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# **1.6-Octave Coherent OAM Supercontinuum Generation in As<sub>2</sub>S<sub>3</sub> Photonic Crystal Fiber**

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**ABSTRACT** We design and simulate an all-normal dispersion arsenic trisulfide (As<sub>2</sub>S<sub>3</sub>) photonic crystal fiber (PCF) with high nonlinearity to enable a flat and coherent orbital angular momentum (OAM) supercontinuum (SC) generation. The photonic crystal fiber features a near-zero and flat negative dispersion with variation between -96.5 and -36.5 ps/(m·km) over a 940-nm wavelength range from 1740 to 2680 nm. A 1946-nm supercontinuum forms from 959 to 2905 nm at -20 dB level which covers a 1.6-octave bandwidth, by launching a 100-fs 5-kW chirp-free hyperbolic secant pulse with wavelength at 2000 nm into a 1.0-cm designed fiber. The generated supercontinuum of the other two vortex modes (TE<sub>01</sub> and TM<sub>01</sub>) can cover more than two octaves by optimizing the proposed fiber structures. The coherence of the generated supercontinuum of the three modes all shows nearly perfect property over the whole bandwidth. In general, we found that the designed ring-core As<sub>2</sub>S<sub>3</sub> PCF with all-normal dispersion could be used for broadband coherent supercontinuum generation of various vortex modes.

**INDEX TERMS** Optical vortices, photonic crystal fibers, supercontinuum.

### I. INTRODUCTION

Light-carrying orbital angular momentum (OAM) has recently drawn extensive attention from researchers due to its great value in classical and quantum communications [1]–[3], stimulated emission depletion (STED) super-resolution microscopy [4], sensing [5], and laser material processing [6]. The OAM beams feature with helical phase fronts of  $\exp(il\phi)$ , where *l* and  $\phi$  represent the topological charge and azimuthal angle, respectively [7]. As a result of the intrinsic orthogonality among OAM modes with different *l* values, they can be used as a modal basis in the mode-division multiplexing (MDM) optical communications systems. In order to better propagate the OAM modes, one needs to avoid the degeneracy of the vortex-like modes. Consequently, the fiber is usually designed with a ring-shaped high-index profile, and large effective refractive index contrast ( $\Delta n_{eff} > 10^{-4}$ ) between different modes can be achieved [8]–[10].

Over the past two decades, the optical fiber community has paid significant attention to photonic crystal fiber (PCF), which enables many novel devices and applications. Its special and adjustable structure empowers several unique properties that could not be easily realized by conventional fibers, such as endlessly single-mode guiding, high birefringence, and controllable nonlinearity [11]–[17]. One of the fundamental advantages of PCF is its flexible dispersion engineering, which could potentially enable broadband supercontinuum (SC) generation.

Supercontinuum with a broad bandwidth and high coherence is of vital importance for many applications, such as optical coherence tomography, optical sensing, and optical frequency comb [18]–[21]. Chalcogenide materials are very promising for nonlinear applications due to its high nonlinear refractive index. By leveraging this material, chalcogenide PCF could achieve both the high nonlinearity and near-zero

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(a)

flat dispersion, which play critical roles in efficient supercontinuum generation over broad bandwidth [22], [23]. Some simulation investigations and experimental demonstrations [24], [25] have further shown that PCF with all-normal dispersion can be used to generate a flat and highly coherent supercontinuum by completely eliminating the modulation instability and the influences of the soliton [26].

In this work, we design and optimize an As<sub>2</sub>S<sub>3</sub> ring-core PCF with all-normal dispersion that supports OAM modes. The PCF features a near-zero and flat negative dispersion with the variation from -96.5 to -36.5 ps/(nm·km) over a 940-nm bandwidth from 1740 to 2680 nm. A 1946-nm supercontinuum is formed from 959 to 2905 nm at -20 dB level, which covers a 1.6-octave bandwidth, when a 100-fs 5-kW chirp-free hyperbolic secant pulse is launched into a 1.0-cm designed fiber. Furthermore, we investigated the SC generation of the  $TE_{01}$  and  $TM_{01}$  modes with all-normal dispersion by optimizing the fiber structure parameters. With a 100-fs 8-kW pump pulse at the wavelength of 2500 nm coupled into a 2-mm optimized PCF, we achieved a supercontinuum of the TE<sub>01</sub> mode covering over 2-octave bandwidth from 819 to 3440 nm at -30 dB. Additionally, by launching a 100-fs 20-kW pulse into a 2-mm long PCF, the supercontinuum of the  $TM_{01}$  mode can be generated from 849 to 3504 nm at  $-20 \, dB$ , which is also larger than two octaves. The generated supercontinua show nearly perfect coherence property over the whole bandwidth.

### **II. RING PCF DESIGN**

Figure 1(a) depicts the concept diagram of OAM supercontinuum generation by using the proposed ring-core As<sub>2</sub>S<sub>3</sub> PCF. As a short pulse launched into the proposed fiber, due to the interaction between the normal dispersion and nonlinear effects along the propagation, a flat and highly coherent SC is generated. The PCF has an air hole in the center. Its cladding consists of seven layers of air holes arranged in a regular hexagonal order, as displayed in Fig. 1(b). The geometric parameters of the fiber are set as follows:  $r_0$  is the radius of the central air hole,  $r_2$  to  $r_8$  are the radii of the air holes in the cladding, and d is the air hole pitch between the centers of proximal holes. The material of the background cladding is As<sub>2</sub>S<sub>3</sub>. Using a full-vector finite-element mode solver and applying the perfectly matched boundary layer, we can obtain the electromagnetic field distributions of the vortex modes  $(TE_{01}, TM_{01}, HE_{2,1}^{even} \text{ and } HE_{2,1}^{odd})$  in the ring-core PCF (d =0.4  $\mu$ m,  $r_0 = 0.17$   $\mu$ m,  $r_2 = 0.1$   $\mu$ m,  $r_3 = 0.15$   $\mu$ m,  $r_4 =$ 0.18  $\mu$ m,  $r_5$  to  $r_8 = 0.19 \mu$ m) at 2000 nm as illustrated in Fig. 1. (c). Furthermore,  $OAM_{1,1}$  mode can be supported in the PCF with the combination of its two eigenmodes  $(OAM_{1,1} = HE_{2,1}^{even} + i \times HE_{2,1}^{odd}).$ 

### **III. SUPERCONTINUUM GENERATION OF OAM1.1 IN PCF** WITH ALL-NORMAL DISPERSION

### A. FIBER PROPERTIES WITH OPTIMIZED DISPERSION

Figure 2(a) illustrates the chromatic dispersion of the  $OAM_{1,1}$ mode in the As<sub>2</sub>S<sub>3</sub> PCF with different  $r_3$  ( $d = 0.4 \ \mu m$ ,



FIGURE 1. (a) The concept diagram of supercontinuum generation in the proposed As<sub>2</sub>S<sub>3</sub> ring PCF. (b) Cross section of the designed ring-core As<sub>2</sub>S<sub>3</sub> PCF. (c) The modal distribution of the fiber eigenmodes (TE<sub>01</sub>, TM<sub>01</sub>, HE<sub>2,1</sub><sup>even</sup> and HE<sub>2,1</sub><sup>odd</sup>) and the corresponding OAM <sub>1,1</sub> mode ( $OAM_{1,1} = HE_{2,1}^{even} + i \times HE_{2,1}^{odd}$ ).

 $r_0 = 0.20 \ \mu \text{m}, r_2 = 0.1 \ \mu \text{m}, r_4 = 0.18 \ \mu \text{m}, r_5 \text{ to } r_8 =$ 0.19  $\mu$ m). To achieve all-normal and near-zero dispersion, we choose  $r_3 = 0.15 \ \mu m$  as the key parameter to the next step optimization. In order to get a flatter dispersion profile represented in Fig. 2(b), we further tailor the radius of the central air hole with  $d = 0.4 \ \mu \text{m}, r_2 = 0.1 \ \mu \text{m}, r_3 =$ 0.15  $\mu$ m,  $r_4 = 0.18 \mu$ m,  $r_5$  to  $r_8 = 0.19 \mu$ m. It can be seen that the dispersion curve of  $r_0 = 0.17 \ \mu m$  is all-normal and flat over a broad bandwidth. The maximum dispersion of the OAM mode in the proposed PCF is  $-36.5 \text{ ps/(nm \cdot km)}$  and its dispersion varies <60 ps/(nm·km) over a 940-nm bandwidth from 1740 to 2680 nm. At 1550 nm, the index difference between vortex modes (TE $_{01}$ , TM $_{01}$  and OAM $_{1,1}$ ) for the same structure parameters As<sub>2</sub>S<sub>3</sub> PCF are all two-ordersof-magnitude larger than the value in the regular ring fiber  $(\sim 10^{-4}).$ 



**FIGURE 2.** (a) Chromatic dispersion of the OAM<sub>1,1</sub> mode for different  $r_3$ . (b) Chromatic dispersion of the OAM<sub>1,1</sub> mode for different  $r_0$ .

The nonlinear coefficient  $\gamma$  and confinement loss of OAM<sub>1,1</sub> are displayed in Fig. 3. As the effective mode area increases with the wavelength, the nonlinear coefficient decreases and the confinement loss increases. At 2000 nm, the effective mode area of the OAM mode is 2.25  $\mu$ m<sup>2</sup>, and the corresponding large nonlinear coefficient is 4.55/W/m. The confinement loss is  $1.04 \times 10^{-4}$  dB/cm, which is relatively low.



**FIGURE 3.** Nonlinear coefficient and confinement loss of  $OAM_{1,1}$  mode in the optimized PCF.

The chromatic dispersion and nonlinear coefficient [27] of the mode supported in the proposed fiber is computed by the formula as follows:

$$D(\lambda) = \frac{-\lambda}{c} \frac{d^2 n_{eff}}{d\lambda^2} \tag{1}$$

$$A_{eff} = \frac{\left| \int (e_v \times h_v^*) \cdot \hat{z} \, dA \right|^2}{\left| \int (e_v \times h_v^*) \cdot \hat{z} \, dA \right|^2} \tag{2}$$

$$\int \left| (e_v \times h_v^*) \cdot z \right| \ dA$$

$$2\pi \ \overline{n_2}$$

$$\gamma = \frac{2\pi}{\lambda} \frac{n_2}{A_{eff}} \tag{3}$$

where *c* represents the speed of the light in a vacuum,  $n_{eff}$  indicates the effective index of vortex modes as a function of the wavelength,  $A_{eff}$  is the effective mode area. The nonlinear refractive index  $n_2$  of As<sub>2</sub>S<sub>3</sub> is set as  $3 \times 10^{-18}$  m<sup>2</sup>/W in our simulation [28].

### **B. FLAT AND COHERENT SC GENERATION**

By using the split-step Fourier method and taking into consideration of the loss, dispersion, nonlinearity, and Raman effect [29], we further simulated the supercontinuum generation in the proposed PCF. A chirp-free hyperbolic secant pulse is launched into the optimized PCF. Because the transmission window of sulfide-based fiber is typically from 0.8 to 7  $\mu$ m, the light could not propagate in the proposed fiber when the wavelength is below 800 nm. According to the experiment results of As<sub>2</sub>S<sub>3</sub> PCFs [30], the loss is set to 0.4 dB/m in the wavelength range of 1000 to 2250 nm. From 800 nm, the loss is set as an exponential decay function towards 0.4 dB/m at 1000 nm [31]. For the wavelength range beyond 2250 nm, the confinement loss surpasses 0.4 dB/m, and thus the confinement loss is considered as the propagation loss. Overall, we used the worst possible loss across the spectral range simulated.

Figure 4(a) displays the effects of the peak power P of the input pulse on the supercontinuum after 10-mm fiber when the full width half maximum (FWHM)  $t_{FWHM}$  of the input pulse is 100 fs. The optical spectrum broadens prominently with the increase of the input pulse peak power. As indicated in Fig. 4(b), we change  $t_{FWHM}$  from 50 to 200 fs while P is set as 5 kW. With the  $t_{FWHM}$  of the input pulse decreasing, the flatness of the supercontinuum spectra gets better. Under the condition of constant peak power, the input pulse with larger  $t_{FWHM}$  has more energy and narrower spectra, which means each frequency component carrying more energy leads to stronger nonlinear effect [32]. To further investigate the influence of the pump wavelength on the SC generation, we change the center wavelength  $\lambda_0$  from 1500 to 2500 nm, while keep P as 5 kW and  $t_{FWHM}$  as 100fs. Figure 4(c) illustrates that the SC spectra gradually moves towards the longer wavelength as  $\lambda_0$  increases. Compared with the wavelength at 2000 nm, the SC is smoother when the input pulse pumps at 2500 nm. The spectrum is more fluctuated and the loss is larger as the wavelength increases.

Figure 5 describes the evolution of the supercontinuum along the  $As_2S_3$  fiber, with a 100-fs 5-kW launched pulse. The optical spectrum is broadened along the propagation



**FIGURE 4.** Influence of different input pulse parameters on SC generation of OAM<sub>1,1</sub> after the 10-mm long As<sub>2</sub>S<sub>3</sub> ring PCF for different (a) peak power P ( $t_{FWHM}$  = 100 fs,  $\lambda_0$  = 2000 nm), (b) pulse FWHM  $t_{FWHM}$ (P = 5 kW,  $\lambda_0$  = 2000 nm), (c) central wavelength  $\lambda_0$  ( $t_{FWHM}$  = 100 fs, P = 5 kW).

length, and tends to be stable and flat at 10-mm length. After 10-mm propagation along the fiber, one can see that the input pulse with P = 5 kW,  $t_{FWHM} = 100$  fs is already able to generate a flat and broad 1946-nm supercontinuum from 959 to 2905 nm at -20 dB, which covers 1.6-octave bandwidth. At -10 dB level, the supercontinuum can still cover > 1.4 octave bandwidth from 1038 to 2837 nm.

Figure 6 represents the temporal and spectral evolutions of the pump pulses along the 1.0-cm  $As_2S_3$  PCF. The principle of spectrum broadening in fiber with all-normal dispersion is self-phase modulation (SPM), self-steepening and optical wave breaking (OWB). The normal dispersion and SPM contribute to the initial temporal and spectral evolutions of the pump pulse. The red and blue frequency components are generated near the front and back edges, respectively. In this process, the peak power of the pulse decreases rapidly. Then, the new spectral components are generated because of OWB, which can be explained as a degenerate four-wave mixing



**FIGURE 5.** Octave-spanning OAM<sub>1,1</sub> supercontinuum generated along the proposed PCF (P = 5 kW,  $t_{FWHM} = 100$  fs,  $\lambda_0 = 2000$  nm) with different length.



**FIGURE 6.** Temporal and spectral evolutions of the pump pulse along 10-mm As<sub>2</sub>S<sub>3</sub> PCF (P = 5 kW,  $t_{FWHM} = 100$  fs,  $\lambda_0 = 2000$  nm).

(FWM). As the pulse continues to propagate after 0.1-cm fiber, the walk-off between the new components gets larger with the accumulated dispersion as identified in Fig. 6(a). The spectra are no longer broadened and become smooth after 0.5-cm propagation, as illustrated in Fig. 6(b).

## IV. SUPERCONTINUUM GENERATION OF $\rm TE_{01}$ AND $\rm TM_{01}$ IN PCF WITH ALL-NORMAL DISPERSION

#### A. FIBER PROPERTIES WITH OPTIMIZED DISPERSION

To enable coherent supercontinuum generation of the other vortex modes in the proposed  $As_2S_3$  ring PCF, we further



**FIGURE 7.** Chromatic dispersion of (a) the  $TE_{01}$  mode for different  $r_2$ , (b) the  $TM_{01}$  mode for different  $r_3$ .



**FIGURE 8.** Nonlinear coefficient and confinement loss of the TE<sub>01</sub> ( $d = 0.4 \ \mu$ m,  $r_0 = 0.18 \ \mu$ m,  $r_2 = 0.1 \ \mu$ m,  $r_3 = 0.17 \ \mu$ m,  $r_4 = 0.18 \ \mu$ m,  $r_5$ to  $r_8 = 0.19 \ \mu$ m) and TM<sub>01</sub> ( $d = 0.4 \ \mu$ m,  $r_0 = 0.08 \ \mu$ m,  $r_2 = 0.08 \ \mu$ m,  $r_3 = 0.14 \ \mu$ m,  $r_4 = 0.18 \ \mu$ m,  $r_5$  to  $r_8 = 0.19 \ \mu$ m) modes in the optimized PCF structure parameters.

optimized the geometric parameters to achieve all-normal and near-zero dispersion of the TE<sub>01</sub> and TM<sub>01</sub> modes. Figure 7(a) depicts the chromatic dispersion of the TE<sub>01</sub> mode in the As<sub>2</sub>S<sub>3</sub> PCF with  $r_2$  varied from 0.08  $\mu$ m to 0.12  $\mu$ m ( $d = 0.4 \mu$ m,  $r_0 = 0.18 \mu$ m,  $r_3 = 0.17 \mu$ m,  $r_4 =$ 0.18  $\mu$ m,  $r_5$  to  $r_8 = 0.19 \mu$ m). As the diameter of the first ring of the cladding air hole increases, the dispersion curve at long wavelength region decreases significantly, while the dispersion slightly increases at the short wavelengths. The dispersion is flatter and near zero when  $r_2 = 0.1 \mu$ m. In the



**FIGURE 9.** Effect of different input pulse parameters on the SC generation for TE<sub>01</sub> and TM<sub>01</sub> when the length of the As<sub>2</sub>S<sub>3</sub> ring PCF is 2 mm ( $\lambda_0$  =2500 nm): (a)-(b) peak power P when  $t_{FWHM}$  = 100 fs, (c)-(d) pulse FWHM t<sub>FWHM</sub> when P = 8 kW for TE<sub>01</sub> and P = 20 kW for TM<sub>01</sub>.

proposed PCF, the maximum dispersion of the TE<sub>01</sub> mode is -3.8 ps/(nm·km). An average of -33.8 ps/(nm·km) dispersion is obtained with  $< \pm 30$  ps/(nm·km) variation over a 794-nm bandwidth from 1624 to 2418 nm.

Figure 7(b) displays the dispersion profiles of the TM<sub>01</sub> mode in the As<sub>2</sub>S<sub>3</sub> PCF when  $r_3$  varies from 0.12  $\mu$ m to 0.16  $\mu$ m ( $d = 0.4 \mu$ m,  $r_0 = 0.08 \mu$ m,  $r_2 = 0.08 \mu$ m,



**FIGURE 10.** Octave-spanning supercontinuum of (a) the TE<sub>01</sub> mode (P = 8 kW,  $t_{FWHM} = 100$  fs,  $\lambda_0 = 2500$  nm), and (b) the TM<sub>01</sub> mode (P = 20 kW,  $t_{FWHM} = 100$  fs,  $\lambda_0 = 2500$  nm) generated along the proposed PCF, respectively.

 $r_4 = 0.18 \ \mu\text{m}$ ,  $r_5$  to  $r_8 = 0.19 \ \mu\text{m}$ ). As one can observe in the figure, the chromatic dispersion at short wavelength region increases with increased  $r_3$ , but at longer wavelength the change is reversed. Therefore, the fiber with  $r_3 = 0.14 \ \mu\text{m}$ is selected to achieve all-normal and flatter dispersion. The dispersion varies between -96.1 and -56.1 ps/(nm·km) over a 660-nm bandwidth from 1855 to 2515 nm.

The nonlinear coefficient  $\gamma$  and confinement loss of the TE<sub>01</sub> and TM<sub>01</sub> modes under the optimized structure are depicted in Fig. 8. With the increased wavelength, the nonlinear coefficient decreases and the confinement loss increases. The wavelengths are 2286 nm and 2470 nm, when the confinement loss of the TE<sub>01</sub> and TM<sub>01</sub> modes surpasses 0.4 dB/m, respectively. At 2500 nm, the nonlinear coefficient  $\gamma$  of TE<sub>01</sub> and TM<sub>01</sub> are 4.30 and 2.36 /W/m. Here, their corresponding confinement losses are 0.05 and 0.006 dB/cm, respectively.



**FIGURE 11.** (a)–(c) Temporal and (b)-(d) spectral evolutions of the pump pulse with  $TE_{01}$  and  $TM_{01}$  modes propagating along the optimized PCF.

### **B. FLAT AND COHERENT SC GENERATION**

Figure 9(a)-9(b) depicts the dependence of the supercontinuum spectra on the input pulse peak power P for TE<sub>01</sub> and TM<sub>01</sub> modes after 2-mm fiber, with the center pump wavelength of 2500 nm and the FWHM of 100 fs. The trend is similar as the OAM mode. As one can see in Fig 9, the supercontinuum broadens with the increasing of the peak power due to the stronger nonlinear effects. SPM and OWB effects will flat the SC spectrum until the peak power is saturated, thus the spectrum no longer broadens. As illustrated in Fig. 9(c)-9(d), we also analyze the effect of the input pulse FWHM on the spectra. With the decreased input pulse width, the generated supercontinuum becomes broader and smoother.

Figure 10 summarizes the supercontinua of the  $TE_{01}$  and  $TM_{01}$  modes propagate along the fiber. With the increased propagation length, the SC spectrum broadens and flattens due to SPM and OWB. The spectrum tends to be stable after 2-mm long propagation. A flat and broad SC spectrum of the  $TE_{01}$  mode is generated after 2-mm propagation with >2 octave bandwidth from 819 to 3440 nm at -30 dB. The supercontinuum of the  $TM_{01}$  mode is generated from 849 to 3504 nm at -20 dB. The spectral coverage of the  $TM_{01}$  supercontinuum is also >2 octave bandwidth. The loss of the  $TM_{01}$  mode, which is lower than that of the  $TE_{01}$  mode, contributes to its broadening at long wavelength range.

More details on the generation of supercontinuum are illustrated in Fig. 11. One can see the temporal and spectral evolutions of the pump pulses with the  $TE_{01}$  and  $TM_{01}$  modes propagating along the optimized PCF. The process of



**FIGURE 12.** The coherence of  $HE_{21}$ ,  $TE_{01}$  and  $TM_{01}$  modes generated supercontinuum (*L* represents the length of the fiber).

the SC generation is the same as the  $OAM_{1,1}$  mode which is discussed in section III. The spectra are both broad and smooth after 2-mm propagation.

### **V. COHERENCE**

Figure 12 illustrates the coherence of the generated supercontinua for different modes. Under the combined effects of the SPM and OWB processes, the SC generated in the all-normal dispersion PCF produces new spectra components, which has fixed phase difference compared with the input pulse. Therefore, the highly coherent SC spectrum can be achieved. This is difficult to be achieved for supercontinuum generated with anomalous dispersion where soliton dynamics effect dominates. In the simulation, we add one photon per mode Gaussian noise with a random phase to the input pulse for computing the coherence and execute 20 times. One can see that the coherence is 1 over the entire supercontinuum bandwidth for  $OAM_{1,1}$ ,  $TE_{01}$ , and  $TM_{01}$  modes, respectively.

### **VI. CONCLUSION**

In conclusion, we proposed an As<sub>2</sub>S<sub>3</sub> ring-core PCF, which could guide vortex modes with all normal dispersion and high nonlinearity. By simulating the light guiding though the proposed fiber with different structure parameters, one can find the effect of these parameters on the chromatic dispersion. The all normal and flat dispersion of the  $OAM_{1,1}$ ,  $TE_{01}$ , and TM<sub>01</sub> modes is achieved by optimizing the PCF structure parameters, respectively. Simulations show that the designed fiber with all-normal dispersion could be used in highly coherent and broad supercontinuum generation because of SPM and OWB. With the dispersion varying from -96.5 to -36.5 ps/(nm·km) over a 940-nm bandwidth, the supercontinuum of the  $OAM_{1,1}$  mode is generated from 959 to 2905 nm at -20 dB which covers a 1.6-octave bandwidth by launching a 100-fs 5-kW chirp-free hyperbolic secant pulse into a 1.0-cm designed fiber. The supercontinuum coverage of the  $TE_{01}$  and  $TM_{01}$  modes in the optimized fiber can both be over 2-octave bandwidth. The coherence of the generated

supercontinuum of the three modes all shows nearly perfect property over the whole supercontinuum bandwidth.

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