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# A Spectral RMIL+ Conjugate Gradient Method for Unconstrained Optimization With Applications in Portfolio Selection and Motion Control

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**ABSTRACT** The Spectral conjugate gradient (SCG) methods are among the efficient variants of CG algorithms which are obtained by combining the spectral gradient parameter and CG parameter. The success of SCG methods relies on effective choices of the step-size  $\alpha_k$  and the search direction  $d_k$ . This paper presents an SCG method for unconstrained optimization models. The search directions generated by the new method possess sufficient descent property without the restart condition and independent of the line search procedure used. The global convergence of the new method is proved under the weak Wolfe line search. Preliminary numerical results are presented which show that the method is efficient and promising, particularly for large-scale problems. Also, the method was applied to solve the robotic motion control problem and portfolio selection problem.

**INDEX TERMS** Spectral algorithm, conjugate gradient algorithms, unconstrained optimization models, motion control, line search procedure, portfolio selection.

#### I. INTRODUCTION

In this paper, we consider the optimization model:

$$\min f(x), \quad x \in \mathbb{R}^n. \tag{1}$$

The function  $f : \mathbb{R}^n \to \mathbb{R}$  has continuous partial derivatives, whose gradient  $\nabla f(x) = g(x)$  is available. This type of problems often arise in economics, management science, engineering and other industrial applications [1]–[4]. The spectral conjugate algorithms are widely used to solve

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problem (1) by

$$x_{k+1} = x_k + t_k d_k, \ k \ge 0,$$
(2)

where  $x_0$  is the initial guess. The step-size  $t_k > 0$  is usually calculated along  $d_k$ . For k = 0, we have  $d_0 = -g_0$  which is known as the Steepest descent direction. However, the subsequent directions of search are recursively computed as

$$d_k = -\theta_k g_k + \beta_k d_{k-1}, \quad k \ge 1.$$
(3)

Here  $\theta_k$  is the spectral parameter and  $\beta_k$  is the conjugate gradient parameter that differentiate the types of spectral CG methods. Some of the known CG parameters are given by Hestenes-Stiefel (HS) [5], Polak-Ribiere-Polyak (PRP) [6],

[7], Liu-Storey (LS) [8], Fletcher-Reeves (FR) [9], Conjugate Descent (CD) [10], Dai-Yuan (DY) [11] whose formulas are given as follow:

$$\begin{split} \beta_k^{HS} &= \frac{g_k^I y_{k-1}}{d_{k-1}^T y_{k-1}}, \quad \beta_k^{PRP} = \frac{g_k^I y_{k-1}}{\|g_{k-1}\|^2}, \\ \beta_k^{LS} &= \frac{g_k^T y_{k-1}}{-g_{k-1}^T d_{k-1}}, \quad \beta_k^{FR} = \frac{\|g_k\|^2}{\|g_{k-1}\|^2}, \\ \beta_k^{CD} &= \frac{\|g_k\|^2}{-d_{k-1}^T g_{k-1}}, \quad \beta_k^{DY} = \frac{\|g_k\|^2}{d_{k-1}^T y_{k-1}}. \end{split}$$

In theory, when exact minimization rule is used, then, all these choices of  $\beta_k$  are equivalent for strongly convex quadratic function f. However, for non-quadratic objective functions, every  $\beta_k$  chosen leads to different numerical performances [12].

The convergence properties of these methods have been studied by various scholars. From the computational point of view, the method of PRP performed better than the FR method. Also, when f is a convex objective function, then, under the exact line search, the PRP algorithm would converge globally [6]. For the exact line search,  $t_k$  is computed to satisfy:

$$f(x_k + t_k d_k) := \min_{t \ge 0} f(x_k + t d_k).$$
(4)

However, for certain non-convex functions, Powell [13] shows that the PRP algorithm would not converge globally.

Other convergence results require the step-size  $t_k$  to satisfy the weak or strong Wolfe line search. The weak Wolfe search technique expect  $t_k$  to satisfy the inequalities.

$$f(x_k + t_k d_k) \le f(x_k) + \delta t_k g_k^T d_k.$$
(5)

$$g(x_k + \alpha_k d_k)^T d_k \ge \sigma g_k^T d_k.$$
(6)

On the other hand, the strong Wolfe (SWP) search technique except  $t_k$  to satisfy (5) and

$$g\left(x_k + t_k d_k\right)^T d_k \le -\sigma |g_k^T d_k|,\tag{7}$$

where  $0 < \delta < \sigma < 1$ . Al-Baali [14] showed that FR algorithm satisfies the sufficient descent condition:

$$g_k^T d_k \le -C \|g_k\|^2, \quad C > 0,$$
 (8)

and established the convergence proof for general function using SWP line search. For recent studies on conjugate gradient algorithms, please refer to [6], [10], [12], [13], [15]–[19].

Recently, Rivaie *et al.* [20] construct a variant of PRP method and give the formula as:

$$\beta_k^{RMIL} = \frac{g_k^T(g_k - g_{k-1})}{\|d_{k-1}\|^2},\tag{9}$$

where the authors replaced  $||g_{k-1}||^2$  with  $||d_{k-1}||^2$  in the denominator of classical PRP CG parameter and showed that the method satisfies (8) and further proved its global convergence under exact minimization condition. However, Dai [21] pointed out the use of a wrong inequality in establishing the

convergence proof of the result in [20]. As a result, Dai [21] presented a modification as:

$$\beta_k^{RMIL+} = \begin{cases} \frac{g_k^I(g_k - g_{k-1})}{\|d_{k-1}\|^2}, & \text{if } 0 \le g_k^T g_{k-1} \le \|g_k\|^2, \\ 0, & \text{otherwise,} \end{cases}$$
(10)

and studied the convergence of RMIL+ using exact minimization rule. Numerical result obtained showed that the RMIL+ is promising. More recently, Yousif [22], studied the convergence of RMIL+ method under strong Wolfe line search.

However, some of the best performing conjugate gradients algorithms, developed recently, are those that incorporated the spectral parameters. An interesting feature of the spectral CG algorithm is that only gradient directions are incorporated at every line search while a non monotone strategy usually guarantees the global convergence [23]. The first known spectral CG algorithms was defined by Birgin and Martínez [24] with the parameters defined as follows:

$$\beta_{k}^{1} = \frac{(\theta_{k}y_{k-1} - s_{k-1})^{T} g_{k}}{s_{k-1}^{T}y_{k-1}}, \quad \beta_{k}^{2} = \frac{\theta_{k}g_{k}^{T}y_{k-1}}{t_{k-1}\theta_{k-1}g_{k-1}^{T}g_{k-1}},$$
$$\beta_{k}^{3} = \frac{\theta_{k}g_{k}^{T} g_{k}}{t_{k-1}\theta_{k-1}g_{k-1}^{T}g_{k-1}},$$

where  $y_{k-1} = g_k - g_{k-1}$  and  $s_{k-1} = x_k - x_{k-1}$ . The method  $\beta_k^1$  reduces to a modified CG algorithm presented by Perry [25] if  $\theta \equiv 1$ , for all k. Moreover, if  $\theta_k \equiv 1$  holds, for all k, and  $\beta_k^2$  satisfies the exact minimization condition, then, the classical PRP CG method by Polak-Ribiere-Polyak [6] is obtained. However, if the successive gradients are orthogonal and the condition  $\theta \equiv 1$  holds, for all k, then  $\beta_k^3$  would reduce to the classical Fletcher-Reeves (FR) [9] algorithm. One of the drawbacks of this method is that  $d_k$  may not be a descent during the iteration process. Hence, restart procedure was employed in [26] to guarantee that the method has a descent direction in all iterations. The convergence analysis of this method was studied under the standard Wolfe line search. Birgin and Martínez [26] further extended their work and introduced an alternative spectral parameter:

$$\theta_k = \frac{s_{k-1}^T s_{k-1}}{s_{k-1}^T y_{k-1}}.$$
(11)

Computing the conjugate gradient coefficients  $\beta_k$  (11) with the spectral parameter in (11) leads to the spectral conjugate gradient (SCG) method. Numerical results obtained under various line search procedures illustrate that the SCG is more efficient compared to the classical methods of PRP [6], FR [9], Perry [25] and the spectral gradient method [27]. More work have been done to improve these methods. Recent research focuses on memoryless BFGS updates for unconstrained optimization [15], [28]–[31]. Another efficient spectral FR (sFR) conjugate gradient method was introduced by Zhang *et al.*, [32] with the spectral parameter  $\theta_k$  and conjugate gradient parameter  $\beta_k$  defined as:

$$\beta_k = \beta_k^{FR} = \frac{\|g_k\|^2}{\|g_{k-1}\|} , \ \theta_k = \frac{d_{k-1}^T y_{k-1}}{\|g_{k-1}\|^2}.$$
(12)

An interesting feature of sFR parameter is that, independent of line search procedures employed,  $d_k$  satisfies  $g_k^T d_k = -\|g_k\|^2$ ,  $\forall k \ge 0$ . Also, the parameter reduces to classical FR parameter provided the exact minimization condition is satisfied [29]. The convergence analysis was discussed under a modified Armijo line search and results obtained from numerical computations showed that sFR method is efficient and promising compare to PRP method. Recently, Liu *et al.* [33] extended the work of Birgin and Martinez, [24] and Zhang *et al.*, [32] to proposed a general spectral parameter that will reduce to the main CG algorithm if an exact line search is used. Under some mild conditions, the authors established the global convergence of the method. For more references on recent spectral conjugate gradient method, please refer to [33]–[39].

Motivated by the above contributions, a new spectral conjugate gradient method is developed in this paper. Some of the contributions of this paper are highlighted as follows:

- A new spectral conjugate gradient algorithm, based on RMIL+, for solving unconstrained optimization is developed.
- The search direction generated by the new algorithm satisfies the sufficient descent property without the restart condition and independent of any line search.
- The global convergence of the new method is proved under the weak Wolfe line search.
- The efficiency of the new algorithm is demonstrated on some standard large-scale problems.
- The new algorithm is applied to solve problems arising from portfolio selection.
- Lastly, the new algorithm is successfully applied to deal with robotic motion control problem.

The rest of the paper is designed as follows. In Section II, a new spectral parameter is presented and the corresponding algorithm is given. The global convergence results of the new formula under the weak Wolfe line search is presented in Section III. Experimental numerical results are presented in Section IV. Applications of the new algorithm in portfolio selection and motion control are discussed in Sections V and VI, respectively, where the finally conclusion in section VII.

## **II. NEW ALGORITHM**

In this section, inspired by the idea of Birgin and Martinez, [24] and Zhang *et al.*, [40], we propose an efficient spectral parameter as follows.

Consider the sequence  $\{x_k\}$  computed using the spectral CG parameter (2) and (3). Multiplying (3) by  $g_k^T$  gives

$$g_k^T d_k = -\theta_k g_k + \beta_k g_k^T d_{k-1} = \frac{g_{k-1}^I d_{k-1}}{\|d_{k-1}\|^2} \|g_k\|^2 \psi_k, \quad (13)$$

where,

$$\psi_k = -\frac{\|d_{k-1}\|^2}{g_{k-1}^T d_{k-1}} \theta_k + \beta_k \frac{\|d_{k-1}\|^2}{g_{k-1}^T d_{k-1}} \frac{g_k^T d_{k-1}}{\|g_k\|^2}.$$

This implies,

$$\frac{g_k^T d_k}{\|g_k\|^2} = \frac{g_{k-1}^T d_{k-1}}{\|d_{k-1}\|^2} \psi_k.$$
(14)

Suppose for every  $k \ge 1$ , we choose the parameter  $\psi_k = 1$ , then from (3) and (14), we get

$$\frac{g_k^T d_k}{\|g_k\|^2} = \frac{g_{k-1}^T d_{k-1}}{\|d_{k-1}\|^2} = \dots = \frac{g_0^T d_0}{\|d_0\|^2} = -1.$$
 (15)

From (15), we have

$$g_k^T d_k = -\|g_k\|^2, \quad \forall k \ge 1.$$
 (16)

Thus, if we choose the spectral parameter  $\theta_k$  to satisfy  $\psi_k \equiv 1$ , then, the direction of search will always satisfy the descent condition regardless of the search procedure used. This analysis motivated us on defining a new parameter  $\theta_k$  as follows.

$$\theta_k = -\frac{g_{k-1}^T d_{k-1}}{\|d_{k-1}\|^2} + \beta_k \frac{g_k^T d_{k-1}}{\|g_k\|^2},\tag{17}$$

where  $k \ge 1$  and  $\psi \equiv 1$ .

The algorithm of our spectral conjugate method is as follows.

## Algorithm 1 sRMIL+ Method

Step 1. Initialization: given  $x_0 \in \mathbb{R}^n$ ,  $\sigma > 0$ ,  $\psi_k > 0$ , set k := 0. If  $||g_k|| \le \epsilon$ , stop. Otherwise, Step 2. Compute  $\beta_k$  by (10). Step 3. Compute  $d_k$  using (3) where  $\theta_k$  is defined in (17). Step 4. Determine  $t_k$  based on (5) and (6). Step 5. Update new iterate based on (2). Step 6. Check if  $||g_k|| = 0$ , terminate. Else, go to step 2 with k = k + 1.

To analyze the convergence of the conjugate gradient method, the assumptions below are often needed. *Assumption A:* 

- 1) f(x) is bounded from below on the level set  $\Omega = \{x \in \mathbb{R}^n | f(x) \le f(x_0) \}.$
- 2) In some neighborhood N of  $\Omega$ , f is smooth and g(x) is Lipchitz continuous on an open convex set N that contains  $\Omega$ , such that, there exist L > 0 (constant) satisfying;

$$||g(x) - g(y)|| \le L ||x - y||, \quad \forall x, y \in N.$$
(18)

Remark 1: From the analysis above, we have shown that the proposed sRMIL+ satisfies the descent condition (16) regardless of the line search. This condition would play a significant part in the convergence of the proposed sRMIL+ algorithm.

## **III. CONVERGENCE ANALYSIS**

The global convergence properties of sRMIL+ under weak Wolfe line search will be studied in this section. Consider the CG parameter defined by (10). If the condition  $0 \le g_k^T g_{k-1} \le ||g_k||^2$ , holds then

$$\beta_k^{RMIL+} = \frac{\|g_k\|^2 - g_k^T g_{k-1}}{\|d_{k-1}\|^2} \le \frac{\|g_k\|^2}{\|d_{k-1}\|^2}$$

where the inequality is obtained by dropping the second term since  $g_k^T g_{k-1} \ge 0$ . On the other hand, it also holds that the condition  $0 \le g_k^T g_{k-1} \le ||g_k||^2$  is equivalent to  $-||g_k||^2 \ge -g_k^T g_{k-1}$ . Therefore

$$\beta_k^{RMIL+} = \frac{\|g_k\|^2 - g_k^T g_{k-1}}{\|d_{k-1}\|^2} \ge \frac{\|g_k\|^2 - \|g_k\|^2}{\|d_{k-1}\|^2} = 0.$$

Hence, it holds that

$$0 \le \beta_k^{RMIL+} \le \frac{\|g_k\|^2}{\|d_{k-1}\|^2}, \ \forall k \ge 1.$$
 (19)

The proofs would be based on the above inequality (19).

Consider the Assumptions A, then, there exists a constant  $\gamma > 0$ , in such a way that we have

$$\|g_k\| \le \gamma, \quad \forall k \in \mathbb{N}.$$

The lemma that follows is based on Zoutendijk [18] condition and has been extensively used in the global convergence analysis of different CG methods.

Lemma 1: Let's suppose Assumption A is true. For CG iterative method defined by (2) and (3), where the search direction  $d_k$  satisfies

$$g_k^T d_k < 0,$$

for  $k \in \mathbb{N}$  and step-size  $t_k$  follows from the weak Wolfe line search, then,

$$\sum_{k=0}^{\infty} \frac{(g_k^T d_k)^2}{\|d_k\|^2} < +\infty.$$
(21)

The proof of this Lemma follows from [17]. From (19) and using Lemma 1, we have the following convergence theorem.

Theorem 1: Suppose Assumption A holds. Consider the sequence  $\{g_k\}$  and  $\{d_k\}$  follows from the proposed algorithm, where  $\beta_k$  is given by (19), and  $t_k$  satisfies the weak Wolfe line search, then,

$$\frac{\|d_k\|^2}{\|g_k\|^4} \le \sum_{i=0}^k \frac{1}{\|g_i\|}.$$
(22)

*Proof:* Applying Cauchy-Schwarz inequality on the descent condition (16), we deduce

$$|d_k\| \ge \|g_k\| \quad \Longrightarrow \quad \frac{1}{\|d_k\|} \le \frac{1}{\|g_k\|}. \tag{23}$$

Now, from (16), (3) and (17), we have

$$d_{k} = \frac{g_{k-1}^{T} d_{k-1}}{\|d_{k-1}\|^{2}} g_{k} - \beta_{k} \frac{g_{k}^{T} d_{k-1}}{\|g_{k}\|^{2}} g_{k} + \beta_{k} d_{k-1}$$
  
$$= -\frac{\|g_{k-1}\|^{2}}{\|d_{k-1}\|^{2}} g_{k} - \beta_{k} \frac{g_{k}^{T} d_{k-1}}{\|g_{k}\|^{2}} g_{k} + \beta_{k} d_{k-1}$$
  
$$= -\frac{\|g_{k-1}\|^{2}}{\|d_{k-1}\|^{2}} g_{k} + \beta_{k} \left(I - \frac{g_{k} g_{k}^{T}}{\|g_{k}\|^{2}}\right) d_{k-1}.$$
(24)

Next, applying norm on both sides of (24) and using (23) gives

$$\begin{aligned} \|d_{k}\| &\leq \frac{\|g_{k-1}\|^{2}}{\|d_{k-1}\|^{2}} \|g_{k}\| + \beta_{k} \left\| I - \frac{g_{k}g_{k}^{T}}{\|g_{k}\|^{2}} \right\| \|d_{k-1}\| \\ &\leq \frac{\|g_{k-1}\|^{2}}{\|g_{k-1}\|^{2}} \|g_{k}\| + \beta_{k} \left\| I - \frac{g_{k}g_{k}^{T}}{\|g_{k}\|^{2}} \right\| \|d_{k-1}\| \\ &\leq \|g_{k}\| + \beta_{k} \left\| I - \frac{g_{k}g_{k}^{T}}{\|g_{k}\|^{2}} \right\| \|d_{k-1}\| \\ &= \|g_{k}\| + \beta_{k} \|d_{k-1}\|. \end{aligned}$$
(25)

Squaring both sides and using (19) and (23) yields

$$\begin{aligned} \|d_{k}\|^{2} &\leq \left(\|g_{k}\| + \beta_{k}\|d_{k-1}\|\right)^{2} \\ &= \|g_{k}\|^{2} + 2\beta_{k}\|g_{k}\|\|d_{k-1}\| + \beta_{k}^{2}\|d_{k-1}\|^{2} \\ &\leq \|g_{k}\|^{2} + 2\frac{\|g_{k}\|^{2}}{\|d_{k-1}\|^{2}}\|g_{k}\|\|d_{k-1}\| + \frac{\|g_{k}\|^{4}}{\|d_{k-1}\|^{4}}\|d_{k-1}\|^{2} \\ &= \|g_{k}\|^{2} + 2\frac{\|g_{k}\|^{3}}{\|d_{k-1}\|} + \frac{\|g_{k}\|^{4}}{\|d_{k-1}\|^{2}} \\ &\leq \|g_{k}\|^{2} + 2\frac{\|g_{k}\|^{3}}{\|g_{k-1}\|} + \frac{\|g_{k}\|^{4}}{\|g_{k-1}\|^{2}} \\ &\leq \frac{\|g_{k}\|^{4}}{\|g_{k}\|^{2}} + 2\frac{\|g_{k}\|^{3}}{\|g_{k-1}\|} + \frac{\|g_{k}\|^{4}}{\|g_{k-1}\|^{2}}. \end{aligned}$$
(26)

Rearranging gives

$$\frac{\|d_k\|^2}{\|g_k\|^4} \le \frac{1}{\|g_k\|^2} + 2\frac{1}{\|g_k\|\|g_{k-1}\|} + \frac{1}{\|g_{k-1}\|^2} = \left(\frac{1}{\|g_k\|} + \frac{1}{\|g_{k-1}\|}\right)^2.$$
(27)

$$\frac{\|d_k\|^2}{\|g_k\|^4} \le \left(\frac{1}{\|g_k\|} + \frac{1}{\|g_{k-1}\|}\right)^2 \le \sum_{i=0}^k \frac{1}{\|g_i\|}.$$
 (28)

The proof is completed.

Theorem 2: Suppose Assumption A holds true. Consider the sequence  $\{g_k\}$  and  $\{d_k\}$  generated by the proposed method, where  $\beta_k$  is given by (19), and  $t_k$  satisfies the weak Wolfe line search, then,

$$\lim_{k \to \infty} \inf \|g_k\| = 0.$$
<sup>(29)</sup>

*Proof:* The proof of Theorem 2 would be done by contradiction. That is, if the conclusion of Theorem 2 is not true, then, there exist a constant c > 0 in such a way that

$$\|g_k\|^2 \ge c, \quad \forall k \ge 1. \tag{30}$$

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TABLE 1.	List of test	functions,	dimensions,	and	initial	points
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Number	Functions	Dimension	Initial Points
1	Extended Rosenbrock	1,000	(-1.2, 1,,-1.2,1)
2	Extended Rosenbrock	1,000	(10,,10)
3	Extended Rosenbrock	10,000	(-1.2, 1,,-1.2,1)
4	Extended Rosenbrock	10,000	(5,,5)
5	Diagonal 4	500	(1,, 1)
6	Diagonal 4	500	(-20,, -20)
7	Diagonal 4	1.000	(1, 1)
8	Diagonal 4	1.000	(-3030)
9	Hager	10	(1, 1)
10	Hager	10	(-1010)
11	Trecanni	2	(-1, 0, 5)
12	Trecanni	2	(-5, 10)
13	Shallow	1 000	(0, 10)
13	Shallow	1,000	(0,,0)
15	Shallow	10,000	(-1, -1)
16	Shallow	10,000	(-10, -10)
10	Leon	2	(-10,, -10)
17	Leon	$\frac{2}{2}$	(2,2) (8.8)
10	Evtended Powel	100	(0,0)
19	Extended Powel	100	(5,-1,0,1,)
20	Extended Power	1 000	(3,,3)
21	Extended Deale	1,000	$(1, 0.0, \dots, 1, 0.0)$
22	Extended Deale	1,000	(0.3,, 0.3)
25	Extended Deale	10,000	$(-1, \dots, -1)$
24	Extended Beale	10,000	(0.3,,0.3)
25	Six Hump Camel	2	(-1,2)
26 27	Six Hump Camel	2	(-5, 10)
27	Three Hump Camel	2	(-1,2)
28	Inree Hump Camel	2	(2,-1)
29	POWER	10	(1,,1)
30	POWER	10	(10,, 10)
31	Colville	4	(2,2,2,2)
32	Colville	4	(10,10,10,10)
33	Dixon and Price	3	(1, 1, 1)
34	Dixon and Price	3	(10, 10, 10)
35	Sphere	5,000	(1,,1)
36	Sphere	5,000	(10,,10)
37	Sum Squares	50	(0,1,,0,1)
38	Sum Squares	50	(10,, 10)
39	NONSCOMP	2	(3,3)
40	NONSCOMP	2	(10, 10)
41	Extended DENSCHNB	10	(1,, 1)
42	Extended DENSCHNB	10	(10,, 10)
43	Extended DENSCHNB	100	(10,, 10)
44	Extended DENSCHNB	100	(-50,, -50)
45	Extended Penalty	10	(1, 2,, 10)
46	Extended Penalty	10	(-10,, -10)
47	Extended Penalty	100	(1,,1)
48	Extended Penalty	100	(-2,, -2)
49	ENGVAL1	50	(2,,2)
50	ENGVAL1	100	(2,,2)
51	ENGVAL8	50	(0,,0)
52	ENGVAL8	100	(0,,0)

TABLE 1.	(Continued.) List of test functions,	dimensions,	and initial	points.
	(			P 0

53	Extended White & Holst	1,000	(-1.2, 1,,-1.2,1)
54	Extended White & Holst	1,000	(10,,10)
55	Extended White & Holst	10,000	(-1.2, 1,,-1.2,1)
56	Extended White & Holst	10,000	(5,,5)
57	Extended Tridiagonal 1	500	(2,, 2)
58	Extended Tridiagonal 1	500	(10,, 10)
59	Extended Tridiagonal 1	1,000	(1,, 1)
60	Extended Tridiagonal 1	1,000	(-10,, -10)
61	FLETCHCR	10	(0,, 0)
62	FLETCHCR	10	(10 10)
63	Zettl	2	(-1, 2)
64	Zettl	2	(10, 10)
65	Ouartic	4	(10.10.10.10)
66	Ouartic	4	(15.15.15.15)
67	Generalized Tridiagonal 1	10	(2 2)
68	Generalized Tridiagonal 1	10	(10,, 10)
69	Ext Freudenstein & Roth	10,000	(-5, -5)
70	Ext Freudenstein & Roth	50,000	(-5, -5)
70	Extended Himmelblau	1,000	(1, 1)
72	Extended Himmelblau	1,000	(20, 20)
73	Extended Himmelblau	10,000	(20,,20)
74	Extended Himmelblau	10,000	(50, 50)
75	Extended Maratos	10,000	(1101 11)
76	Extended Maratos	10	(1.1, 0.1,, 1.1, )
70	Booth	10	(-1,, -1) (5, 5)
78	Booth	$\frac{2}{2}$	(3, 3)
70	Quadratic OE2	50	(10, 10)
80	Quadratic QF2	50	(0.3,, 0.3)
81	Matyas	50 2	(30,, 30)
82	Matyas	$\frac{2}{2}$	(1, 1) (20, 20)
82	Ouedratic OE1	50	(20, 20) (1, 1)
83 94	Quadratic QF1	50	(1,,1)
04 05	Quadratic QF1	500	(10,, 10)
85	Quadratic QF1	500	(1,,1)
80 97	Quadratic QL1 Constalized Tridiagonal 2	500	$(-3, \dots, -3)$
07	Constant and Tridiagonal 2	4	(1,1,1,1) (10,10,10,10)
00	Deneralized Indiagonal 2	4	(10, 10, 10, 10)
09	Raydan 1	10	(1,,1)
90	Raydan 1	10	$(-10, \dots, -10)$
91	Raydan 1	100	$(-1, \dots, -1)$
92	Kayuali I	1.000	(-10,, -10)
95	Concretized Quartic	1,000	(3,,3)
94	Enternale d'Ora dantia Danalta OD1	1,000	$(20, \dots, 20)$
95	Extended Quadratic Penalty QP1	4	(1,1,1,1)
90	Extended Quadratic Penalty QP1	4	(10, 10, 10, 10)
9/	Extended Quadratic Penalty QP2	100	(1,,1)
98	Extended Quadratic Penalty QP2	100	(10,, 10)
99 100	Extended Quadratic Penalty QP2	500	(10,, 10)
100	Extended Quadratic Penalty QP2	500	(20,, 20)
101	QUARTICM	5,000	(2,,2)
102	QUARTICM	10,000	(2,,2)
103	QUARTICM	15,000	(2,,2)
104	QUARTICM	20,000	(2,,2)
105	DENSCHNA	10,000	(-1,,-1)

106	DENSCHNA	100,000	(-1,,-1)
107	DENSCHNC	5,000	(100,,100)
108	DENSCHNC	50,000	(100,,100)
109	Extended Block-Diagonal BD1	5,000	(1.02,,1.02)
110	Extended Block-Diagonal BD1	50,000	(1.02,,1.02)
111	Extended Block-Diagonal BD1	100,000	(1.02,,1.02)
112	HIMMELBH	50	(0.2,,0.2)
113	HIMMELBH	100	(0.2,,0.2)
114	HIMMELBH	1,000	(0.2,,0.2)
115	Extended Hiebert	10,000	(1.04,, 1.04)
116	Extended Hiebert	50,000	(1.04,, 1.04)
117	Extended Hiebert	100,000	(1.04,, 1.04)
118	Price 4	2	(-2,-2)
119	Price 4	2	(3,-2)
120	Rotated Ellipse	2	(-2,-2)
121	Rotated Ellipse	2	(0.2,0.2)
122	Zirilli or Aluffi-Pentini's	2	(2,2)
123	Zirilli or Aluffi-Pentini's	2	(-2,-2)
124	Diagonal Double Border Arrow Up	500	(1.005,,1.005)
125	Diagonal Double Border Arrow Up	5,000	(1.005,,1.005)
126	Diagonal Double Border Arrow Up	50,000	(1.005,,1.005)
127	HARKERP	1,000	(1,,1000)
128	HARKERP	50,000	(1,2,,50000)
129	Extended Quadratic Penalty QP3	10	(15,15,,15)
130	Extended Quadratic Penalty QP3	100	(15,15,,15)

 TABLE 1. (Continued.) List of test functions, dimensions, and initial points.

From Theorem 1, we have

$$\frac{\|d_k\|^2}{\|g_k\|^4} \le \frac{k+1}{c},\tag{31}$$

which implies

$$\sum_{k=0}^{\infty} \frac{\|g_k\|^4}{\|d_k\|^2} \ge \sum_{k=0}^{\infty} \frac{c}{k+1} = \infty.$$
 (32)

However, since (16) hold true, then, from (21), we obtain

$$\sum_{k=0}^{\infty} \frac{\|g_k\|^4}{\|d_k\|^2} = \sum_{k=0}^{\infty} \frac{(g_k^T d_k)^2}{\|d_k\|^2} < \infty.$$
(33)

It is clear that (32) and (33) yield contradiction. This implies that (29) holds and thus completes the proof.  $\Box$ 

## **IV. PRELIMINARY RESULTS**

This section presents the numerical results on 130 benchmark test problems to illustrate the efficiency of the proposed sRMIL+ method and compare the performance with the RMIL+ method [21], PRP method [6], [7], sFR method [40], and sPRP method [33]. These algorithms were coded in MAT-LAB R2019a and compiled with personal laptop; Intel Core i7 processor, 16 GB RAM, 64bit Windows 10 Pro operating system. A large number of the benchmark functions and initial points are considered by Andrei [41] and Jamil-Yang [42] as in Table 1. The dimensions of our test problems ranging from 2 to 100,000. All the methods are implemented using the weak Wolfe line search with  $\delta = 0.0001$ ,  $\sigma = 0.001$  and the termination criteria was set as  $||g_k|| \le 10^{-6}$ . We use "F" to denote when the iteration is bigger than 10,000 or never reach the optimal point.

All numerical results are presented in Table 2 and Table 3, where NOI represents the number of iterations, NOF represents the number of function evaluations, and CPU represents the central processing unit time. Tables 2 and 3 show that all methods failed to successfully solve the ENGVAL8 function with dimension 100, and for all, we get that the RMIL+ method solves 73% (95 out of 130), the PRP method 71% (93 out of 130), the sFR method 85% (111 out of 130), sPRP, and sRMIL+ methods 96% (125 out of 130). So, this is indicating that the sRMIL+ method is superior at solving the test problems considered compared with RMIL, PRP, and sFR methods. However, the sRMIL+ method is competitive with the sPRP method.

On the other hand, to compare and visually characterize the numerical results in Tables 2 and 3, we use the performance profile tool of Dolan and Moré [43] to describe the performance of the RMIL+, PRP, sFR, sPRP, and sRMIL+ methods based on the NOI, NOF, and CPU time, respectively. Let *S* is set of solvers, *P* is test problems, for  $n_s$  solvers and  $n_p$  problems, the performance profile  $\xi : \mathbb{R} \rightarrow [0, 1]$  is formulated as follows:

$$\xi(\tau) := \frac{1}{n_p} size \{ p \in P_l | \log_2(r_{p,s}) \le \tau \}, \quad \forall \tau \in \mathbb{R}^+,$$

## TABLE 2. Numerical results of RMIL+, PRP, and sFR methods.

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$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	Number		RMII	_ <del>+</del>		PRP		sFR			
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		NOI	NOF	CPU	NOI	NOF	CPU	NOI	NOF	CPU	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1	27	176	0.0488	19	123	0.0377	179	293	0.1955	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2	40	243	0.0667	F	F	F	163	1181	0.2378	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3	32	192	0.3874	19	123	0.231	200	986	1.6746	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4	40	195	0.3768	20	136	0.4796	831	5101	8.4652	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	5	F	F	F	F	F	F	31	90	0.0254	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	6	F	F	F	F	F	F	56	165	0.0392	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7	F	F	F	F	F	F	39	114	0.053	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	8	F	F	F	F	F	F	64	189	0.0549	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	9	F	F	F	F	F	F	34	105	0.0048	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10	F	F	F	F	F	F	89	309	0.0091	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	1	3	0.0013	1	3	1.95E-04	1	3	1.88E-04	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	12	5	23	0.007	5	23	6.89E-04	7	30	7.20E-04	
14       14       59       0.0303       13       51       0.018       96       389       0.0928         15       F       F       F       F       F       F       F       47       149       0.3167         16       F       F       F       F       F       F       F       372       1298       2.4379         17       31       179       0.0023       17       136       0.0012       66       363       0.0035         18       35       265       0.0033       28       243       0.0032       709       4235       0.0522         19       70       863       0.0716       3337       10084       0.7111       5589       16877       1.0729         20       39       225       0.0443       2312       7053       0.4623       6019       18187       1.2789         21       52       14       48       0.2153       F       F       F       87       288       1.1917         24       F       F       F       F       F       F       F       7       96       0.1033         26       11       66       0.0026 </td <td>13</td> <td>11</td> <td>39</td> <td>0.0154</td> <td>F</td> <td>F</td> <td>F</td> <td>55</td> <td>171</td> <td>0.0483</td>	13	11	39	0.0154	F	F	F	55	171	0.0483	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	14	14	59	0.0303	13	51	0.018	96	389	0.0928	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	15	F	F	F	F	F	F	47	149	0.3167	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	16	F	F	F	F	F	F	372	1298	2.4379	
18       35       265       0.0033       28       243       0.0032       709       4235       0.0522         19       70       863       0.0716       3337       10084       0.7111       5589       16877       1.0729         20       39       225       0.0443       2312       7053       0.4623       6019       18187       1.2789         21       52       191       0.0992       15       69       0.0479       75       249       0.1303         22       F       F       F       9       44       0.0367       81       267       0.1455         23       11       48       0.2153       F       F       F       87       288       1.1917         24       F       F       F       F       F       F       F       F       796       0.0133         26       11       66       0.0026       F	17	31	179	0.0023	17	136	0.0012	66	363	0.0035	
19708630.07163337100840.71115589168771.072920392250.0443231270530.46236019181871.278921521910.099215690.0479752490.130322FFFF9440.0367812670.14552311480.2153FFF872881.191724FFFF10470.222872851.2099258360.00536300.00727960.01032611660.0026FFFFFF28154000.0108FFFFFF291233690.010210307.66E-0410309.52E-04301394170.012310308.78E-0410309.73E-0431103243390.07261488180.2155FFF3266928190.0324863720.0167130.007134130.0056130.0071130.005735FFFFFF934050.018137461380.015225750.0067	18	35	265	0.0033	28	243	0.0032	709	4235	0.0522	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	19	70	863	0.0716	3337	10084	0.7111	5589	16877	1.0729	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20	39	225	0.0443	2312	7053	0.4623	6019	18187	1.2789	
22FFF944 $0.0367$ 81267 $0.1455$ 231148 $0.2153$ FFF87288 $1.1917$ 24FFFF1047 $0.222$ 87285 $1.2099$ 25836 $0.0053$ 630 $0.007$ 2796 $0.0103$ 261166 $0.0026$ FFFFFF2815400 $0.0108$ FFFFFF29123369 $0.0102$ 1030 $7.66E-04$ 1030 $9.52E-04$ 30139417 $0.0123$ 1030 $8.78E-04$ 1030 $9.73E-04$ 3110324339 $0.0726$ 148818 $0.2155$ FFF326692819 $0.0324$ 86372 $0.0167$ 3 $169$ $0.0029$ 3313 $0.0083$ 13 $0.0071$ 13 $0.0057$ 35FFFFFF122 $0.0013$ 3646194 $0.0083$ 56266 $0.0063$ 25122 $0.0013$ 3746138 $0.0152$ 2575 $0.0057$ 2575 $0.0043$ 3881243 $0.2223$ 41123 $0.0097$ 41123 $0.0181$ 3954193 $0.018$	21	52	191	0.0992	15	69	0.0479	75	249	0.1303	
2311480.2153FFF872881.191724FFFF10470.222872851.2099258360.00536300.00727960.01032611660.0026FFFFFF28154000.0108FFFFFF291233690.010210307.66E-0410309.52E-04301394170.012310308.78E-0410309.73E-0431103243390.07261488180.2155FFF3266928190.0324863720.0167331690.002933130.0083130.0071130.005735FFFFF16602.10E-0336461940.0083562660.0063251220.001337461380.015225750.005725750.004338812430.2223411230.0097411230.0115416228.45E-045194.20E-039310.0012428370.00228370.00231149	22	F	F	F	9	44	0.0367	81	267	0.1455	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	23	11	48	0 2153	F	F	5.5557 F	87	288	1 1917	
258360.00536300.00727960.01032611660.0026FFFF53620700.043827FFFFFFFFFFF28154000.010210307.66E-0410309.52E-04301394170.012310308.78E-0410309.73E-0431103243390.07261488180.2155FFF3266928190.0324863720.0167331690.002933130.0083130.0071130.005734130.0056130.0071130.005735FFFFFF16602.10E-0336461940.0083562660.0063251220.001337461380.015225750.00481566370.018139541930.018315760.00481566370.0124017940.2085FFF934050.0115416228.45E-045194.20E-039310.0017438370.0022837	23	F	F	6.2155 F	10	47	0 222	87	285	1 2099	
25365656565060.007275060.0105261166 $0.0026$ FFFFFFFF2815400 $0.0108$ FFFFFFFF29123369 $0.0102$ 10307.66E-0410309.52E-0430139417 $0.0123$ 10308.78E-0410309.73E-043110324339 $0.0726$ 148818 $0.2155$ FFF326692819 $0.0324$ 86372 $0.0167$ 13 $0.0071$ 3413 $0.0056$ 13 $0.0071$ 13 $0.0057$ 35FFFFFF1660 $2.10E-03$ 3646194 $0.0083$ 56266 $0.0063$ 25122 $0.013$ 3746138 $0.0152$ 2575 $0.0057$ 2575 $0.0043$ 3881243 $0.2223$ 41123 $0.0097$ 41123 $0.0181$ 3954193 $0.0183$ 1576 $0.0048$ 156637 $0.0136$ 401794 $0.2085$ FFFF93405 $0.0115$ 41622 $8.45E-04$ 519 $4.20E-03$ 931 $0.0012$ <td>25</td> <td>8</td> <td>36</td> <td>0.0053</td> <td>6</td> <td>30</td> <td>0.222</td> <td>27</td> <td>96</td> <td>0.0103</td>	25	8	36	0.0053	6	30	0.222	27	96	0.0103	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	25	11	50 66	0.0035	F	50 F	0.007 F	536	2070	0.0103	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20	F	F	0.0020 F	F	F	F	550 F	2070 F	0.0450 F	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	28	15	400	0.0108	F	F	F	F	F	F	
20123503 $0.0102$ 1030 $1.02104$ 1030 $9.02104$ 30139417 $0.0123$ 1030 $8.78E-04$ 1030 $9.73E-04$ 3110324339 $0.0726$ 148818 $0.2155$ FFF326692819 $0.0324$ 86372 $0.0167$ 33169 $0.0029$ 3313 $0.0083$ 13 $0.0071$ 13 $0.0071$ 3413 $0.0056$ 13 $0.0071$ 13 $0.0057$ 35FFFFFF66 $2.10E-03$ 3646194 $0.0083$ 56266 $0.0063$ 25122 $0.013$ 3746138 $0.0152$ 2575 $0.0057$ 2575 $0.0043$ 3881243 $0.2223$ 41123 $0.0097$ 41123 $0.0181$ 3954193 $0.0183$ 1576 $0.0048$ 156637 $0.0136$ 401794 $0.2085$ FFFF93405 $0.0115$ 41622 $8.45E-04$ 519 $4.20E-03$ 931 $0.0012$ 42837 $0.0022$ 837 $0.0023$ 1149 $0.017$ 43837 $0.0093$ 837 $0.0044$ 1149 $0.017$ <tr< td=""><td>20</td><td>123</td><td>369</td><td>0.0100</td><td>10</td><td>30</td><td>7 66F-04</td><td>10</td><td>30</td><td>9 52E-04</td></tr<>	20	123	369	0.0100	10	30	7 66F-04	10	30	9 52E-04	
3010310	30	139	417	0.0102	10	30	8 78F-04	10	30	9.73E-04	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	31	1032	4330	0.0726	148	818	0.2155	F	F	5.75E 04 F	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	32	669	2819	0.0720	86	372	0.0167	33	169	0 0029	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	33	1	3	0.0024	1	3	0.0167	1	3	0.002)	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	34	1	3	0.0005	1	3	0.0071	1	3	0.0071	
36 $46$ $194$ $0.0083$ $56$ $266$ $0.0063$ $25$ $122$ $0.0013$ $37$ $46$ $138$ $0.0152$ $25$ $75$ $0.0057$ $25$ $75$ $0.0043$ $38$ $81$ $243$ $0.2223$ $41$ $123$ $0.0097$ $41$ $123$ $0.0181$ $39$ $54$ $193$ $0.0183$ $15$ $76$ $0.0048$ $156$ $637$ $0.0136$ $40$ $17$ $94$ $0.2085$ $F$ $F$ $F$ $93$ $405$ $0.0115$ $41$ $6$ $22$ $8.45E-04$ $5$ $19$ $4.20E-03$ $9$ $31$ $0.0012$ $42$ $8$ $37$ $0.0022$ $8$ $37$ $0.0023$ $11$ $49$ $0.0017$ $43$ $8$ $37$ $0.0093$ $8$ $37$ $0.0044$ $11$ $49$ $0.0017$ $44$ $9$ $43$ $0.0181$ $7$ $37$ $0.0032$ $63$ $223$ $0.0257$ $45$ $27$ $112$ $0.0038$ $31$ $117$ $0.0017$ $20$ $76$ $0.0027$ $46$ $26$ $103$ $0.0021$ $9$ $46$ $6.12E-04$ $19$ $74$ $0.0018$ $47$ $19$ $87$ $0.0056$ $12$ $82$ $0.006$ $F$ $F$ $F$ $48$ $19$ $89$ $0.0124$ $13$ $87$ $0.0077$ $F$ $F$ $F$ $49$ $47$ $817$ $0.0301$ $22$ $409$ </td <td>35</td> <td>F</td> <td>F</td> <td>0.0050 F</td> <td>F</td> <td>F</td> <td>5.0071 F</td> <td>16</td> <td>60</td> <td>2 10E-03</td>	35	F	F	0.0050 F	F	F	5.0071 F	16	60	2 10E-03	
37 $46$ $138$ $0.0152$ $25$ $75$ $0.0057$ $25$ $75$ $0.0043$ $38$ $81$ $243$ $0.2223$ $41$ $123$ $0.0097$ $41$ $123$ $0.0181$ $39$ $54$ $193$ $0.0183$ $15$ $76$ $0.0048$ $156$ $637$ $0.0136$ $40$ $17$ $94$ $0.2085$ $F$ $F$ $F$ $93$ $405$ $0.0115$ $41$ $6$ $22$ $8.45E-04$ $5$ $19$ $4.20E-03$ $9$ $31$ $0.0012$ $42$ $8$ $37$ $0.0022$ $8$ $37$ $0.0023$ $11$ $49$ $0.0017$ $43$ $8$ $37$ $0.0093$ $8$ $37$ $0.0032$ $63$ $223$ $0.0257$ $45$ $27$ $112$ $0.0038$ $31$ $117$ $0.0017$ $20$ $76$ $0.0027$ $46$ $26$ $103$ $0.0021$ $9$ $46$ $6.12E-04$ $19$ $74$ $0.0018$ $47$ $19$ $87$ $0.0056$ $12$ $82$ $0.006$ $F$ $F$ $F$ $48$ $19$ $89$ $0.0124$ $13$ $87$ $0.0077$ $F$ $F$ $F$ $49$ $47$ $817$ $0.0301$ $22$ $409$ $0.0147$ $23$ $431$ $0.019$ $50$ $F$ $49$ $47$ $817$ $0.0301$ $22$ $409$	36	46	194	0.0083	56	266	0.0063	25	122	0.0013	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	37	46	138	0.0003	25	200 75	0.00057	25	75	0.0013	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	38	81	243	0.2223	25 41	123	0.0097	25 41	123	0.0181	
35 $51$ $153$ $0.0105$ $15$ $16$ $0.0016$ $150$ $0.017$ $40$ $17$ $94$ $0.2085$ $F$ $F$ $F$ $F$ $93$ $405$ $0.0115$ $41$ $6$ $22$ $8.45E-04$ $5$ $19$ $4.20E-03$ $9$ $31$ $0.0012$ $42$ $8$ $37$ $0.0022$ $8$ $37$ $0.0023$ $11$ $49$ $0.0017$ $43$ $8$ $37$ $0.0093$ $8$ $37$ $0.0044$ $11$ $49$ $0.01$ $44$ $9$ $43$ $0.0181$ $7$ $37$ $0.0032$ $63$ $223$ $0.0257$ $45$ $27$ $112$ $0.0038$ $31$ $117$ $0.0017$ $20$ $76$ $0.0027$ $46$ $26$ $103$ $0.0021$ $9$ $46$ $6.12E-04$ $19$ $74$ $0.0018$ $47$ $19$ $87$ $0.0056$ $12$ $82$ $0.006$ $F$ $F$ $F$ $48$ $19$ $89$ $0.0124$ $13$ $87$ $0.0077$ $F$ $F$ $F$ $49$ $47$ $817$ $0.0301$ $22$ $409$ $0.0147$ $23$ $431$ $0.019$ $50$ $F$ $F$ $F$ $F$ $F$ $F$ $F$ $F$ $F$ $52$ $F$ $F$ $F$ $F$ $F$ $F$ $F$ $F$ $F$ $52$ $F$	39	54	193	0.0183	15	76	0.0048	156	637	0.0136	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	40	17	94	0.2085	F	F	5.0010 F	93	405	0.0115	
41 $6$ $122$ $6.632$ $6.632$ $10$ $1.262$ $603$ $11$ $49$ $0.0012$ $42$ $8$ $37$ $0.0022$ $8$ $37$ $0.0023$ $11$ $49$ $0.0017$ $43$ $8$ $37$ $0.0093$ $8$ $37$ $0.0044$ $11$ $49$ $0.01$ $44$ $9$ $43$ $0.0181$ $7$ $37$ $0.0032$ $63$ $223$ $0.0257$ $45$ $27$ $112$ $0.0038$ $31$ $117$ $0.0017$ $20$ $76$ $0.0027$ $46$ $26$ $103$ $0.0021$ $9$ $46$ $6.12E-04$ $19$ $74$ $0.0018$ $47$ $19$ $87$ $0.0056$ $12$ $82$ $0.006$ $F$ $F$ $F$ $48$ $19$ $89$ $0.0124$ $13$ $87$ $0.0077$ $F$ $F$ $F$ $49$ $47$ $817$ $0.0301$ $22$ $409$ $0.0147$ $23$ $431$ $0.019$ $50$ $F$ $F$ $F$ $22$ $416$ $0.0251$ $22$ $386$ $0.0273$ $51$ $14$ $63$ $0.2976$ $14$ $78$ $0.2305$ $F$ $F$ $F$ $52$ $F$	40	6	22	8.45F-04	5	19	4 20F-03	9	31	0.0012	
43       8       37       0.0093       8       37       0.0044       11       49       0.01         44       9       43       0.0181       7       37       0.0032       63       223       0.0257         45       27       112       0.0038       31       117       0.0017       20       76       0.0027         46       26       103       0.0021       9       46       6.12E-04       19       74       0.0018         47       19       87       0.0056       12       82       0.006       F       F       F         48       19       89       0.0124       13       87       0.0077       F       F       F         49       47       817       0.0301       22       409       0.0147       23       431       0.019         50       F       F       F       22       416       0.0251       22       386       0.0273         51       14       63       0.2976       14       78       0.2305       F       F       F         52       F       F       F       F       F       F       F       F <td>42</td> <td>8</td> <td>37</td> <td>0.0022</td> <td>8</td> <td>37</td> <td>0.0023</td> <td>11</td> <td><u>4</u>9</td> <td>0.0012</td>	42	8	37	0.0022	8	37	0.0023	11	<u>4</u> 9	0.0012	
44       9       43       0.0181       7       37       0.0032       63       223       0.0257         45       27       112       0.0038       31       117       0.0017       20       76       0.0027         46       26       103       0.0021       9       46       6.12E-04       19       74       0.0018         47       19       87       0.0056       12       82       0.006       F       F       F         48       19       89       0.0124       13       87       0.0077       F       F       F         49       47       817       0.0301       22       409       0.0147       23       431       0.019         50       F       F       F       23       366       0.0273         51       14       63       0.2976       14       78       0.2305       F       F       F         52       F       F       F       F       F       F       F       F       F	43	8	37	0.0022	8	37	0.0023	11	49	0.01	
45       27       112       0.0038       31       117       0.0017       20       76       0.0027         46       26       103       0.0021       9       46       6.12E-04       19       74       0.0018         47       19       87       0.0056       12       82       0.006       F       F       F         48       19       89       0.0124       13       87       0.0077       F       F       F         49       47       817       0.0301       22       409       0.0147       23       431       0.019         50       F       F       F       2       416       0.0251       22       386       0.0273         51       14       63       0.2976       14       78       0.2305       F       F       F         52       F       F       F       F       F       F       F       F       F	43	9	43	0.0093	7	37	0.0032	63	223	0.0257	
46       26       103       0.0021       9       46       6.12E-04       19       74       0.0018         47       19       87       0.0056       12       82       0.006       F       F       F         48       19       89       0.0124       13       87       0.0077       F       F       F         49       47       817       0.0301       22       409       0.0147       23       431       0.019         50       F       F       F       22       416       0.0251       22       386       0.0273         51       14       63       0.2976       14       78       0.2305       F       F       F         52       F       F       F       F       F       F       F       F	45	27	112	0.0038	31	117	0.0017	20	76	0.0027	
47       19       87       0.0056       12       82       0.006       F       F       F         48       19       89       0.0124       13       87       0.0077       F       F       F         49       47       817       0.0301       22       409       0.0147       23       431       0.019         50       F       F       F       22       416       0.0251       22       386       0.0273         51       14       63       0.2976       14       78       0.2305       F       F       F         52       F       F       F       F       F       F       F       F       F	46	26	103	0.0021	9	46	6 12F-04	19	74	0.0018	
48       19       89       0.0124       13       87       0.0077       F       F       F         49       47       817       0.0301       22       409       0.0147       23       431       0.019         50       F       F       F       22       416       0.0251       22       386       0.0273         51       14       63       0.2976       14       78       0.2305       F       F       F         52       F       F       F       F       F       F       F       F	40	19	87	0.0021	12	82	0.006	F	F	5.0010 F	
49       47       817       0.0301       22       409       0.0147       23       431       0.019         50       F       F       F       22       416       0.0251       22       386       0.0273         51       14       63       0.2976       14       78       0.2305       F       F       F         52       F       F       F       F       F       F       F       F	48	19	89	0.0124	13	87	0.0077	F	F	F	
50     F     F     22     407     0.0147     25     451     0.017       50     F     F     F     22     416     0.0251     22     386     0.0273       51     14     63     0.2976     14     78     0.2305     F     F     F       52     F     F     F     F     F     F     F     F	49	47	817	0.0301	22	409	0.0147	23	431	0 019	
51 14 63 0.2976 14 78 0.2305 F F F 52 F F F F F F F F F F F	50	F	F	5.5501 F	22	416	0.0251	23	386	0.0273	
52 F F F F F F F F F	51	14	63	0.2976	14	78	0.2305	F	F	F	
	52	F	F	F	F	F	F	Ē	F	F	

 TABLE 2. (Continued.) Numerical results of RMIL+, PRP, and sFR methods.

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$										
54         F         F         21         181         0.0898         850         4788         1.763           55         16         102         0.3907         15         104         0.3841         50         127         0.8213           56         38         260         0.0144         F         F         F         26         97         0.0399           58         5         26         0.0145         5         26         0.0139         9         50         0.0126           59         7         40         0.0276         F         F         F         20         0.0128         10         11         0.0718           61         72         311         0.0084         56         263         0.0078         299         1489         0.0333           63         16         69         0.0028         10         45         0.0011         26         95         2.50E-03           64         F         F         F         F         F         F         44         1330         0.0313           63         16         0.1356         8         54         0.137         13         0.0022         56	53	16	102	0.0588	15	104	0.0525	49	214	0.1055
55       16       102 $0.3907$ 15       104 $0.3841$ 50       127 $0.8213$ 56       38       260 $0.9512$ 22       203 $0.7392$ 130       1308 $4.4304$ 57       6       37       0.0144       5       26 $0.0139$ 9       50 $0.0182$ 59       7       40 $0.0276$ F       F       F       5       127 $0.0716$ 60       9       55 $0.0425$ 13       68 $0.0458$ 29       121 $0.0716$ 61       72       311 $0.0084$ 56       263 $0.0055$ 1208 $5994$ $0.0791$ 62       111       548 $0.0128$ 10       45 $0.0011$ 20 $82$ $0.0027$ 65       F       F       F       F       F       F       44       1330 $0.5172$ 66       F       F       F       F       F       44       1330 $0.5172$ 67       22       74 $0.0003$ 27       17	54	F	F	F	21	181	0.0898	850	4788	1.763
56         38         260         0.9512         22         203         0.7392         130         1308         4.4304           57         6         37         0.0144         F         F         F         26         97         0.0399           58         5         26         0.0145         5         26         0.0139         9         50         0.0181           60         9         55         0.0425         13         68         0.0458         29         121         0.0718           61         72         311         0.0084         56         263         0.0078         299         1489         0.0333           63         16         69         0.0028         10         45         0.0011         26         95         2.50E.03           64         F         F         F         F         F         F         537         14628         2.2454           66         F         F         F         F         F         F         6337         173         0.0034           61         13         0.1356         8         54         0.1337         13         55         0.1317      <	55	16	102	0.3907	15	104	0.3841	50	127	0.8213
57       6       37       0.0144       F       F       F       26       97       0.0399         58       5       26       0.0145       5       26       0.0139       9       50       0.0182         59       7       40       0.0276       F       F       F       35       127       0.0718         60       9       55       0.0425       13       68       0.0458       29       121       0.0718         61       72       311       0.0084       56       263       0.0055       1208       5994       0.0791         62       111       548       0.0183       71       376       0.0078       299       1489       0.0333         63       16       69       0.0028       10       45       0.0012       20       82       0.0027         65       F       F       F       F       F       F       7       0.057       27       90       0.0044         68       28       120       0.0032       27       117       0.0037       43       173       0.0038         69       11       63       0.1356       8       5	56	38	260	0.9512	22	203	0.7392	130	1308	4.4304
58       5       26       0.0139       9       50       0.0182         59       7       40       0.0276       F       F       F       F       3       51       127       0.0182         60       9       55       0.0425       13       68       0.0458       29       121       0.0716         61       72       311       0.0084       56       263       0.0058       1208       5994       0.0731         63       16       69       0.0023       10       45       0.0011       26       95       2.50E-03         64       F       F       F       F       F       F       F       537       14628       2.2454         66       F       F       F       F       F       F       7       90       0.004         68       28       120       0.003       27       117       0.0057       27       90       0.004         69       11       63       0.1326       8       54       0.1141       17       80       0.5088         71       11       63       0.0137       8       44       0.0127       115 <t< td=""><td>57</td><td>6</td><td>37</td><td>0.0144</td><td>F</td><td>F</td><td>F</td><td>26</td><td>97</td><td>0.0399</td></t<>	57	6	37	0.0144	F	F	F	26	97	0.0399
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	58	5	26	0.0145	5	26	0.0139	9	50	0.0182
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	59	7	40	0.0276	F	F	F	35	127	0.0716
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	60	9	55	0.0425	13	68	0.0458	29	121	0.0718
62         111         548         0.0183         71         376         0.0078         299         1489         0.0333           63         16         69         0.0028         10         45         0.0011         26         95         2.50E-03           64         F         F         F         F         F         F         F         537         14628         2.2454           66         F         F         F         F         F         F         F         F         90         0.004           67         22         74         0.0058         23         77         0.0057         27         90         0.004           68         28         120         0.003         27         117         0.0037         43         173         0.0038           69         11         63         0.1356         8         54         0.0137         17         80         0.5808           71         11         44         0.0217         13         55         0.1317           75         207         923         0.0331         F         F         F         F         F         F         F <th< td=""><td>61</td><td>72</td><td>311</td><td>0.0084</td><td>56</td><td>263</td><td>0.0055</td><td>1208</td><td>5994</td><td>0.0791</td></th<>	61	72	311	0.0084	56	263	0.0055	1208	5994	0.0791
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	62	111	548	0.0183	71	376	0.0078	299	1489	0.0333
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	63	16	69	0.0028	10	45	0.0011	26	95	2.50E-03
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	64	F	F	F	12	59	0.0012	20	82	0.0027
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	65	F	F	F	F	F	F	537	14628	2.2454
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	66	F	F	F	F	F	F	44	1330	0.5172
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	67	22	74	0.0058	23	77	0.0057	27	90	0.004
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	68	28	120	0.003	27	117	0.0037	43	173	0.0038
70         11         63 $0.4922$ 8         54 $0.3937$ 17         80 $0.5808$ 71         11         44 $0.0155$ 8         34 $0.0327$ 15         56 $0.0243$ 72         7         34 $0.0165$ 6         31 $0.0127$ 9         40 $0.0185$ 73         9         42 $0.0952$ 8         45 $0.1075$ 17         115 $0.2521$ 74         11         50 $0.137$ 8         44 $0.1027$ 13         55 $0.1317$ 75         207         923 $0.0331$ F         <	69	11	63	0.1356	8	54	0.1141	17	80	0.1977
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	70	11	63	0.4922	8	54	0.3937	17	80	0.5808
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	71	11	44	0.0215	8	34	0.0327	15	56	0.0243
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	72	7	34	0.0165	6	31	0.0127	9	40	0.0185
74         11         50         0.137         8         44         0.1027         13         55         0.1317           75         207         923         0.0331         F         <	73	9	42	0.0952	8	45	0.1075	17	115	0.2521
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	74	11	50	0.137	8	44	0.1027	13	55	0.1317
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	75	207	923	0.0331	F	F	F	F	F	F
76772622.88E-04262.34E-04262.24E-0478262.84E-04262.34E-04262.24E-0479782800.0225702500.02411164070.240480773340.0327582750.0322FFFF81FFFFFFF11770.003483692070.0115381140.0049381140.006184782340.0104401200.0073401200.00688544713410.17161313930.07191313930.0638650015000.20461374110.0721374110.0683877210.0027FFF341012.18E-0188FFF11590.0019FFF89271050.002622870.0032954750.2468921808410.0609FFFFFF9380227880.05171636960.013327310960.023394100207880.05171636960.013327310960.02469430296 </td <td>76</td> <td>31</td> <td>195</td> <td>0.0134</td> <td>25</td> <td>188</td> <td>0 004</td> <td>182</td> <td>1750</td> <td>0 0338</td>	76	31	195	0.0134	25	188	0 004	182	1750	0 0338
78262.84E-04264.06E-04262.96E-047978280 $0.0225$ 70250 $0.0241$ 116407 $0.2404$ 8077334 $0.0327$ 58275 $0.0322$ FFFF81FFFFFFFFFFF8369207 $0.0115$ 38114 $0.0049$ 38114 $0.0061$ 8478234 $0.0104$ 40120 $0.0073$ 40120 $0.0068$ 854471341 $0.1716$ 131393 $0.0719$ 131393 $0.063$ 865001500 $0.2046$ 137411 $0.072$ 137411 $0.0683$ 87721 $0.0027$ FFF341012.18E-0188FFF1159 $0.0019$ FFF8927105 $0.0026$ 2287 $0.0021$ 2184 $0.0071$ 9037170 $0.0062$ 37157 $0.0036$ 197635 $0.0325$ 91109505 $0.0394$ 74409 $0.032$ 95475 $0.2468$ 92180841 $0.0609$ FFFFFF938022788 $0.0517$ 163696 $0.0133$ 2731096 $0.0253$ </td <td>70</td> <td>2</td> <td>6</td> <td>2 58E-04</td> <td>25</td> <td>6</td> <td>2 34E-04</td> <td>2</td> <td>6</td> <td>2 41E-04</td>	70	2	6	2 58E-04	25	6	2 34E-04	2	6	2 41E-04
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	78	2	6	2.36E-04 2.84E-04	$\frac{2}{2}$	6	2.54E-04 4.06E-04	$\frac{2}{2}$	6	2.41E-04 2.96E-04
191010010010010010010010080773340.0327582750.0322FFFF81FFFFFFFF9630.010282FFFFFFFF11770.003483692070.0115381140.0049381140.006184782340.0104401200.0073401200.00688544713410.17161313930.07191313930.0638650015000.20461374110.0721374110.0683877210.0027FFF341012.18E-0188FFFF11590.0019FFF89271050.002622870.002121840.007190371700.0062371570.00361976350.0325911095050.0394744090.032954750.2468921808410.0609FFFFFF9380227880.05171636960.013327310960.02539514530.00126 </td <td>79 79</td> <td>78</td> <td>280</td> <td>0.0225</td> <td>70</td> <td>250</td> <td>0.0241</td> <td>116</td> <td>407</td> <td>0 2404</td>	79 79	78	280	0.0225	70	250	0.0241	116	407	0 2404
81FFFFFFF9630.010282FFFFFFFF11770.003483692070.0115381140.0049381140.006184782340.0104401200.0073401200.00688544713410.17161313930.07191313930.0638650015000.20461374110.0721374110.0683877210.0027FFF341012.18E-0188FFFF11590.0019FFF89271050.002622870.002121840.007190371700.0062371570.00361976350.0325911095050.0394744090.032954750.2468921808410.0609FFFFFF9380227880.05171636960.013327310960.02539514530.00126286.26E-0420720.00419615680.00139499.52E-04511940.004297343130.158 <td< td=""><td>80</td><td>70</td><td>334</td><td>0.0327</td><td>58</td><td>275</td><td>0.0322</td><td>F</td><td>F</td><td>5.2101 F</td></td<>	80	70	334	0.0327	58	275	0.0322	F	F	5.2101 F
811 <th1< th="">11<th< td=""><td>81</td><td>F</td><td>F</td><td>6.65<i>21</i> Е</td><td>F</td><td>F</td><td>F</td><td>9</td><td>63</td><td>0.0102</td></th<></th1<>	81	F	F	6.65 <i>21</i> Е	F	F	F	9	63	0.0102
83 $69$ $207$ $0.0115$ $38$ $114$ $0.0049$ $38$ $114$ $0.0061$ $84$ $78$ $234$ $0.0104$ $40$ $120$ $0.0073$ $40$ $120$ $0.0068$ $85$ $447$ $1341$ $0.1716$ $131$ $393$ $0.0719$ $131$ $393$ $0.063$ $86$ $500$ $1500$ $0.2046$ $137$ $411$ $0.072$ $137$ $411$ $0.0683$ $87$ $7$ $21$ $0.0027$ $F$ $F$ $F$ $34$ $101$ $2.18E-01$ $88$ $F$ $F$ $F$ $111$ $59$ $0.0019$ $F$ $F$ $F$ $89$ $27$ $105$ $0.0026$ $22$ $87$ $0.0021$ $21$ $84$ $0.0071$ $90$ $37$ $170$ $0.0062$ $37$ $157$ $0.0036$ $197$ $635$ $0.0325$ $91$ $109$ $505$ $0.0394$ $74$ $409$ $0.032$ $95$ $475$ $0.2468$ $92$ $180$ $841$ $0.0609$ $F$ $F$ $F$ $F$ $F$ $F$ $93$ $802$ $2788$ $0.0517$ $163$ $696$ $0.0133$ $273$ $1096$ $0.0253$ $94$ $806$ $2811$ $0.0454$ $113$ $495$ $0.0133$ $273$ $1096$ $0.0253$ $95$ $14$ $53$ $0.0012$ $6$ $28$ $6.26E-04$ $20$ $72$ $0.0041$ $96$ $15$ $68$ $0.0013$ <	82	F	F	F	F	F	F	11	77	0.0034
84         78         234         0.0104         40         120         0.0073         40         120         0.0068           85         447         1341         0.1716         131         393         0.0719         131         393         0.063           86         500         1500         0.2046         137         411         0.072         137         411         0.0683           87         7         21         0.0027         F         F         F         34         101         2.18E-01           88         F         F         F         F         11         59         0.0019         F         F         F           89         27         105         0.0026         22         87         0.0021         21         84         0.0071           90         37         170         0.0062         37         157         0.0036         197         635         0.0325           91         109         505         0.0394         74         409         0.032         95         475         0.2468           92         180         841         0.0609         F         F         F         F	83	69	207	0.0115	38	114	0.0049	38	114	0.0061
8544713410.17161313930.07191313930.0638650015000.20461374110.0721374110.0683877210.0027FFF341012.18E-0188FFFF11590.0019FFF89271050.002622870.002121840.007190371700.0062371570.00361976350.0325911095050.0394744090.032954750.2468921808410.0609FFFFFF9380227880.05171636960.013827210750.02489480628110.04541134950.013327310960.02539514530.00126286.26E-0420720.00419615680.00139499.52E-04511940.004297343130.0254222350.016138840750.178798302960.0252272960.023349050200.208199576200.1127394930.0871217213673.45910069743	84	78	234	0.0104	40	120	0.0073	40	120	0.0068
86 $500$ $150$ $0.0176$ $137$ $411$ $0.072$ $137$ $411$ $0.0683$ $87$ $7$ $21$ $0.0027$ $F$ $F$ $F$ $34$ $101$ $2.18E-01$ $88$ $F$ $F$ $F$ $11$ $59$ $0.0019$ $F$ $F$ $F$ $89$ $27$ $105$ $0.0026$ $22$ $87$ $0.0021$ $21$ $84$ $0.0071$ $90$ $37$ $170$ $0.0062$ $37$ $157$ $0.0036$ $197$ $635$ $0.0325$ $91$ $109$ $505$ $0.0394$ $74$ $409$ $0.032$ $95$ $475$ $0.2468$ $92$ $180$ $841$ $0.0609$ $F$ $F$ $F$ $F$ $F$ $F$ $93$ $802$ $2788$ $0.0517$ $163$ $696$ $0.0138$ $272$ $1075$ $0.0248$ $94$ $806$ $2811$ $0.0454$ $113$ $495$ $0.0133$ $273$ $1096$ $0.0253$ $95$ $14$ $53$ $0.0012$ $6$ $28$ $6.26E-04$ $20$ $72$ $0.0041$ $96$ $15$ $68$ $0.0013$ $9$ $49$ $9.52E-04$ $51$ $194$ $0.0042$ $97$ $34$ $313$ $0.0254$ $22$ $235$ $0.0161$ $388$ $4075$ $0.1787$ $98$ $30$ $296$ $0.0252$ $27$ $296$ $0.0233$ $490$ $5020$ $0.2081$ $99$ $57$ $620$ $0.1127$ <t< td=""><td>85</td><td>447</td><td>1341</td><td>0.1716</td><td>131</td><td>393</td><td>0.0719</td><td>131</td><td>393</td><td>0.063</td></t<>	85	447	1341	0.1716	131	393	0.0719	131	393	0.063
877 $21$ $0.0027$ FFFF $34$ $101$ $2.18E-01$ $88$ FFFF11 $59$ $0.0019$ FFFF $89$ $27$ $105$ $0.0026$ $22$ $87$ $0.0021$ $21$ $84$ $0.0071$ $90$ $37$ $170$ $0.0062$ $37$ $157$ $0.0036$ $197$ $635$ $0.0325$ $91$ $109$ $505$ $0.0394$ $74$ $409$ $0.032$ $95$ $475$ $0.2468$ $92$ $180$ $841$ $0.0609$ FFFFFF $93$ $802$ $2788$ $0.0517$ $163$ $696$ $0.0138$ $272$ $1075$ $0.0248$ $94$ $806$ $2811$ $0.0454$ $113$ $495$ $0.0133$ $273$ $1096$ $0.0253$ $95$ $14$ $53$ $0.0012$ $6$ $28$ $6.26E-04$ $20$ $72$ $0.0041$ $96$ $15$ $68$ $0.0013$ $9$ $49$ $9.52E-04$ $51$ $194$ $0.0042$ $97$ $34$ $313$ $0.0254$ $22$ $235$ $0.0161$ $388$ $4075$ $0.1787$ $98$ $30$ $296$ $0.0252$ $27$ $296$ $0.0233$ $490$ $5020$ $0.2081$ $99$ $57$ $620$ $0.1127$ $39$ $493$ $0.087$ $1217$ $21367$ $3.459$ $100$ $69$ $743$ $0.1158$	86	500	1500	0.2046	137	411	0.072	137	411	0.0683
88FFF1159 $0.0019$ FFFF8927105 $0.0026$ 2287 $0.0021$ 2184 $0.0071$ 9037170 $0.0062$ 37157 $0.0036$ 197635 $0.0325$ 91109505 $0.0394$ 74409 $0.032$ 95475 $0.2468$ 92180841 $0.0609$ FFFFFF938022788 $0.0517$ 163696 $0.0138$ 2721075 $0.0248$ 948062811 $0.0454$ 113495 $0.0133$ 2731096 $0.0253$ 951453 $0.0012$ 628 $6.26E-04$ 2072 $0.0041$ 961568 $0.0013$ 949 $9.52E-04$ 51194 $0.0042$ 9734313 $0.0254$ 22235 $0.0161$ 3884075 $0.1787$ 9830296 $0.0252$ 27296 $0.0233$ 4905020 $0.2081$ 9957620 $0.1127$ 39493 $0.087$ 121721367 $3.459$ 10069743 $0.1158$ 43528 $0.082$ 143625608 $4.0323$ 101FFFFFF327 $0.177$ 102FFFFFF327 $0.177$	87	7	21	0.0027	F	F	F	34	101	2.18E-01
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	88	F	F	F	11	59	0.0019	F	F	F
9037170 $0.0062$ 37157 $0.0036$ 197 $635$ $0.0325$ 91109505 $0.0394$ 74409 $0.032$ 95475 $0.2468$ 92180841 $0.0609$ FFFFFFF938022788 $0.0517$ 163696 $0.0138$ 2721075 $0.0248$ 948062811 $0.0454$ 113495 $0.0133$ 2731096 $0.0253$ 951453 $0.0012$ 628 $6.26E-04$ 2072 $0.0041$ 961568 $0.0013$ 949 $9.52E-04$ 51194 $0.0042$ 9734313 $0.0254$ 22235 $0.0161$ 3884075 $0.1787$ 9830296 $0.0252$ 27296 $0.0233$ 4905020 $0.2081$ 9957620 $0.1127$ 39493 $0.087$ 121721367 $3.459$ 10069743 $0.1158$ 43528 $0.082$ 143625608 $4.0323$ 101FFFFFF327 $0.1332$ 103FFFFFF327 $0.1332$ 104FFFFFF327 $0.177$ 105FFFFFF327 $0.217$ 105<	89	27	105	0.0026	22	87	0.0021	21	84	0.0071
911095050.0394744090.032954750.2468921808410.0609FFFFFFF9380227880.05171636960.013827210750.02489480628110.04541134950.013327310960.02539514530.00126286.26E-0420720.00419615680.00139499.52E-04511940.004297343130.0254222350.016138840750.178798302960.0252272960.023349050200.208199576200.1127394930.0871217213673.459100697430.1158435280.0821436256084.0323101FFFFFF3270.1332103FFFFF73270.1332103FFFFFF3270.17104FFFFFF3270.217105FFF15440.186723660.265106FFF15441.405627 <t< td=""><td>90</td><td>37</td><td>170</td><td>0.0062</td><td>37</td><td>157</td><td>0.0036</td><td>197</td><td>635</td><td>0.0325</td></t<>	90	37	170	0.0062	37	157	0.0036	197	635	0.0325
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	91	109	505	0.0394	74	409	0.032	95	475	0.2468
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	92	180	841	0.0609	F	F	F	F	F	F
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	93	802	2788	0.0517	163	696	0.0138	272	1075	0.0248
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	94	806	2811	0.0454	113	495	0.0133	273	1096	0.0253
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	95	14	53	0.0012	6	28	6.26E-04	20	72	0.0041
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	96	15	68	0.0013	9	49	9.52E-04	51	194	0.0042
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	97	34	313	0.0254	22	235	0.0161	388	4075	0.1787
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	98	30	296	0.0252	27	296	0.0233	490	5020	0.2081
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	99	57	620	0.1127	39	493	0.087	1217	21367	3.459
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	100	69	743	0.1158	43	528	0.082	1436	25608	4.0323
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	101	F	F	F	F	F	F	3	27	0.0847
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	102	F	F	F	F	F	F	3	27	0.1332
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	103	F	F	F	F	F	F	3	27	0.17
105         F         F         F         15         44         0.1867         23         66         0.265           106         F         F         F         15         44         1.4056         27         78         2.4636	104	F	F	F	F	F	F	3	27	0.217
<u>106 F F F 15 44 1.4056 27 78 2.4636</u>	105	F	F	F	15	44	0.1867	23	66	0.265
	106	F	F	F	15	44	1.4056	27		2.4636

107	10	86	0.1111	11	91	0.0745	50	222	0.2247
108	10	86	0.6165	11	91	0.7072	52	228	1.8732
109	12	269	0.2379	11	256	0.236	10	194	0.1955
110	13	246	1.8967	11	199	1.6463	9	131	1.0683
111	12	286	4.412	11	257	4.0298	12	255	4.0832
112	7	22	0.0076	5	15	0.0011	10	30	0.005
113	7	30	0.003	5	15	0.0031	10	30	0.006
114	7	48	0.0292	5	15	0.0101	F	F	F
115	F	F	F	26	220	0.4321	60	281	0.5859
116	F	F	F	26	220	1.5976	66	299	2.5239
117	F	F	F	26	220	3.6466	66	299	4.8565
118	20	127	0.0025	16	91	0.0018	4013	12128	0.1617
119	39	171	0.0172	24	150	0.0036	4796	14474	0.2015
120	42	1261	0.0185	48	1484	0.012	F	F	F
121	31	946	0.0086	42	1304	0.0124	F	F	F
122	F	F	F	F	F	F	33	97	0.0032
123	F	F	F	F	F	F	29	62	0.006
124	14	421	0.0595	F	F	F	F	F	F
125	36	1067	0.7225	F	F	F	F	F	F
126	F	F	F	F	F	F	F	F	F
127	F	F	F	F	F	F	16	114	0.0388
128	F	F	F	F	F	F	F	F	F
129	10	51	0.0018	13	77	0.0016	15	66	0.0022
130	27	159	0.0213	16	108	0.0089	F	F	F

TABLE 2. (Continued.) Numerical results of RMIL+, PRP, and sFR methods.



FIGURE 1. Performance profiles based on NOI.

where  $1 \le s \le n_s$ ,  $r_{p,s}$  is the performance ratio which is defined by:  $r_{p,s} := t_{p,s} / \min\{t_{p,s}\}$  and for each solver  $s \in S_l$ and each problem  $p \in P_l$ , they define  $t_{p,s}$  is NOI or NOF or CPU time required to solve problem p by solver s. According to their rules, the method with the curve at the top is the best.

From Figures 1, 2 and 3, we can see that the sRMIL+ curve is mostly at the top of the RMIL+, PRP, and sFR curves, so it is indicating that the sRMIL+ algorithm outperforms the RMIL+, PRP, and sFR methods based on NOI, NOF, and CPU time. Meanwhile, when we compare the sRMIL+ method with the sPRP method, both methods are competitive based on NOI, NOF, and CPU time. Finally, by combining Tables 2, 3 and Figures 1, 2, 3, we can take conclusion that



FIGURE 2. Performance profiles based on NOF.

sRMIL+ method perform better than RMIL+, PRP and SFR, on other hand the sPRP and sRMIL+ methods are almost the same performance. This demonstrates that the methods proposed in this paper have good numerical performance.

## **V. APPLICATION IN PORTFOLIO SELECTION**

In this section, we present the application of the proposed method for solving portfolio selection problem. Theory of portfolio selection was first proposed by Harry Markowitz in his paper "Portfolio Selection" [44]. In this paper, we only consider the stock portfolio. Stock portfolio can be defined as a collection of stocks owned by investors. Portfolio theory is based on the fact that investors will invest their money in

## TABLE 3. Numerical results of sPRP, and sRMIL+ methods.

Number		sPR	Р	sRMIL+			
	NOI	NOF	CPU	NOI	NOF	CPU	
1	18	120	0.0318	23	147	0.0365	
2	20	144	0.0438	26	295	0.0676	
3	18	120	0.2253	23	147	0.2603	
4	19	129	0.243	36	508	0.7877	
5	5	13	0.0051	6	16	0.0051	
6	5	13	0.0058	6	16	0.0048	
7	5	13	0.0062	8	22	0.0086	
8	5	13	0.0094	8	22	0.0063	
9	36	94	0.007	16	53	0.0016	
10	31	95	0.0032	19	93	0.0023	
11	1	3	2.22E-04	1	3	1.59E-04	
12	5	23	5.43E-04	5	23	5.33E-04	
13	8	32	0.019	7	30	0.0145	
14	14	63	0.0287	17	74	0.026	
15	12	43	0.0952	14	48	0.1018	
16	11	57	0.1207	13	73	0.1853	
17	14	108	0.002	19	197	0.0017	
18	29	308	0.0039	34	303	0.0037	
19	3261	9856	0.7004	70	863	0.0693	
20	101	401	0.0382	39	225	0.0245	
20	13	-61	0.0349	16	121	0.0245	
21	10	Δ <del>1</del>	0.0371	10	/3	0.0332	
22	10	47	0.0371	0	45 70	0.0002	
23	10	47	0.201	10	49	0.2008	
2 <del>4</del> 25	6	30	8 17E-04	7	33	7 39F-04	
25 26	8	30 42	1 10E-03	12	55 57	1 20E-03	
20 27	16	430	0.2081	12	214	0.0044	
27	9		0.0072	13	367	0.0044	
20	10	2 <del>4</del> 0 30	$1.10E_{-}03$	10	307	9 30F-04	
30	10	30	$9.12E_{-0.0}$	10	30	9.30E-04	
31	137	801	0.0083	134	1471	0.0107	
31	87	377	0.0003	67	/33	0.0107	
32	1	3	0.0043	1	3	0.0036	
34	1	3	0.0074	1	3	0.0050	
35	27	07	0.0074	10	78	$9.20E_{-0.0}$	
36	60	92 281	0.002	30	144	0.0027	
30	25	201 75	0.0030	50	150	0.0027	
39	23 41	122	0.004	20	272	0.0097	
30	41	70	0.008	00 15	275	0.0108	
39 40	13	79 72	0.009	15	72 60	0.0041	
40 41	13	10	0.0041 8 60E 02	5	10	0.003 6 70E 04	
41 42	3 0	19	0.00E-03	3 11	19	0.72E-04	
42	ð	51 27	0.0046	11	49	0.0013	
43	ð	3/ 41	0.0035	11 0	49 41	0.0033	
44	8 22	41	0.0039	ð 10	41	0.0034	
45	33 7	125	0.1931	19	90 44	0.0095	
40 47	/	30 05	0.0030	9	44	0.0026	
47	13 E	85	0.0092	23	142	0.01/1	
48	г 22	F 410	F 0.0220	21 49	141	0.0163	
49 50	22	419	0.0229	48	813 710	0.0405	
	24	489	0.0323	43	/19	0.0434	

 TABLE 3. (Continued.) Numerical results of sPRP, and sRMIL+ methods.

51	F	F	F	F	F	F
52	F	F	F	F	F	F
53	14	98	0.0547	17	111	0.0562
54	23	229	0.1045	30	408	0.1625
55	14	98	0.362	17	111	0.4085
56	31	308	1.0713	33	220	0.7971
57	13	63	0.0287	7	220 46	0.025
50	15	26	0.0287	5	40 26	0.023
50	12	20 62	0.0128	10	20	0.0156
59	15	05	0.044	12	94	0.055
60		45	0.0338	13	104	0.059
61	56	263	0.0077	58	279	0.0108
62	53	285	0.006	68	524	0.0164
63	9	43	1.90E-03	12	57	8.27E-04
64	11	49	1.30E-03	15	67	0.0014
65	18	434	0.1061	18	411	0.1426
66	17	477	0.1394	14	340	0.1119
67	23	77	0.0019	24	83	0.0016
68	27	117	0.003	31	144	0.0026
69	F	F	F	F	F	F
70	F	F	F	F	F	F
71	7	31	0.0126	12	45	0.0155
72	6	31	0.0135	6	31	0.0228
73	8	45	0.1121	8	44	0.0999
73 74	6	33	0.0867	7	36	0.0909
75	34	263	0.0007	, E	50 E	0.0909 F
75	27	203	0.2413	20	257	0.0087
70	21	208	4.12E.04	30	231	0.0067
70	2	0	4.12E-04	2	0	2.43E-04
/8	2	0	2.42E-04	2	0	2.34E-04
/9	70	250	0.0065	101	497	0.0143
80	58	275	0.0069	78	392	0.0152
81	9	63	0.0079	9	63	7.60E-03
82	11	77	0.0033	11	77	0.0024
83	38	114	0.0059	76	353	0.0149
84	40	120	0.0091	71	321	0.0148
85	131	393	0.0661	262	1755	0.2009
86	137	411	0.0699	260	1211	0.22
87	16	40	7.40E-03	9	26	7.03E-04
88	14	60	7.10E-03	11	54	1.30E-03
89	20	80	0.0094	22	90	0.0024
90	32	146	0.0086	46	308	0.01
91	76	446	0.0363	117	1259	0.0537
92	169	900	0.0576	152	1789	0.0812
93	163	695	0.0131	88	1403	0.0176
94	113	495	0.0136	51	305	0.0091
05	6	-75 -78	5.27E 04	6	205	5.07E 04
95 06	0	20 50	0.27E-04	0	20 70	0 12E 04
90 07	フ つ1	- JU - 110	9.32E-04	ァ つつ	77 202	9.12E-04
۶/ 00	21	228	0.0178	22	203	0.0189
98	21 41	290	0.0193	21 41	233	0.0158
99	41	508	0.0881	41	442	0.0828
100	37	440	0.0806	53	568	0.1064
101	3	27	0.0751	3	27	0.0709
102	3	27	0.1336	3	27	0.1228
103	3	27	0.1772	3	27	0.1687

TABLE 3. (Continued.) Numerical results of sPRP, and sRMIL+ methods.

104	3	27	0.2193	3	27	0.2145
105	7	27	0.1166	11	42	0.1878
106	7	27	1.1403	9	35	1.2819
107	11	91	0.086	12	92	0.0861
108	11	91	0.7223	11	89	0.6681
109	12	263	0.2703	11	149	0.1724
110	12	242	2.0159	12	195	1.5232
111	13	275	4.2859	11	149	2.7943
112	5	15	0.0012	5	15	0.0011
113	5	15	0.0024	5	15	0.0015
114	5	15	0.0111	5	15	0.0107
115	25	217	0.4152	23	144	0.2744
116	25	217	1.8073	21	136	0.969
117	25	217	3.3591	21	136	2.1777
118	18	110	0.0023	11	77	0.0022
119	19	119	0.0023	10	68	0.0018
120	50	1387	0.0151	40	1183	0.0108
121	43	1196	0.01	28	878	0.0083
122	7	20	7.89E-04	6	22	7.17E-04
123	22	55	0.0019	10	33	9.82E-04
124	39	1267	0.1274	14	421	0.0614
125	61	1825	1.2331	36	1066	0.7244
126	72	2154	14.1106	41	1322	10.273
127	8	68	0.0238	8	68	0.0218
128	10	170	1.2856	8	101	0.7042
129	8	43	0.001	8	43	9.96E-04
130	16	113	0.012	17	111	0.0126



FIGURE 3. Performance profiles based on CPU time.

various types of stocks, where the main objective is to reduce risk. According to [45], the return  $R_i$  on stock  $s_i$  is formulated by

$$R_i = \frac{P_t - P_{t-1}}{P_{t-1}}$$

where  $P_t$  is the price of the stock at time t and  $P_{t-1}$  is the price of stock at time t - 1. The expected return of the portfolio's return is defined as

$$\mu = \mathbb{E}\left(\sum_{i=1}^{n} w_i R_i\right) = \sum_{i=1}^{n} w_i \mu_i, \qquad (34)$$

and variance of the portfolio's return is defined as

$$\sigma^2 = \operatorname{Var}\left(\sum_{i=1}^n w_i R_i\right) = \sum_{i=1}^n \sum_{j=1}^n w_i w_j \operatorname{Cov}(R_i, R_j), \quad (35)$$

where *n* is number of stocks,  $w_i$  is the percentage of the value of the stock contained in the portfolio and  $Cov(R_i, R_j)$  is the covariance of  $R_i$  and  $R_j$ .

One way to optimize a portfolio is to minimize risk. Risk here is defined as the variance of the portfolio's return  $\sigma^2$ . So that the problem of portfolio selection can be written in the following model

$$\begin{cases} \text{minimize} : \sigma^2 = \operatorname{Var}\left(\sum_{i=1}^n w_i R_i\right) \\ \text{subject to} : \sum_{i=1}^n w_i = 1. \end{cases}$$
(36)

In this research, the stock price used is the weekly closing price of 9 stocks and the stocks being considered are PT Bank Central Asia Tbk (BBCA), PT Bank Rakyat Indonesia (Persero) Tbk (BBRI), PT Unilever Indonesia Tbk (UNVR), PT Telekomunikasi Indonesia Tbk (TLKM), PT Indofood CBP Sukses Makmur Tbk (ICBP), PT Bank Mandiri (Persero) Tbk (BMRI), PT Perusahaan Gas Negara Tbk (PGAS), PT Astra International Tbk (ASII) and PT Bank Negara Indonesia Tbk (BBNI) where the stock closing price is obtained from the data http://finance.yahoo.com/., over a period of 3 years (Jan 1, 2018 - Dec 31, 2020). Based on this

 TABLE 4. Mean and Variance of return of all stocks.

Stocks	BBCA	BBRI	UNVR	TLKM	ICBP	BMRI	PGAS	ASII	BBNI	_
Mean	-0.0020	0.0003	0.0031	0.0025	0.0005	0.0028	0.0036	0.0032	0.0037	
Variance	0.0013	0.0027	0.0013	0.0017	0.0014	0.0031	0.0067	0.0024	0.0035	

TABLE 5. Covariance of return of all stocks.

Stocks	BBCA	BBRI	UNVR	TLKM	ICBP	BMRI	PGAS	ASII	BBNI	
BBCA	0.0013	0.0013	0.0005	0.0006	0.0005	0.0014	0.0017	0.0012	0.0015	
BBRI	0.0013	0.0027	0.0006	0.0009	0.0006	0.0024	0.0023	0.0018	0.0025	
UNVR	0.0005	0.0006	0.0013	0.0005	0.0006	0.0009	0.0010	0.0007	0.0007	
TLKM	0.0006	0.0009	0.0005	0.0017	0.0005	0.0011	0.0016	0.0009	0.0012	
ICBP	0.0005	0.0006	0.0006	0.0005	0.0014	0.0008	0.0009	0.0005	0.0008	
BMRI	0.0014	0.0024	0.0009	0.0011	0.0008	0.0031	0.0028	0.0019	0.0028	
PGAS	0.0017	0.0023	0.0010	0.0016	0.0009	0.0028	0.0067	0.0023	0.0031	
ASII	0.0012	0.0018	0.0007	0.0009	0.0005	0.0019	0.0023	0.0024	0.0019	
BBNI	0.0015	0.0025	0.0007	0.0012	0.0008	0.0028	0.0031	0.0019	0.0035	
										-

data, we have return of each weekly closing stock price and also obtained the mean, variance, and covariance values of return in Tables 4 and 5, respectively.

Let  $w_1, w_2, \ldots, w_9$  be the proportions allocated to BBCA, BBRI, UNVR, TLKM, ICBP, BMRI, PGAS, ASII and BBNI, respectively. By setting  $w_9 = 1 - w_2 - w_2 - w_3 - w_4 - w_5 - w_6 - w_7 - w_8$  and using the data in Tables 4 and 5, we can form problem (36) into an unconstrained optimization problem as follows:

 $\left\{ (-0.2e - 3w_1 - 0.2e - 3w_2 - 0.10e - 2w_3) \right\}$ min  $\mathbf{w} \in \mathbb{R}^8$  $-0.9e - 3w_4 - 0.10e - 2w_5 - 0.1e - 3w_6$  $+0.2e - 3w_7 - 0.3e - 3w_8 + 0.15e - 2)w_1 +$  $(-0.12e - 2w_1 + 0.2e - 3w_2 - 0.19e - 2w_3)$  $-0.16e - 2w_4 - 0.19e - 2w_5 - 0.1e - 3w_6$  $-0.2e - 3w_7 - 0.7e - 3w_8 + 0.25e - 2)w_2$  $+(-0.2e - 3w_1 - 0.1e - 3w_2 + 0.6e - 3w_3)$  $-0.2e - 3w_4 - 0.1e - 3w_5 + 0.2e - 3w_6$  $+0.3e - 3w_7 + 0.7e - 3w_3 + (-0.6e - 3w_1)$  $-0.3e - 3w_2 - 0.7e - 3w_3 + 0.5e - 3w_4$  $-0.7e - 3w_5 - 0.1e - 3w_6 + 0.4e - 3w_7$  $-0.3e - 3w_8 + 0.12e - 2w_4 + (-0.3e - 3w_1)$  $-0.2e - 3w_2 - 0.2e - 3w_3 - 0.3e - 3w_4$  $+0.6e - 3w_5 + 0.8e - 3 + 0.1e - 3w_7$  $-0.3e - 3w_8)w_5 + (-0.14e - 2w_1)w_5 + (-0.14e -0.4e - 3w_2 - 0.19e - 2w_3 - 0.17e - 2w_4$  $-0.20e - 2w_5 + 0.3e - 3w_6 + 0.28e - 2$  $-0.9e - 3w_8)w_6 + (-0.14e - 2w_1 - 0.8)w_6 + (-0.14e - 0.8)w_6 + (-0.14$  $e - 3w_2 - 0.21e - 2w_3 - 0.15e - 2w_4$  $-0.22e - 2w_5 - 0.3e - 3w_6 + 0.36e - 2w_7$  $-0.8e - 3w_8 + 0.31e - 2)w_7 + (-0.7e - 3w_1)w_7 + (-0.7e - 3w_1$  $-0.1e - 3w_2 - 0.12e - 2w_3 - 0.10e - 2w_4$ 

$$\begin{array}{l} -0.14e - 2w_5 + 0.19e - 2 + 0.4e - 3w_7 \\ +0.5e - 3w_8)w_8 + (-0.20e - 2w_1 \\ -0.10e - 2w_2 - 0.28e - 2w_3 - 0.23e - 2w_4 \\ -0.27e - 2w_5 - 0.7e - 3w_6 - 0.4e - 3w_7 \\ -0.16e - 2w_8 + 0.35e - 2)(1 - w_1 - w_2 \\ -w_3 - w_4 - w_5 - w_6 - w_7 - w_8) \end{array} \}.$$

By running Algorithm 1 with an initial point (0.25,..., 0.25), then the problem above has a solution  $w_1 = 0.4322$ ,  $w_2 = 0.1201$ ,  $w_3 = 0.2892$ ,  $w_4 = 0.2464$ ,  $w_5 = 0.2333$ ,  $w_6 = -0.1818$ ,  $w_7 = -0.0854$ ,  $w_8 = 0.0187$ , and also we obtained  $w_9 = 0.0727$ . Furthermore, based on (34) and (35), we have  $\mu = 0.0003$  and  $\sigma^2 = 0.0006$ , respectively. Therefore, we can take the proportion of each stock with minimal risk, i.e, 43.22% BBCA, 12.01% BBRI, 28.92% UNVR, 24.64% TLKM, 23.33% ICBP, -18.18%, BMRI, -8.54% PGAS, 1.87% ASII and 7.27% BBNI. Because there is a minus sign in the proportion of ICBP and BMRI stocks, it indicates that investor can do short shelling. As a final conclusion here, investors can consider this portfolio with a minimal risk is 0.0006 and an expected portfolio return value is 0.0003.

## VI. APPLICATION IN TWO-JOINT PLANAR ROBOTIC MOTION CONTROL

Additional efficiency test for the good performance of the sRMIL+ method is demonstrated by implementing it to solve a two-joint planar robotic motion control problem. To begin with, a brief description of discrete-time kinematics equation of two-joint planar robot manipulator will be given as presented in [46]. Let  $u_k \in \mathbb{R}^2$  denotes the joint angle vector and  $v_k \in \mathbb{R}^2$  be end effector position vector. A discrete-time kinematics equation of two-joint planar robot two-joint planar robot manipulator at a position level is described by the following model

$$\Omega(u_k) = v_k. \tag{37}$$



FIGURE 4. Manipulator trajectories.

Let  $\ell_1$  and  $\ell_2$ , respectively, denote the lengths of the first and second rod. The mapping  $\Omega : \mathbb{R}^n \to \mathbb{R}^n$  is the kinematics mapping where its structure is given as follows

$$\Omega(u) = \begin{bmatrix} \ell_1 \cos(u_1) + \ell_2 \cos(u_1 + u_2), & \ell_2 \sin(u_1) \\ & + \ell_2 \sin(u_1 + u_2) \end{bmatrix}^T.$$

In motion control problem, at each instant time, say  $t_k \in [0, t_{\text{final}}]$  where  $t_{\text{final}}$  is the end of task duration, a series nonlinear least squares problems which are a special case of the unconstrained optimization problem needed to be solved as follows

$$\min_{v_k \in \mathbb{R}^2} \frac{1}{2} \| v_k - \widehat{v}_k \|^2,$$
(38)

where  $\hat{v}_k$  represents the end effector controlled track.

Following similar approach presented in [1], [47], the end effector, that is  $\hat{v}_k$ , used in this experiment, is controlled to track a Lissajous curve given as

$$\widehat{\nu}_{k} = \left[\frac{3}{2} + \frac{1}{5}\sin\left(\frac{\pi t_{k}}{5}\right), \quad \frac{\sqrt{3}}{2} + \frac{1}{5}\sin\left(\frac{2\pi t_{k}}{5} + \frac{\pi}{3}\right)\right]^{T}.$$
(39)

The implementation of the sRMIL+ algorithm with regards to the motion control experiment was performed using MATLAB R2019b and run on a PC with intel Core(TM) i5-8250u processor with 4 GB of RAM and CPU 1.60 GHZ. The initial point used is  $u_0 = [u_1, u_2] = [0, \frac{\pi}{3}]^T$  with the task duration  $[0, t_{\text{final}}]$  being divided into 200 equal parts, where  $t_{\text{final}} = 10$  seconds and  $\ell_1 = \ell_2 = 1$ .

The motion control experimental results are presented in Figures 4–7, where Figure 4 depicts the robot trajectories synthesized by the sRMIL+ algorithm and Figure 5 plots the end effector trajectory and desired path. The errors of the sRMIL+ algorithm are reported in Figures 6–7, where Figure 6 shows the error recorded on horizontal axis and Figure 7 shows the error recorded on the vertical axis. It is



FIGURE 5. End effector trajectory and desired path.



FIGURE 6. Tracking errors on the horizontal x-axis.



FIGURE 7. Tracking errors on the vertical y-axis.

apparent from Figures 4 and 5 that the sRMIL+ algorithm successfully executed the task given to it. The error recorded during the execution of the task is as low as  $10^{-5}$ . This is evident from Figures 6 and 7. This confirms the efficiency and applicability of the proposed sRMIL+ algorithm.

## **VII. CONCLUSION**

In this paper, we presented a new spectral conjugate gradient direction based on the idea of recent RMIL+ CG coefficient. For the proposed method, the sufficient descent condition always holds regardless of the line search procedure used. The global convergence proof was established under some standard assumptions. Preliminary experiment was conducted to check the performance of the proposed algorithm. The numerical results obtained showed that the new algorithm is not only efficient but also promising in practice when compared with some existing CG algorithms. Furthermore, the proposed spectral method was extended to solve problems of portfolio selection and robotic motion control to demonstrate its applicability to real-world problems.

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