circumference is 1 mm.

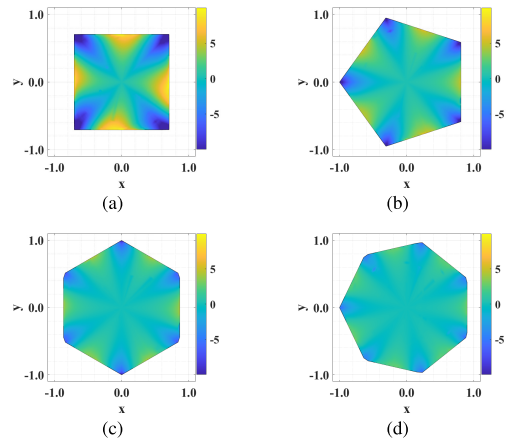


**FIGURE 4.** Charge density: Blu line the analytical result given by (32). Red line the numerical evaluation. We compared the results along the line  $\theta = \pi/8$ , i.e., from the origin to the vertex of the octagon. For numerical reason the potential on the surface  $\phi_S$  has been set 100 volts. The thickness of the foil is 0.01 mm, and the radius of the circumscribed circumference is 1 mm.

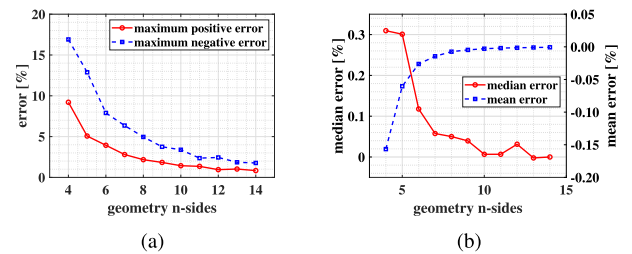
## VI. DISCUSSION OF THE NUMERICAL RESULTS

The potential  $\phi$  resulting from the numerical integration of Eq. (31), with the  $A$  and  $B$  coefficient obtained according to the aforementioned method, is calculated, and the error  $E$  derived from Eq. (43) is shown in Fig. 5 for different geometries ( $\phi_S = 1$ ). In particular, it is shown that the value of  $\phi$  is underestimated with respect to the attended value  $\phi_S = 1$  in the corner region in all the cases. At the same time, the error

$E$  practically vanishes in the center of the domain. The error  $E$  is significantly reduced with the increase of the polygon sides, as shown in Figs. 5 a-d. This behavior is expected since, increasing  $n$ , the influence of the corners is reduced. The domain tends to a circular shape and Eq. (19) with  $a(\theta) = a$  gives the exact expression for potential  $\phi(r, \theta)$ . A quantitative analysis is performed on the maximum positive and negative percent error  $E$ , the median and mean error along with the numerical domain, which is shown in Fig. 6.



**FIGURE 5.** Representation of the percent error  $E$  in polygonal domains: Square domain, plot (a). Pentagonal domain, plot (b). Hexagonal domain, plot (c). Heptagonal domain, plot (d).

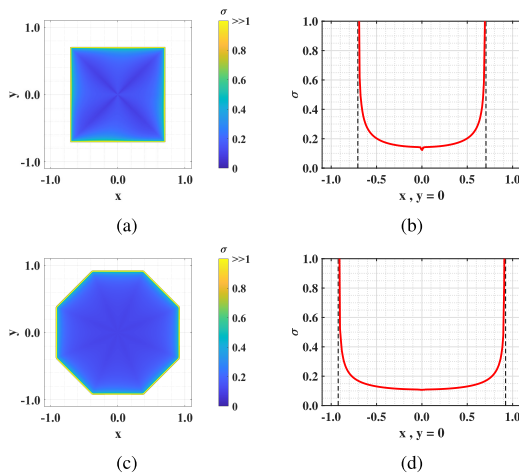


**FIGURE 6.** Numerical analysis of the different types of error as function of the polygon sides. Plot (a): The  $x$ -axis represents the side number of the polygons while the  $y$ -axis represents the percent error. Plot (b): The  $x$ -axis represents the side number of the polygons while the  $y$ -axes represent the median (on the left) and mean (on the right) error.

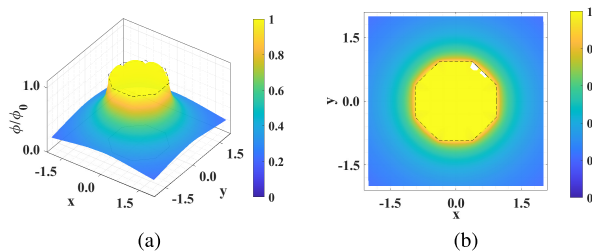
The error  $E$  has a descent trend as a function of  $n$ , while the domain tends to the circular one. By comparing Figs. 5 and 6, we observe that the largest error is located on the corner area, where it reaches value  $-18\%$  on the square domain case. A slight overestimation of  $\phi$  occurs on the side area within a  $9\%$  range. Regarding the numerical calculations, the largest error amount is found on the domain borders, where Eqs. (32) and (33) diverge, thus introducing an underestimation of  $\phi$  during the numerical integration. The presented calculations show an average underestimation error within  $0.2\%$  range and a median error within  $0.35\%$  range for all the tested cases, thus confirming the capability of the current method to perform a satisfactory evaluation of the electrical potential  $\phi$  and the charge density  $\sigma$  on the chosen domains. The obtained values of  $A$ ,  $B$ , and the norm  $N^{(2)}$  for the different domains are shown in Tab. 1.

**TABLE 1.** Evaluated values of the coefficients  $A$ ,  $B$ , and  $N^{(2)}$  for the polygonal cases. The value of  $A$  is of the order of  $\pi^{-2} \approx 0.1013$ .

$n$ sides	$A$	$B$	$N^{(2)}$
4	0.1012	-0.0291	3.05
5	0.1015	-0.0100	1.88
6	0.1011	-0.0098	1.22
7	0.1011	-0.0104	0.90
8	0.1012	-0.0085	0.64
9	0.1012	-0.0073	0.50
10	0.1011	-0.0052	0.39
11	0.1012	-0.0044	0.32
12	0.1014	-0.0041	0.28
13	0.1012	-0.0013	0.23
14	0.1012	-0.0011	0.19



**FIGURE 7.** Charge density in two different domains. In (a) and (b) the density  $\sigma$  is plotted for a square domain and for the line  $y = 0$ , respectively. In (c) and (d) the density  $\sigma$  is plotted for an octagonal domain and for the line  $y = 0$ , respectively.



**FIGURE 8.** Figure (a): Plot of the electrical potential generated by a conducting octagonal surface given by Eq. (31) evaluated at  $z = 0$ . Figure (b): Plot of the electrical potential generated by a conducting octagonal surface given by Eq. (31) evaluated at  $z = 0$ . A point of view from above.

According to Eq. (31), at  $x = y = z = 0$ , the integral associated to the  $\sigma^{(0)}$  term takes the value  $A\pi^2$  for any border  $a(\theta)$ . The value of  $M_1$  is expected approximately  $\pi^2$ , and consequently the value of  $A$  is of the order of  $\pi^{-2} \approx 0.1013$  as consistently shown in Tab. 1. The coefficient  $B$  decreases as the number of sides increases, which is also expected. Indeed, while  $n$  increases, the domain tends to a circle, reducing the corrective term's contribution to zero. However, it is worthy to notice that the low contribution of the  $M_2(x_i, y_i)$  term to the potential  $\phi$  leads to higher sensitivity in  $B$  calculation through the solution of the over-determined system shown in Eq. (41). Finally, Figs. 7b and 7d show the charge density behavior on

a sample line i.e.  $y = 0$  in order to highlight its divergent behavior on the borders.

### VII. CONCLUSION

In this paper, we presented an analytical formulation of the problem of electrostatic charge distributions on arbitrarily shaped conductor surfaces. We derived an approximate analytical formulation via a perturbative approach consisting in adopting a deformed ellipsoidal coordinate system. We analytically showed the intuitive result that the charge density takes divergent values on the border of two-dimensional conductors providing the closed analytical expression of the quantities of interest. The approach is applicable when, developing the border equation in Fourier series, the first non-constant border Fourier coefficient is small compared to the constant term, regardless of the geometry of the edge. To the zero-order, we showed that the problem is solved by assigning to the constant  $A$  the value  $\pi^{-2}$  for all the borders. We compared the analytical results with a numerical analysis based on the Finite Element Methods (FEM). For this purpose we analyzed several polygonal contours, and the agreement between the two approaches, already at the zero perturbative order, was found remarkable. This allows us to perform an analytical treatment of the density charge distribution on an arbitrary shaped conducting surface. The presented approach can overcome the difficulty of dealing with divergent quantities when a series approach is used.

### REFERENCES

- [1] P. M. Morse and H. Feshbach, *Methods of Theoretical Physics*. New York, NY, USA: McGraw-Hill, 1953.
- [2] L. D. Landau, E. M. Lifshitz, and L. P. Pitaevskii, *Electrodynamics of Continuous Media*, 2nd ed. Oxford, U.K.: Butterworth-Heinemann, 1984.
- [3] J. D. Jackson, *Classical Electrodynamics*, 3rd ed. Hoboken, NJ, USA: Wiley, 1999.
- [4] L. Enze, "The application of a surface charge density distribution function to the solution of boundary value problems," *J. Phys. D, Appl. Phys.*, vol. 20, no. 12, pp. 1609–1615, Dec. 1987, doi: 10.1088/0022-3727/20/12/011.
- [5] D. Fan, "The charge-density distribution on conductor surfaces," *J. Phys. D, Appl. Phys.*, vol. 21, no. 2, pp. 365–366, Feb. 1988, doi: 10.1088/0022-3727/21/2/019.
- [6] P. A. Krutitskii, D. Y. Kwak, and Y. K. Hyon, "Numerical treatment of a skew-derivative problem for the Laplace equation in the exterior of an open arc," *J. Eng. Math.*, vol. 59, no. 1, pp. 25–60, Jul. 2007, doi: 10.1007/s10665-006-9058-x.
- [7] M. Boutaayamou, R. V. Sabariego, and P. Dular, "Electrostatic analysis of moving conductors using a perturbation finite element method," *IEEE Trans. Magn.*, vol. 45, no. 2, pp. 266–274, Mar. 2009, doi: 10.1109/TMAG.2009.2012541.
- [8] J. D. Jackson, "A curious and useful theorem in two-dimensional electrostatics," *Amer. J. Phys.*, vol. 67, no. 2, pp. 107–115, Feb. 1999, doi: 10.1119/1.19203.
- [9] M. Dhamodaran and R. Dhanasekaran, "Evaluation of the capacitance and charge distribution of metallic objects by electrostatic analysis," *J. Sci. Ind. Res.*, vol. 75, pp. 552–556, Sep. 2016. [Online]. Available: https://www.scirp.org/journal/paperinformation.aspx?paperid=65868, doi: 10.4236/cs.2016.74025.
- [10] D. Kim, W.-G. Kim, I. K. Jin, H. Park, S.-G. Im, and Y.-K. Choi, "A study of the charge distribution and output characteristics of an ultra-thin triboelectric layer," *Nano Energy*, vol. 62, pp. 458–464, Aug. 2019, doi: 10.1016/j.nanoen.2019.05.070.

- [11] J. Zhang, M. Chi, Q. Chen, W. Sun, and J. Cao, "Effect of temperature on space charge distribution in two layers of transformer oil and impregnated pressboard under DC voltage," *IEEE Access*, vol. 8, pp. 16647–16655, 2020, doi: [10.1109/ACCESS.2020.2967633](https://doi.org/10.1109/ACCESS.2020.2967633).
- [12] C. Sciascia, M. Celebrano, M. Binda, D. Natali, G. Lanzani, and J. R. Cabanillas-Gonzalez, "Electric field and charge distribution imaging with sub-micron resolution in an organic thin-film transistor," *Organic Electron.*, vol. 13, no. 1, pp. 66–70, Jan. 2012, doi: [10.1016/j.orgel.2011.09.023](https://doi.org/10.1016/j.orgel.2011.09.023).
- [13] L. Yang and K. Dayal, "Influence of strain on space-charge distribution at ferroelectric thin-film free surfaces," *Acta Mater.*, vol. 60, no. 19, pp. 6457–6463, Nov. 2012, doi: [10.1016/j.actamat.2012.07.050](https://doi.org/10.1016/j.actamat.2012.07.050).
- [14] P. Ferraro, S. Grilli, and P. De Natale, Eds., *Ferroelectric Crystals for Photonic Applications: Including Nanoscale Fabrication and Characterization Techniques*, 2nd ed. Berlin, Germany: Springer-Verlag, 2014, p. 503.
- [15] Z. Liu and X. Dang, "A new method for state of charge and capacity estimation of lithium-ion battery based on dual strong tracking adaptive H infinity filter," *Math. Problems Eng.*, vol. 2018, Sep. 2018, Art. no. 5218205, doi: [10.1155/2018/5218205](https://doi.org/10.1155/2018/5218205).
- [16] D. Kang, K. Tang, J. Koh, W. Liang, and J. P. Lemmon, "Homogenous charge distribution by free-standing porous structure for dendrite-free Li metal anode," *J. Energy Chem.*, vol. 44, pp. 68–72, May 2020, doi: [10.1016/j.jechem.2019.09.005](https://doi.org/10.1016/j.jechem.2019.09.005).
- [17] R. Giannetti, M. Macucci, and B. Tellini, "Remarks on models for prediction of radiated fields in electrical discharge events," *Electr. Lett.*, vol. 37, pp. 817–819, Jun. 2001, doi: [10.1049/el:20010575](https://doi.org/10.1049/el:20010575).
- [18] M. Macucci and B. Tellini, "Measurement of RF emissions from electrostatic discharges between charged insulators," *IEEE Trans. Instrum. Meas.*, vol. 57, no. 7, pp. 1403–1409, Jul. 2008, doi: [10.1109/TIM.2008.917194](https://doi.org/10.1109/TIM.2008.917194).
- [19] L. Huang, Q. Zhang, Y. Li, L. Shi, C. Gao, J. Wang, and F. Guo, "Correlation of charge distribution among different branches in a natural lightning flash," *IEEE Access*, vol. 6, pp. 42829–42836, 2018, doi: [10.1109/ACCESS.2018.2859399](https://doi.org/10.1109/ACCESS.2018.2859399).
- [20] A. S. Khair, "Electrostatic forces on two almost touching nonspherical charged conductors," *J. Appl. Phys.*, vol. 114, no. 13, Oct. 2013, Art. no. 134906, doi: [10.1063/1.4824540](https://doi.org/10.1063/1.4824540).
- [21] G. Paffuti, E. Cataldo, A. Di Lieto, and F. Maccarrone, "Circular plate capacitor with different discs," *Proc. Roy. Soc. A, Math., Phys. Eng. Sci.*, vol. 472, no. 2194, Oct. 2016, Art. no. 20160574, doi: [10.1098/rspa.2016.0574](https://doi.org/10.1098/rspa.2016.0574).
- [22] G. Paffuti, "Numerical and analytical results for the two discs capacitor problem," *Proc. Roy. Soc. A, Math., Phys. Eng. Sci.*, vol. 473, no. 2197, Jan. 2017, Art. no. 20160792, doi: [10.1098/rspa.2016.0792](https://doi.org/10.1098/rspa.2016.0792).
- [23] F. Maccarrone and G. Paffuti, "Capacitance and forces for two square electrodes," *J. Electrostatics*, vol. 89, pp. 20–29, Oct. 2017, doi: [10.1016/j.elstat.2017.06.007](https://doi.org/10.1016/j.elstat.2017.06.007).
- [24] C. Bednarz, H. Schreiber, and M. Leone, "Efficient multiport equivalent circuit for skin and proximity effect in parallel conductors with arbitrary cross sections," *IEEE Trans. Electromagn. Compat.*, vol. 60, no. 6, pp. 2053–2056, Dec. 2018, doi: [10.1109/TEMC.2018.2789998](https://doi.org/10.1109/TEMC.2018.2789998).
- [25] R. Faila, M. Bologna, and B. Tellini, "Dendrite growth model in battery cell combining electrode edge effects and stochastic forces into a diffusion limited aggregation scheme," *J. Power Sources*, vol. 433, no. 1, Sep. 2019, Art. no. 126675, doi: [10.1016/j.jpowsour.2019.05.081](https://doi.org/10.1016/j.jpowsour.2019.05.081).
- [26] G. J. Rees, D. Spencer Jolly, Z. Ning, Y. T. J. Marrow, G. E. Pavlovskaya, and P. G. Bruce, "Imaging sodium dendrite growth in all-solid-state sodium batteries using  $^{23}\text{Na}$   $T_2$ -weighted magnetic resonance imaging," *Angew. Chem. Int. Ed.*, vol. 60, no. 4, pp. 2110–2115, 2021, doi: [10.1002/anie.202013066](https://doi.org/10.1002/anie.202013066).
- [27] E. Boridy, "Solution of some electrostatic potential problems involving spherical conductors: A dual series approach," *IEEE Trans. Electromagn. Compat.*, vol. EMC-29, no. 2, pp. 132–140, May 1987, doi: [10.1109/TEMC.1987.304352](https://doi.org/10.1109/TEMC.1987.304352).
- [28] J. M. Aguirregabiria, A. Hernández, and M. Rivas, "An example of surface charge distribution on conductors carrying steady currents," *Amer. J. Phys.*, vol. 60, no. 2, pp. 138–141, Feb. 1992, doi: [10.1119/1.16932](https://doi.org/10.1119/1.16932).
- [29] P. A. Polyakov, N. E. Ruskova, and Y. V. Samukhina, "New solutions for charge distribution on conductor surface," *J. Electrostatics*, vol. 77, pp. 147–152, Oct. 2015, doi: [10.1016/j.elstat.2015.08.003](https://doi.org/10.1016/j.elstat.2015.08.003).
- [30] V. I. Fabrikant, E. Karapetian, and S. V. Kalinin, "Exact, approximate and asymptotic solutions of the Klein–Gordon integral equation," *J. Eng. Math.*, vol. 115, no. 1, pp. 141–156, Apr. 2019, doi: [10.1007/s10665-019-09996-4](https://doi.org/10.1007/s10665-019-09996-4).
- [31] L. D. Landau and E. M. Lifshitz, *The Classical Theory of Fields*, 4th ed. Oxford, U.K.: Pergamon, 1951.
- [32] *Matworks: Numerically Evaluate Double Integral*. Accessed: 2021. [Online]. Available: [https://www.mathworks.com/help/matlab/ref/integral\\_2.html](https://www.mathworks.com/help/matlab/ref/integral_2.html)
- [33] L. F. Shampine, "Vectorized adaptive quadrature in MATLAB," *J. Comp. Appl. Math.*, vol. 211, no. 2, pp. 131–140, Feb. 2008, doi: [10.1016/j.cam.2006.11.021](https://doi.org/10.1016/j.cam.2006.11.021).
- [34] L. F. Shampine, "MATLAB program for quadrature in 2D," *J. Comp. Appl. Math.*, vol. 202, no. 1, pp. 266–274, Aug. 2008, doi: [10.1016/j.amc.2008.02.012](https://doi.org/10.1016/j.amc.2008.02.012).



**MAURO BOLOGNA** was born in 1961.

He received the degree in physics from the University of Pisa, Pisa, Italy, in 1988, and the Ph.D. degree in physics from the Center of Nonlinear Science, University of North Texas, in 2002. From 1999 to 2003, he was with the Center of Nonlinear Science, University of North Texas. Currently, he is a Professor with the Department of Electrical and Electronic Engineering, University of Tarapacá. His main research interests include non-poissonian processes, magnetohydrodynamics, and non-linear science.



**GIANLUCA CAPOSCIUTTI** was born in Grosseto, Italy, in 1990. He received the M.S. degree in energy engineering and the Ph.D. degree in energy, systems, territory, and construction engineering from the University of Pisa, Pisa, Italy, in 2015 and 2019, respectively. He is currently a Research Fellow with the Department of Energy, Structures, Territory and Construction Engineering, University of Pisa. His research interests include characterization of batteries and electric and thermal measurements.

**KRISTOPHER J. CHANDÍA** (Member, IEEE) was born in Arica, Chile, in 1979. He received the B.S. degree in electronic engineering, the M.S. degree in telecommunications engineering, and the Ph.D. degree in science from the Universidad de Tarapacá, Arica, in 2005, 2006, and 2010, respectively. Since 2010, he has been with the Universidad de Tarapacá, where he is currently an Assistant Professor with the Department of Electrical and Electronic Engineering. Since 2006, his research interests include non-linear circuits, memristors, electromagnetic wave theory, waveguides, and optical fibers in communication systems. He is a member of the IEEE Circuits and Systems Society and the IEEE Microwave Theory and Techniques Society. Since 2012, he has been the Editor-in-Chief of *INGENIARE Revista Chilena de Ingeniería*.



**BERNARDO TELLINI** (Senior Member, IEEE) was born in Pisa, Italy, in 1969. He received the M.S. (Laurea) and Ph.D. degrees in electrical engineering from the University of Pisa, Pisa, in 1993 and 1999, respectively. Since 2000, he has been with the University of Pisa, where he is currently a Full Professor of electrical measurements with the Department of Energy, Systems, Territory and Construction Engineering. His research interests include characterization of electrical and magnetic properties of materials, aging process in battery cells, electromagnetic emission associated with fast electromagnetic transients, sensors, and transducers for pulsed power applications, measurement of position, and magneto hydrodynamics problems. He is a member of the IEEE Instrumentation and Measurement Society and the IEEE Magnetics Society. He was the Chair of European Pulsed Power Laboratories, from 2010 to 2014. He is currently the Chair of the IEEE Italy Section. He served as the general chair and the general co-chair for several IEEE conferences in the field of measurements and other IEEE technological topics.



• • •