

Received June 21, 2020, accepted July 4, 2020, date of publication July 7, 2020, date of current version July 20, 2020.

Digital Object Identifier 10.1109/ACCESS.2020.3007767

# Nonsmooth PI Controller for Uncertain Systems

SHARAT CHANDRA MAHTO<sup>1</sup>, (Member, IEEE), DURGESH KUMAR<sup>1</sup>, (Member, IEEE),  
SHYAM KAMAL<sup>1</sup>, (Member, IEEE), ASIF CHALANGA<sup>2</sup>,  
XIAOGANG XIONG<sup>3</sup>, (Member, IEEE), SHANHAI JIN<sup>4</sup>, (Member, IEEE),  
AND SHYAM KRISHNA NAGAR<sup>1</sup>, (Member, IEEE)

<sup>1</sup>Department of Electrical Engineering, Indian Institute of Technology (BHU), Varanasi 221005, India

<sup>2</sup>Department of Computer Science, University College London, London WC1E 6BT, U.K.

<sup>3</sup>Department of Mechanical Engineering and Automation, Harbin Institute of Technology (Shenzhen), Shenzhen 518055, China

<sup>4</sup>School of Engineering, Yanbian University, Yanji 133000, China

Corresponding author: Shanhai Jin (jinshanhai@ybu.edu.cn)

This work was supported in part by the National Natural Science Foundation of China under Grant 61963035, in part by the Research Foundation of Jilin Province Development and Reform Commission under Grant 2019C048-2, and in part by the Shenzhen Peacock Technology Innovation under Grant KQJSCX20170726103546683.

**ABSTRACT** This paper investigates the problem of nonsmooth feedback stabilization for the higher order uncertain chain of integrators. For achieving the specified goal, the integral term of classical Proportional-Integral (PI) controller is replaced by an integral of the discontinuous function. Replacing this integrator, the overall control becomes absolutely continuous rather than discontinuous as in the first order sliding mode control. With this proposed scheme, the property of invariance concerning the matched Lipschitz uncertainty is still preserved. The main technical contribution of the paper is a sound and non-trivial Lyapunov analysis of the closed loop system controlled by nonsmooth PI controller. The effectiveness of the proposed controller is illustrated with the help of numerical simulation on the magnetic suspension system.

**INDEX TERMS** Nonsmooth PI, stability and stabilization, strict Lyapunov function.

## I. INTRODUCTION

Stability, of a perturbed system, is one of the classical problems in the control literature [1]. There are several ways to address this problem. For example, consider the system  $\dot{\chi} = F(\chi, \rho(t)) + G(\chi, \rho(t))u$ ;  $\sigma = h(\chi)$  where  $u$  is the control signal,  $\chi$  is the states of the system,  $\sigma$  is the output, and  $\rho(t)$  represents unknown external perturbations or model uncertainties. In several practical scenarios, one of the main objectives is to construct a feedback control law  $u$  such that the output  $\sigma$  robustly tracks a reference signal  $\sigma_0$ , despite unknown external perturbations or model uncertainties. There are several different methodologies already reported in the literature to simplify the above-mentioned problem for the design of a feedback control  $u$ . One such strategy is known as a normal form [7], [8]

$$\begin{aligned} \dot{\zeta} &= f_0(\zeta, x, d(t)) \\ \dot{x}_i &= x_{i+1}, \quad i = 1, \dots, n-1 \\ \dot{x}_n &= f(\zeta, x, t) + g(\zeta, x, t)u + d(t) \\ \sigma &= x_1 \end{aligned} \quad (1)$$

The associate editor coordinating the review of this manuscript and approving it for publication was Feiqi Deng<sup>1</sup>.

where  $\zeta \in \mathbb{R}^p$  and  $x \in \mathbb{R}^n$  are the states,  $f : \mathbb{R}^p \times \mathbb{R}^n \times [0, \infty) \rightarrow \mathbb{R}^p$  and  $g : \mathbb{R}^p \times \mathbb{R}^n \times [0, \infty) \rightarrow \mathbb{R}$  are known nominal nonlinearities,  $u \in \mathbb{R}$  is the control input, subsystem  $\dot{\zeta} = f_0(\zeta, x, d(t))$  with  $f_0 : \mathbb{R}^p \times \mathbb{R}^n \times [0, \infty) \rightarrow \mathbb{R}^p$  represents the zero dynamics of the system [7], and  $d(t)$  corresponds to uncertainties/perturbations. It has been already reported in literature that if subsystem  $\dot{\zeta} = f_0(\zeta, x, d(t))$  is Input-to-State stable [1] with respect to  $x$  and  $d(t)$ , then the above mentioned tracing problem (1) can be reduced to stabilization of uncertain chain of integrator

$$\begin{aligned} \dot{x}_i &= x_{i+1}, \quad i = 1, \dots, n-1 \\ \dot{x}_n &= f(\zeta, x, t) + g(\zeta, x, t)u + d(t) \\ \sigma &= x_1 \end{aligned} \quad (2)$$

about the equilibrium point  $x = 0$ .

The main intention of control researchers is to investigate the problem that, if the above system with known  $f(\zeta, x, t)$ ,  $g(\zeta, x, t) \neq 0$  is uniformly asymptotically stable at the origin, then what can be said about the stability and behaviour of the perturbed system for  $d(t) \neq 0$  at the equilibrium point  $x = 0$ ? There are several approaches available in the literature to solve this problem. In [1], it is reported that if  $d(t)$  vanishes at the equilibrium point, then classical state

feedback can guarantee the asymptotic stability. However, for nonvanishing disturbances at the origin the memoryless state feedback control (proportional control) doesn't ensure the uniform asymptotical stability of the system [1]. It is found that some classes of nonvanishing perturbations are taken care by the dynamic state feedback like simple PI (proportional-integral feedback control), but it fails to handle the time varying perturbations [2]–[5].

Several delicate controllers have been investigated to enhance control performance and robustness. Sliding mode control (SMC) [6] is one of them. It is one of the most promising control technique for controlling plants under uncertain conditions [10], [17], [18]. However, this controller is still not quite popular in industries because of their discontinuous nature.

In the last two decades, some methods have been proposed to construct continuous control action based on the sliding mode. One such idea is coined by Prof. Levant [13], [14] known as “Higher order sliding mode”. The main idea is to introduce one or more integrators in the system such that the control signal becomes a continuous function [14]. For instance, to obtain the absolute continuous control signal for the system  $\dot{x} = f(t, x) + g(t, x) + u$ ,  $x \in \mathbb{R}$ , an integrator is introduced to increase the order of the system by one and then discontinuous higher order sliding mode algorithm can be used. However, the implementation of these controllers required the knowledge of  $\dot{x}$ . In this case, we can reconstruct perturbation, by computing  $g(t, x) = \dot{x} - f(t, x) - u$ , and it would be possible to compensate it without a discontinuous control [15].

To avoid the above-mentioned drawbacks, a nonlinear PI controller (the Super-twisting algorithm [13], [16], [21]) has been proposed. This controller gives finite time stability in the presence of continuous Lipschitz perturbation for relative degree one system concerning control. However, recently it is found in the literature that the chattering is still there because of the nonlipschitz term in STA which generates the infinite force at the origin [16]. Furthermore, generalization as well as practical implementation of Super-twisting is not so straightforward because one has to maintain homogeneity in order to ensure finite time stability also it is difficult to implement the fractional power in an industrial environment [9], [25]. It is important to mention here that various Lyapunov function that has been suggested for the popular Super-twisting and its variant [11], [22], [23], [26] is not applicable if the nonlinear proportional term is replaced by a linear one. Therefore, it is important to look into that if a proportional term of Super-twisting is replaced by linear one then how to give mathematical guarantee for the convergence of the modified algorithm? The further question of interest: is it possible to extend the same structure for a higher order uncertain case with the mathematical guarantee for the convergence?

## A. MAIN OBJECTIVES

Motivating from the above fact and wide applicability and acceptability of PI and its variants in the industries, it seems

that some more work is required in the area of the classical PI controller for following goals,

- modify classical PI control and give sound mathematical proof to tune gains such that it can handle all kind of Lipschitz disturbances either vanishing or nonvanishing at the origin. (One can further note that if a disturbance is discontinuous, no continuous control can handle it).
- design control such that overall control signal is absolutely continuous.
- propose a controller such that it does not require information on higher derivatives of the state variables to compensate for the differentiable matched disturbances.

## B. MAIN CONTRIBUTIONS

For achieving the specified goal integral part of PI controller is replaced by a discontinuous integrator. Adding this extra integrator overall control is still absolutely continuous rather than first order sliding mode control, but the property of invariance concerning Lipschitz matched uncertainties is still preserved. Finally, we prove the stability of the closed-loop system via a homogeneous, continuously differentiable and strict Lyapunov function. Another advantage of the proposed controller over first order sliding mode is that it is also able to reject ramp time varying disturbances.

The rest of the paper is organized as follows. The notions and preliminaries and problem formulation are established in Section II and IV, respectively. The main results of the paper and discussion about the proposed controller are presented in Section IV. The construction of Lyapunov Function along with the proof of main Theorems and numerical simulation, are documented in V and VI respectively. Finally, some concluding remarks are included in Section VII.

## II. NOTIONS AND PRELIMINARIES

Our notations are standard. We let  $\mathbb{R}$  denote the real numbers and  $\mathbb{R}^+$  denote the nonnegative reals. The dilation operator for  $x = [x_1, \dots, x_n] \in \mathbb{R}^n$  is defined as  $\Delta_\lambda^r := (\lambda^{r_1}x_1, \dots, \lambda^{r_n}x_n)$ ,  $\forall \lambda > 0$ , where  $r_i > 0$  with  $i = 1, \dots, n$  are the weights of the individual coordinate of  $x$ . A functional  $V : \mathbb{R}^n \rightarrow \mathbb{R}$  is said to be (weighted)  $r$ -homogeneous of degree  $h \in \mathbb{R}$  if the following identity  $V(\Delta_\lambda^r x) = \lambda^h V(x)$  holds. Homogeneous functions have several elegant properties, we are going to recall a result about continuous real-valued homogeneous functions ([20], Lemma 4.2), which will be used in the proof of the main Theorems of this note.

*Lemma 1: Suppose  $V_1$  and  $V_2$  are continuous real-valued functions  $V_i : \mathbb{R}^n \rightarrow \mathbb{R}$ , homogeneous with the same weights and degrees  $l_1 > 0$  and  $l_2 > 0$ , respectively, and  $V_1$  is positive-definite. Then for every  $x \in \mathbb{R}^n$ ,*

$$\left[ \min_{\{z:V_1(z)=1\}} [V_1(x)]^{\frac{l_2}{l_1}} \leq V_2(x) \leq \left[ \max_{\{z:V_1(z)=1\}} [V_1(x)]^{\frac{l_2}{l_1}} \right].$$

Also we have used the Young's inequality in order to show the positive definiteness of Lyapunov function, which can be stated as:

*Lemma 2:* The following inequality is always satisfied  $ab \leq c^p \frac{a^p}{p} + c^{-q} \frac{b^q}{q}$ , for any positive real numbers  $a, b, c > 0$  and  $p, q > 1$ , with  $\frac{1}{p} + \frac{1}{q} = 1$ .

Apart from the above two Lemma we use the following notion. For a positive integer  $n$ . The signum vector function  $SIGN(x)$  is a function  $\mathbb{R}^n \rightarrow \mathbb{R}^n$  whose behavior in each coordinate is as per the signum function. Explicitly, it is defined as the function  $(x_1, \dots, x_n) \mapsto (\text{sign}(x_1), \dots, \text{sign}(x_n))$ .

### III. BACKGROUND AND PROBLEM FORMULATION

In this paper, we consider the  $n^{\text{th}}$  order uncertain chain of integrators, given as

$$\begin{aligned} \dot{x}_i &= x_{i+1}, \quad i = 1, \dots, n-1, \\ \dot{x}_n &= u + d(t), \end{aligned} \tag{3}$$

where  $\mathbf{X}^T = [x_1 \ x_2 \ \dots \ x_n] \in \mathbb{R}^{1 \times n}$  are the states,  $u \in \mathbb{R}$  is the control input and  $d(t)$  represents the uncertainties/perturbations. Our main is to design a *continuous or at least absolutely continuous controller*  $u$  such that system (3) stabilizes at the origin despite of the uncertainties/perturbations  $d(t)$ .

For an illustration of the proposed control strategy consider a simplified model of the motion of an underwater vehicle  $\dot{v} + v|v| = \bar{u} + d$  where  $v \in \mathbb{R}$  is the vehicle velocity and  $\bar{u} \in \mathbb{R}$  is the control input (the thrust provided by a propeller) and  $d$  is unknown disturbance due to water wave [24]. One can assume that the disturbance  $d$  is an arbitrary combination of  $\sin(t)$  and  $\cos(t)$ . Suppose that control objective is to maintain constant velocity  $v_d$  in spite of  $d$ . Now suppose  $x_1 := v - v_d$  and  $\bar{u} := u + v|v|$ , then one can write

$$\dot{x}_1 = u + d, \quad x_1 \in \mathbb{R}. \tag{4}$$

In the absence of uncertainties  $d$ , a simple proportional continuous feedback control  $u := \alpha(x_1)$ ,  $\alpha : \mathbb{R} \rightarrow \mathbb{R}$  is able to stabilize the system (4) at the origin. However, above mentioned feedback controller fails to stabilize the system (4) in the presence of non-vanishing perturbation  $d \neq 0$ , because at the origin feedback is zero but perturbations  $d$  are nonzero. Now, suppose the case where perturbation  $d$  is non-vanishing but some unknown constant, then simple continuous PI controller  $u := \alpha(x_1) + \int_0^t k_I x_1(\tau) d\tau$  or  $u := k_P x_1 + \int_0^t k_I x_1(\tau) d\tau$  with proper  $k_P$  and  $k_I$  can stabilize the origin because of the following facts:

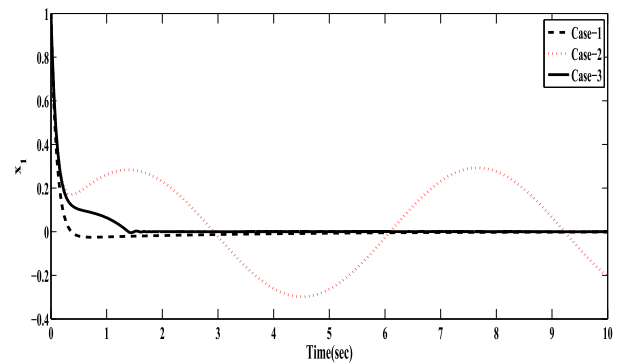
The closed-loop system can be written as  $\dot{x}_1 = \alpha(x_1) + \int_0^t k_I x_1(\tau) d\tau + d$ , which can be further simplified as

$$\dot{x}_1 = \alpha(x_1) + z, \quad \dot{z} = k_I x_1 \tag{5}$$

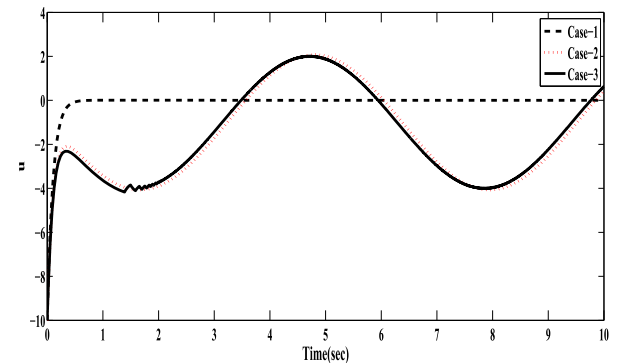
where  $z := \int_0^t k_I x_1(\tau) d\tau + d$ . The closed-loop system (5) is a second order disturbance-free system in the transformed domain. Therefore, using the proper selection of  $\alpha$  and  $k_I$  it is possible to show that origin is asymptotically stable. However, if  $d$  is not constant, then closed loop system is no longer disturbance-free. In such case, we need to rethink about some more appropriate memory based continuous integral controllers. It is important to note here that memoryless

discontinuous control like first order sliding mode can be a choice for the solving the above-mentioned problem provided  $d$  is bounded. However, we aim to find some class of continuous controllers keeping in mind that it is very similar to the existing PI controller and also able to tackle large classes of non vanishing disturbances.

To get a better insight and for further generalization of the result, closed loop system (8) has been simulated in Matlab environment. For the simulation, the controller gains are selected as  $k_1 = 10, k_2 = 3$  and the initial condition of state is chosen as  $x_1(0) = 1$ . Case-1 of Fig. 1 shows state evolution, when classical PI control is applied to the disturbance free system, Case-2 of Fig. 1 demonstrates the state evolution of the system in the presence of disturbance,  $d = 1 + 3 \sin(t)$  when classical PI is applied and finally, Case-3 of Fig. 1 shows the state evolution in the case of proposed nonsmooth PI controller. One can observe that in the presence of disturbance also the proposed controller provides the same response as in the disturbance free case. Simulation results of Fig. 2 in Case-3 also confirm that the control effort is continuous.



**FIGURE 1.** Evolution of state: Case-1 classical PI to the disturbance free system, Case-2 and 3 classical and proposed PI in the presence of disturbances respectively.



**FIGURE 2.** Evolution of control signal: Case-1 classical PI to the disturbance free system, Case-2 and 3 classical and proposed PI in the presence of disturbances respectively.

*Remark 1:* The main benefits of the proposed controller over the first order sliding mode is that overall control is continuous and property of insensitivity with respect to Lipschitz

disturbance is retained. Another advantage of the proposed controller over first order sliding mode is that it is also able to reject ramp (time-varying) disturbances.

#### IV. MAIN RESULTS

##### A. NONSMOOTH PI FOR THE FIRST ORDER SYSTEM (FOR $n = 1$ IN (3))

In this paper, we are going to show that the following Theorem gives the asymptotic stability of the system (4) about the origin, if the nonlinear proportional term of Super-twisting controller  $u := -k_1|x_1|^{1/2}\text{sign}(x_1) - k_2 \int_0^t \text{sign}(x_1(\tau))d\tau$  is replaced by linear one  $u = -k_1x_1 - k_2 \int_0^t \text{sign}(x_1(\tau))d\tau$  where  $k_1$  and  $k_2$  are the designed parameters.

**Theorem 1:** Consider the system (4) with  $|\dot{d}(t)| \leq d_0; \forall t \geq 0$ . Then the nonsmooth control law

$$u = -k_1x_1 - k_2 \int_0^t \text{sign}(x_1(\tau))d\tau \quad (6)$$

stabilizes the origin asymptotically in spite of disturbance  $d(t)$  for any  $k_1 > 0$  and  $d_0 \leq k_2 \leq L(t) \left( \pi_1 + \frac{2\frac{3}{2}}{3}\pi_2 \right)$  with

$\pi_1 \geq \frac{2^2 2^{\frac{5}{6}}}{3^2} \pi_2$  where  $\pi_i; i = 1, 2$  are some positive constants and  $L : \mathbb{R}^+ \rightarrow \mathbb{R}^+$  is the some positive continuously differential function with  $0 < c_2^{-1} \leq L(t) \leq c_1$ , and  $\dot{L}(t) \in [0, c_3]; \forall t \geq 0$  where  $c_1, c_2$  and  $c_3$  are fixed constants.

**Remark 2:** System (4) can be re-written as  $\dot{x}_1 = -k_1x_1 + z, \dot{z} = -(k_2 - \dot{d}(t) \text{sign}(x_1)) \text{sign}(x_1)$ . Therefore, stability of  $\dot{x}_1 = -k_1x_1 + z, \dot{z} = -k'(t) \text{sign}(x_1), k' : \mathbb{R}^+ \rightarrow \mathbb{R}^+$  implies the stability of system (6). The same is reflected in Theorem 1.

##### B. NONSMOOTH PI FOR THE HIGHER ORDER UNCERTAIN CHAIN OF INTEGRATORS

The following Theorem gives the asymptotic stability of the system (3).

**Theorem 2:** Consider the system (3) with  $|\dot{d}(t)| \leq d_0; \forall t \geq 0$ . Then the nonsmooth control law

$$u = -\mathbf{K}_p \mathbf{X} - \int_0^t K_I \text{sign}(\mathbf{K}_p \mathbf{X}) d\tau \quad (7)$$

stabilizes the origin asymptotically in spite of disturbance  $d(t)$  if  $\mathbf{K}_p$  and  $K_I$  are selected such that

- all the eigenvalues of matrix  $\mathbf{Q} := (\mathbf{A} - \mathbf{B}\mathbf{K}_p)$  must be negative and real for any proper selection of  $\mathbf{K}_p = [k_1 \ k_2 \ \dots \ k_n]$  and

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & 0 \end{bmatrix} \text{ and } \mathbf{B} = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 1 \end{bmatrix},$$

- and gain  $K_I$  satisfy  $d_0 \leq K_I \leq L(t) \left( -\pi_1 \|\mathbf{B}\| + \frac{2\frac{3}{2}}{3}\pi_2 \mathbf{B} \right)$

with  $\frac{2\frac{3}{2}}{3} \|\pi_2\| \geq \pi_1 \geq \frac{2^2 2^{\frac{5}{6}}}{3^2} \|\pi_2\|$  where  $\pi_1$  is any positive constant and  $L : \mathbb{R}^+ \rightarrow \mathbb{R}^+$  is the some

positive continuously differential function with  $0 < c_2^{-1} \leq L(t) \leq c_1$ , and  $\dot{L}(t) \in [0, c_3]; \forall t \geq 0$  where  $c_1, c_2$  and  $c_3$  are fixed constants and  $\pi_2 = [\pi_{21} \ \pi_{22} \ \dots \ \pi_{2n}]$  with some positive constants  $\pi_{2i} > 0$  for  $i = 1, \dots, n$ .

**Remark 3:** The main benefit of the proposed controller over the first-order sliding mode is that overall control is continuous, and property of insensitivity concerning differentiable disturbance is retained. Another advantage of the proposed controller over the first-order sliding mode is that it can also reject ramp time-varying disturbances.

##### V. CONSTRUCTION OF LYAPUNOV FUNCTION AND PROOF OF MAIN THEOREMS

Next result states the detailed proof of Theorem 1.

**Proof 1:** On substitution of the proposed controller (6) into (8), the closed loop system is given by

$$\dot{x}_1 = -k_1x_1 + z, \dot{z} = -k_2 \text{sign}(x_1) + \dot{d} \quad (8)$$

where  $z(t) := -k_2 \int_0^t \text{sign}(x_1(\tau))d\tau + d$ . The solution of (8) is understood in the sense of Fillipov [19]. By introducing time-varying change of variables

$$z_1(t) = \frac{x(t)}{L(t)}, z_2(t) = \frac{z(t)}{L(t)}, L(t) > 0, \forall t \geq 0 \quad (9)$$

In the new co-ordinates, system (8) is given by

$$\dot{z}_1 = -\left(k_1 + \frac{\dot{L}}{L}\right)z_1 + z_2, \dot{z}_2 = -\frac{k_2}{L} \text{sign}(z_1) + \frac{\dot{d}}{L} - z_2 \frac{\dot{L}}{L} \quad (10)$$

In general, an algebraic equivalence of systems (8) and (10) does not preserve the stability properties of a dynamical system. For this, it is necessary and sufficient to have topological equivalence: algebraic equivalence plus the condition  $|L(t)| \leq c_1$  and  $|L^{-1}(t)| \leq c_2$  where  $c_1$  and  $c_2$  are fixed constants [12]. Also, system (8) and (10) are not homogenous or weighted homogeneous. Still, one can use the weighted homogeneous Lyapunov function to prove stability. Also, the various Lyapunov function that has been suggested for the Super-twisting is not straightforwardly applicable to the proposed nonsmooth PI. Therefore, we have looked at some different Lyapunov analysis which is also the main technical contribution of this note. Consider the following Lyapunov function in the new coordinates

$$V(z) = \left(\pi_1 |z_1| + \frac{1}{2}z_2^2\right)^{\frac{3}{2}} + \pi_2 z_1 z_2 \geq \left(\pi_1 |z_1| + \frac{1}{2}z_2^2\right)^{\frac{3}{2}} - \pi_2 |z_1||z_2| \quad (11)$$

Applying norm inequality to  $\left(\pi_1 |z_1| + \frac{1}{2}z_2^2\right)^{\frac{3}{2}}$  and Young's inequality (see Lemma 2) to term  $\pi_2 |z_1||z_2|$ , we are going to

show that proposed Lyapunov function (11) is bounded from below by zero.

$$V(z) \geq (\pi_1 |z_1|)^{\frac{3}{2}} + \left(\frac{1}{2} z_2^2\right)^{\frac{3}{2}} - \pi_2 \left(\frac{2}{3} g^{\frac{3}{2}} |z_1|^{\frac{3}{2}} + \frac{1}{3} g^{-3} |z_2|^3\right) \\ = \left(\pi_1^{\frac{3}{2}} - \frac{2}{3} \pi_2 g^{\frac{3}{2}}\right) |z_1|^{\frac{3}{2}} + \left(\left(\frac{1}{2}\right)^{\frac{3}{2}} - \frac{1}{3} \pi_2 g^{-3}\right) |z_2|^3.$$

where  $g \geq 0$ .

It is important to note here that  $V \geq 0$  for all  $z$  if each of  $\left(\pi_1^{\frac{3}{2}} - \frac{2}{3} \pi_2 g^{\frac{3}{2}}\right)$  and  $\left(\frac{1}{2}\right)^{\frac{3}{2}} - \frac{1}{3} \pi_2 g^{-3}$  should be greater than 0. Suppose

$$2^{\frac{1}{2}} \left(\frac{\pi_2}{3}\right)^{\frac{1}{3}} < g < \left(\frac{3}{2\pi_2}\right)^{\frac{2}{3}} \pi_1,$$

which implies

$$\left(\frac{3}{2\pi_2}\right)^{\frac{2}{3}} \pi_1 > 2^{\frac{1}{2}} \left(\frac{\pi_2}{3}\right)^{\frac{1}{3}}.$$

Thus,  $\pi_1 \geq \frac{2^{\frac{1}{2}} \pi_2^{\frac{2}{3}}}{3} \pi_2$ . Selecting  $g$  to be the linear combination of  $2^{\frac{1}{2}} \left(\frac{\pi_2}{3}\right)^{\frac{1}{3}}$  and  $\left(\frac{3}{2\pi_2}\right)^{\frac{2}{3}} \pi_1$  will lead to  $V \geq 0$ . Thus  $g = \alpha 2^{\frac{1}{2}} \left(\frac{\pi_2}{3}\right)^{\frac{1}{3}} + (1 - \alpha) \left(\frac{3}{2\pi_2}\right)^{\frac{2}{3}} \pi_1$ ,  $0 \leq \alpha \leq 1$ . Now our next aim is to show  $\dot{V} < 0$ ,

$$\dot{V} = \left\{ \frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} \pi_1 \text{sign}(z_1) + \pi_2 z_2 \right\} \dot{z}_1 \\ + \left\{ \frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} z_2 + \pi_2 z_1 \right\} \dot{z}_2 \\ = -\frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right) \chi + \pi_2 z_2^2 - \pi_2 \left(k_1 + \frac{\dot{L}}{L}\right) z_1 z_2 \\ - \pi_2 \frac{k_2}{L} \text{sign}(z_1) z_1 + \pi_2 z_1 \frac{\dot{d}}{L} - \pi_2 z_1 z_2 \frac{\dot{L}}{L},$$

where  $\chi := \pi_1 \text{sign}(z_1) \left(\left(k_1 + \frac{\dot{L}}{L}\right) z_1 - z_2\right) + z_2 \left(\frac{k_2}{L} \text{sign}(z_1) + z_2 \frac{\dot{L}}{L} - \frac{\dot{d}}{L}\right)$ . One can also rewrite  $\dot{V}$  as,

$$\dot{V} = -W_1(z) \left(\frac{\dot{L}}{L}\right) + W_2(z) \left(\frac{\dot{d}}{L}\right) - W_3^*(z), \quad (12)$$

where

$$W_1(z) = \frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} \left(\pi_1 |z_1| + z_2^2\right) + 2\pi_2 z_1 z_2 \\ W_2(z) = \frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} z_2 + \pi_2 z_1 \\ W_3^*(z) = \left(\frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} k_1 \pi_1 + \pi_2 \frac{k_2}{L}\right) |z_1| \\ + \frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} \left(\frac{k_2}{L} - \pi_1\right) \text{sign}(z_1 z_2) |z_2| \\ - \pi_2 z_2^2 + \pi_2 k_1 z_1 z_2. \quad (13)$$

We are going to show that  $W_3^*(z)$  would dominate over  $W_2(z)$ , given that  $|\dot{d}| < k_2$ . Since,

$$\frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} |z_2| \geq \frac{3}{2} \left(\frac{1}{2}\right)^{\frac{1}{2}} z_2^2,$$

therefore,

$$\pi_2 (2)^{\frac{1}{2}} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} |z_2| \geq -\pi_2 z_2^2 \text{ and } W_3^* \leq W_3',$$

where,

$$W_3' = \left\{ \frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} k_1 \pi_1 + \pi_2 \frac{k_2}{L} \right\} |z_1| \\ + \left\{ \frac{3}{2} \left(\pi_1 + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} \chi_1 \right\} |z_2| + \pi_2 k_1 z_1 z_2, \quad (14)$$

where  $\chi_1 := \left(\frac{k_2}{L} \text{sign}(z_1 z_2) - \pi_1 \text{sign}(z_1 z_2) + \frac{2^{\frac{3}{2}}}{3} \pi_2\right)$ .

Again, as  $z_1 z_2 \leq \frac{2}{3} c^{\frac{3}{2}} |z_1|^{\frac{3}{2}} + \frac{1}{3} c^{-3} |z_2|^3$ , so  $W_3' \leq W_3$ , where  $W_3$  can be written as

$$W_3 = \left\{ \frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} k_1 \pi_1 + \pi_2 \frac{k_2}{L} \right\} |z_1| \\ + \left\{ \frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} \chi_1 \right\} |z_2| \\ + \pi_2 k_1 \left(\frac{2}{3} c^{\frac{3}{2}} |z_1|^{\frac{3}{2}} + \frac{1}{3} c^{-3} |z_2|^3\right). \quad (15)$$

Since  $\left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}} |z_1| \geq \pi_1^{\frac{1}{2}} |z_1|^{\frac{3}{2}}$ ,  $2 \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right) |z_2| \geq |z_2|^3$ ,  $W_3^f \geq W_3$ , where  $W_3^f$  can be written as,

$$W_3^f = \left\{ \chi_2 \left(k_1 \pi_1 + \frac{4}{9} \pi_2 k_1 \pi_1^{-\frac{1}{2}} c^{\frac{3}{2}}\right) + \pi_2 \frac{k_2}{L} \right\} |z_1| \\ + \chi_2 \left(\chi_1 + \frac{4}{9} \pi_2 k_1 c^{-3} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}}\right) |z_2|, \quad (16)$$

where  $\chi_2 := \frac{3}{2} \left(\pi_1 |z_1| + \frac{1}{2} z_2^2\right)^{\frac{1}{2}}$ . For  $W_3^f$  to be greater than zero  $\forall z$ , both the coefficients of equation (16) should be independently greater than zero, that is, if

$$\chi_2 \left(k_1 \pi_1 + \frac{4}{9} \pi_2 k_1 \pi_1^{-\frac{1}{2}} c^{\frac{3}{2}}\right) + \pi_2 \frac{k_2}{L} \geq 0, \\ \left(\frac{k_2}{L} - \pi_1\right) \text{sign}(z_1 z_2) + \frac{2^{\frac{3}{2}}}{3} \pi_2 + \frac{8}{27} \pi_2 k_1 c^{-3} \chi_2 \geq 0. \quad (17)$$

These two inequalities are satisfied if,

$$\frac{k_2}{L} - \pi_1 + \frac{2^{\frac{3}{2}}}{3} \pi_2 + \frac{8}{27} \pi_2 k_1 c^{-3} \chi_2 \geq 0 \\ -\frac{k_2}{L} + \pi_1 + \frac{2^{\frac{3}{2}}}{3} \pi_2 + \frac{8}{27} \pi_2 k_1 c^{-3} \chi_2 \geq 0, \quad (18)$$

which can be rewritten as

$$0 \leq k_2 \leq L \left( \pi_1 + \frac{2^{\frac{3}{2}}}{3} \pi_2 \right). \quad (19)$$

Since,

$$W_3^f(z) \geq W_3^{f*}(z) \triangleq \alpha |z_1| + \beta \left( \pi_1 |z_1| + \frac{1}{2} z_2^2 \right)^{\frac{1}{2}} |z_2|, \quad (20)$$

with

$$\begin{aligned} \alpha &= \min_z \left[ \chi_2 \left( k_1 \pi_1 + \frac{4}{9} \pi_2 k_1 \pi_1^{-\frac{1}{2}} c^{\frac{3}{2}} \right) + \pi_2 \frac{k_2}{L} \right] \geq 0 \\ \beta &= \min_z \left[ \chi_1 + \frac{8}{27} \pi_2 k_1 c^{-3} \chi_2 \right] \geq 0, \end{aligned} \quad (21)$$

$W_3^{f*}(z)$  is a continuous and homogeneous positive definite function. According to Lemma 1, it follows that  $\forall z \in \mathbb{R}^2$ ,

$$W_2(z) \leq \gamma W_3^{f*}(z) \text{ is satisfied, with } \gamma = \max_{\{z: W_3^{f*}(z)=1\}} > 0,$$

because both  $W_2(z)$  and  $W_3^{f*}(z)$  are continuous and homogeneous with same weights and degree. Finally,

$$\begin{aligned} W_1(z) &= \frac{3}{2} \left( \pi_1 |z_1| + \frac{1}{2} z_2^2 \right)^{\frac{1}{2}} \left( \pi_1 |z_1| + z_2^2 \right) + 2\pi_2 z_1 z_2 \\ &\geq \frac{3}{2} (\pi_1 |z_1|)^{\frac{1}{2}} \pi_1 |z_1| + \frac{3}{2} \left( \frac{1}{2} z_2^2 \right)^{\frac{1}{2}} z_2^2 \\ &\quad - 2\pi_2 \left( \frac{2}{3} g^{\frac{3}{2}} |z_1|^{\frac{3}{2}} + \frac{1}{3} g^{-3} |z_2|^3 \right) \\ &= \left( \frac{3}{2} \pi_1^{\frac{3}{2}} - \frac{4}{3} \pi_2 g^{\frac{3}{2}} \right) |z_1|^{\frac{3}{2}} + \left( \frac{3}{2^{\frac{3}{2}}} - \frac{2\pi_2}{3} g^{-3} \right) |z_2|^3 \end{aligned} \quad (22)$$

$W_1(z)$  is positive-definite if  $\frac{3}{2} \pi_1^{\frac{3}{2}} - \frac{4}{3} \pi_2 g^{\frac{3}{2}} > 0$  and  $\frac{3}{2^{\frac{3}{2}}} - \frac{2\pi_2}{3} g^{-3} > 0$  or equivalently

$$\frac{2^{\frac{5}{6}}}{3^{\frac{5}{3}}} \pi_2^{\frac{1}{3}} < g < \frac{3^{\frac{4}{3}}}{2^2} \frac{\pi_1}{\pi_2^{\frac{2}{3}}}$$

and such a  $g$  exists if  $\pi_1 > \frac{2^{\frac{5}{6}} 2^2}{3^2} \pi_2$ . Thus  $\pi_1$  should be selected such that  $\pi_1 > \frac{2^{\frac{5}{6}} 2^2}{3^2} \pi_2$ . It can be noted that it also fulfills  $\pi_1 \geq \frac{2^{\frac{1}{2}} 2^{\frac{2}{3}}}{3} \pi_2$  required for  $V \geq 0$ . This completes the proof.  $\square$

### A. PROOF OF THEOREM 2

*Proof 2:* After applying proposed controller (7) into (3), the closed loop system is given by

$$\begin{aligned} \dot{\mathbf{X}} &= \mathbf{A}\mathbf{X} - \mathbf{B}\mathbf{K}_P\mathbf{X} + \mathbf{B}\mathbf{Z} \\ \dot{\mathbf{Z}} &= -K_I \text{sign}(\mathbf{K}_P\mathbf{X}) + \dot{d} \end{aligned} \quad (23)$$

where,  $\mathbf{Z} = -\int_0^t K_I \text{sign}(\mathbf{K}_P\mathbf{X}) d\tau + d$ . On applying the following time-varying change of variables,  $\mathbf{Z}_1(t) := \frac{\mathbf{X}(t)}{L(t)}$ ,  $Z_2(t) := \frac{Z(t)}{L(t)}$ , one can rewrite the (23) as

$$\begin{aligned} \dot{\mathbf{Z}}_1 &= -\left( \frac{\dot{L}}{L} \mathbf{I} + \mathbf{B}\mathbf{K}_P - \mathbf{A} \right) \mathbf{Z}_1 + \mathbf{B}Z_2 \\ \dot{Z}_2 &= -\frac{\dot{L}}{L} Z_2 - \frac{K_I}{L} \frac{\mathbf{K}_P\mathbf{Z}_1}{\|\mathbf{K}_P\mathbf{Z}_1\|} + \frac{\dot{d}}{L}, \end{aligned} \quad (24)$$

where  $\mathbf{I}$  is an identity matrix and  $L(t)$  is some continuously differentiable time varying positive function  $\mathbb{C}^1$  i.e.,  $L(t) > 0 \forall t \geq 0$  and  $\dot{L} > 0$  exists. Also, to maintain topological equivalence so that stability of transferred system (24) implies stability of original closed loop system (23) we are further assuming that  $|L(t)| \leq c_1$  and  $|L^{-1}(t)| \leq c_2$  (where  $c_1$  and  $c_2$  are fixed constants [12]).

Now consider the  $V(\mathbf{Z})$  be a Lyapunov function in the new co-ordinates

$$V(\mathbf{Z}) = \left( \pi_1 \|\mathbf{Z}_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{3}{2}} + \pi_2 \mathbf{Z}_1 Z_2, \quad (25)$$

where  $\mathbf{Z} := [\mathbf{Z}_1^T \ Z_2]^T$ ,  $\pi_1 > 0$  and  $\pi_2 = [\pi_{21} \ \pi_{22} \ \dots \ \pi_{2n}]$  with  $\pi_{2i} > 0$  for  $i = 1, \dots, n$ . Next using Young's (see Lemma 2) and norm inequalities, we are going to show that proposed Lyapunov function (25) is bounded from below by zero.

$$\begin{aligned} V(\mathbf{Z}) &\geq (\pi_1 \|\mathbf{Z}_1\|)^{\frac{3}{2}} + \left( \frac{1}{2} Z_2^2 \right)^{\frac{3}{2}} \\ &\quad - \|\pi_2\| \left( \frac{2}{3} g^{\frac{3}{2}} \|\mathbf{Z}_1\|^{\frac{3}{2}} + \frac{1}{3} g^{-3} |Z_2|^3 \right), \quad g \geq 0 \\ &= \left( \pi_1^{\frac{3}{2}} - \frac{2}{3} \|\pi_2\| g^{\frac{3}{2}} \right) \|\mathbf{Z}_1\|^{\frac{3}{2}} \\ &\quad + \left( \left( \frac{1}{2} \right)^{\frac{3}{2}} - \frac{1}{3} \|\pi_2\| g^{-3} \right) |Z_2|^3. \end{aligned} \quad (26)$$

For  $V \geq 0$ ;  $\forall \mathbf{Z}$ , we have selected  $\pi_1 \geq \frac{2^{\frac{1}{2}} 2^{\frac{2}{3}}}{3} \|\pi_2\|$  and  $g = \alpha 2^{\frac{1}{2}} \left( \frac{\pi_2}{3} \right)^{\frac{1}{3}} + (1 - \alpha) \left( \frac{3}{2\|\pi_2\|} \right)^{\frac{2}{3}} \pi_1$ ,  $0 \leq \alpha \leq 1$  same as first order case.

Time derivative of Lyapunov function (25) along the system trajectory (24)

$$\begin{aligned} \dot{V}(\mathbf{Z}) &= \left( \Theta \pi_1 \text{SIGN}(\mathbf{Z}_1^T) + \pi_2 Z_2 \right) \dot{\mathbf{Z}}_1 + \left( \Theta Z_2 + \pi_2 \mathbf{Z}_1 \right) \dot{Z}_2 \\ &= \left( \Theta \pi_1 \text{SIGN}(\mathbf{Z}_1^T) + \pi_2 Z_2 \right) \\ &\quad \left( -\left( \frac{\dot{L}}{L} \mathbf{I} + \mathbf{B}\mathbf{K}_P - \mathbf{A} \right) \mathbf{Z}_1 + \mathbf{B}Z_2 \right) \\ &\quad + \left( \Theta Z_2 + \pi_2 \mathbf{Z}_1 \right) \left( -\frac{\dot{L}}{L} Z_2 - \frac{K_I}{L} \frac{\mathbf{K}_P\mathbf{Z}_1}{\|\mathbf{K}_P\mathbf{Z}_1\|} + \frac{\dot{d}}{L} \right), \end{aligned} \quad (27)$$

where

$$\Theta := \frac{3}{2} \left( \pi_1 \|\mathbf{Z}_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}}$$

or

$$\dot{V}(Z) = -W_1 \left( \frac{\dot{L}}{L} \right) + W_2 \left( \frac{\dot{d}}{L} \right) - W_3^*, \quad (28)$$

where,

$$W_1 = \frac{3}{2} \left( \pi_1 \|Z_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}} \left( \pi_1 \|Z_1\| + Z_2^2 \right) + 2Z_2 \pi_2 Z_1 \quad (29a)$$

$$W_2 = \frac{3}{2} \left( \pi_1 \|Z_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}} Z_2 + \pi_2 Z_1 \quad (29b)$$

$$W_3^* = \frac{3}{2} \left( \pi_1 \|Z_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}} \Xi + \pi_2 Z_2 (\mathbf{BK}_P - \mathbf{A}) Z_1 - Z_2^2 \pi_2 \mathbf{B} + \frac{K_I}{L} \pi_2 Z_1 \text{sign}(\mathbf{K}_P Z_1) \quad (29c)$$

where

$$\Xi := \pi_1 \frac{Z_1^\top (\mathbf{BK}_P - \mathbf{A}) Z_1}{\|Z_1\|} - \pi_1 Z_2 \frac{Z_1^\top \mathbf{B}}{\|Z_1\|} + Z_2 \frac{K_I}{L} \text{sign}(\mathbf{K}_P Z_1).$$

We are going to show that  $W_3^*$  would dominate over  $W_2$ , given that  $|\dot{d}| < K_I$ .

Since, we have selected  $\mathbf{K}_P$  such that  $\mathbf{Q} := \mathbf{BK}_P - \mathbf{A}$  has positive eigenvalues. Then using Rayleigh inequality one can write  $\lambda_{\min}\{\mathbf{Q}\} \|Z_1\|^2 \leq Z_1^\top \mathbf{Q} Z_1 \leq \lambda_{\max}\{\mathbf{Q}\} \|Z_1\|^2$ , where  $\lambda_{\min}\{\mathbf{Q}\}$  and  $\lambda_{\max}\{\mathbf{Q}\}$  are the minimum and maximum eigenvalues of the matrix  $\mathbf{Q}$ . One can further write  $\pi_1 \frac{Z_1^\top (\mathbf{BK}_P - \mathbf{A}) Z_1}{\|Z_1\|} \leq \pi_1 \lambda_{\max}\{\mathbf{Q}\} \|Z_1\|$ . Furthermore,  $\frac{K_I}{L} \pi_2 Z_1 \text{sign}(\mathbf{K}_P Z_1) \leq \frac{K_I}{L} \|\pi_2\| \|Z_1\|$ , provided  $K_I \geq 0$  and  $\pi_1 Z_2 \frac{Z_1^\top \mathbf{B}}{\|Z_1\|} \leq \pi_1 \|\mathbf{B}\| |Z_2|$ . Therefore,  $W_3^* < W_3''$ , where

$$W_3'' := \frac{3}{2} \left( \pi_1 \|Z_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}} \Theta_1 + \pi_2 Z_2 (\mathbf{BK}_P - \mathbf{A}) Z_1 - Z_2^2 \pi_2 \mathbf{B} + \frac{K_I}{L} \alpha_1 \|\mathbf{K}_P\| \|Z_1\|. \quad (30)$$

where  $\alpha_1 := \pi_2 \mathbf{K}_P^\top (\mathbf{K}_P \mathbf{K}_P^\top)^{-1} > 0$  and  $\Theta_1 := \pi_1 \lambda_{\max}\{\mathbf{Q}\} \|Z_1\| + \pi_1 \|\mathbf{B}\| Z_2 + \frac{K_I}{L} \text{sign}(Z_2 \mathbf{K}_P Z_1) |Z_2|$ . Since,  $\frac{3}{2} \left( \pi_1 \|Z_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}} |Z_2| \geq \frac{3}{2} \left( \frac{1}{2} \right)^{\frac{1}{2}} z_2^2$ , therefore,

$$W_3^{iv} = \frac{3}{2} \left( \pi_1 \|Z_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}} \Theta_2 + \pi_2 Z_2 (\mathbf{BK}_P - \mathbf{A}) Z_1 + \frac{K_I}{L} \alpha_1 \|\mathbf{K}_P\| \|Z_1\|, \quad (31)$$

where

$$\Theta_2 := \pi_1 \lambda_{\max}\{\mathbf{Q}\} \|Z_1\| + \pi_1 \|\mathbf{B}\| Z_2 + \frac{K_I}{L} \text{sign}(Z_2 \mathbf{K}_P Z_1) |Z_2| + \frac{2^{\frac{3}{2}}}{3} \pi_2 \mathbf{B} |Z_2|. \quad (32)$$

Again, as

$$\|Z_1\| |Z_2| \leq \frac{2}{3} c^{\frac{3}{2}} \|Z_1\|^{\frac{3}{2}} + \frac{1}{3} c^{-3} |Z_2|^3; c > 0, \quad (33a)$$

$$\left( \pi_1 \|Z_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}} \|Z_1\| \geq \pi_1^{\frac{1}{2}} \|Z_1\|^{\frac{3}{2}}, \quad (33b)$$

$$2 \left( \pi_1 \|Z_1\| + \frac{1}{2} Z_2^2 \right) |Z_2| \geq |Z_2|^3. \quad (33c)$$

So  $W_3^{iv} \leq W_3^{vi}$ , where  $W_3^{vi}$  can be written as

$$W_3^{vi} = \left( \Theta \Theta_3 + \frac{K_I}{L} \alpha_1 \|\mathbf{K}_P\| \right) \|Z_1\| + \Theta \left( \Theta_4 + \frac{8}{27} c^{-3} \Theta (\|\pi_2\| \|\mathbf{BK}_P - \mathbf{A}\|) \right) |Z_2|, \quad (34)$$

where,

$$\Theta_3 := \pi_1 \lambda_{\max}\{\mathbf{Q}\} + \frac{4}{9} c^{\frac{3}{2}} \pi_1^{-\frac{1}{2}} (\|\pi_2\| \|\mathbf{BK}_P - \mathbf{A}\|), \quad (35)$$

$$\Theta_4 := \pi_1 \|\mathbf{B}\| \text{sign}(Z_2) + \frac{K_I}{L} \text{sign}(Z_2 \mathbf{K}_P Z_1) + \frac{2^{\frac{3}{2}}}{3} \pi_2 \mathbf{B} \quad (36)$$

For  $W_3^{vi}$  to be greater than zero  $\forall Z$ , both the coefficients  $\Theta_3$  and  $\Theta_4$  of equation (34) should be independently greater than zero, that is, if

$$\pm \pi_1 \|\mathbf{B}\| \pm \frac{K_I}{L} + \frac{2^{\frac{3}{2}}}{3} \pi_2 \mathbf{B} \geq 0. \quad (37)$$

For inequality  $\Theta_4 \geq 0$  to be satisfied, all of inequalities (37) have to be satisfied, which can be re-written as

$$0 \leq K_I \leq L \left( -\pi_1 \|\mathbf{B}\| + \frac{2^{\frac{3}{2}}}{3} \pi_2 \mathbf{B} \right). \quad (38)$$

Furthermore, (38) is satisfied only if  $\frac{2^{\frac{3}{2}}}{3} \|\pi_2\| \geq \pi_1$ . Since,

$$W_3^{vi}(Z) \geq W_3^{vi*}(Z) \triangleq \alpha \|Z_1\| + \beta \left( \pi_1 \|Z_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}} |Z_2|, \quad (39)$$

with

$$\alpha = \min_Z \left[ \Theta \Theta_3 + \frac{K_I}{L} \alpha \|\mathbf{K}_P\| \right] \geq 0$$

$$\beta = \min_Z \left[ \Theta_4 + \frac{8}{27} c^{-3} \Theta (\|\pi_2\| \|\mathbf{BK}_P - \mathbf{A}\|) \right] \geq 0, \quad (40)$$

$W_3^{vi*}(Z)$  is a continuous and homogeneous positive definite function. According to Lemma 1, it follows that  $\forall Z \in \mathbb{R}^{n+1}$ ,  $W_2(Z) \leq \gamma W_3^{vi*}(Z)$  is satisfied, with  $\gamma = \max_{\{Z: W_3^{vi*}(Z)=1\}} > 0$ , because both  $W_2(Z)$  and  $W_3^{vi*}(Z)$  are continuous and homogeneous with same weights and degree.

$$W_1(Z) = \frac{3}{2} \left( \pi_1 \|Z_1\| + \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}} \left( \pi_1 \|Z_1\| + Z_2^2 \right) + 2Z_2 \pi_2 Z_1$$

$$\geq \frac{3}{2} (\pi_1 \|Z_1\|)^{\frac{1}{2}} \pi_1 \|Z_1\| + \frac{3}{2} \left( \frac{1}{2} Z_2^2 \right)^{\frac{1}{2}} Z_2^2$$

$$- 2 \|\pi_2\| \left( \frac{2}{3} g^{\frac{3}{2}} \|Z_1\|^{\frac{3}{2}} + \frac{1}{3} g^{-3} |Z_2|^3 \right)$$

$$= \left( \frac{3}{2} \pi_1^{\frac{3}{2}} - \frac{4}{3} \|\pi_2\| g^{\frac{3}{2}} \right) \|Z_1\|^{\frac{3}{2}} + \left( \frac{3}{2^{\frac{3}{2}}} - \frac{2 \|\pi_2\|}{3} g^{-3} \right) |Z_2|^3. \quad (41)$$

$W_1(z)$  is positive-definite if  $\frac{3}{2}\pi_1^{\frac{3}{2}} - \frac{4}{3}\|\pi_2\|g^{\frac{3}{2}} > 0$  and  $\frac{3}{2} - \frac{2\|\pi_2\|}{3}g^{-3} > 0$  or equivalently  $\frac{2\sqrt[5]{6}}{3}\|\pi_2\|^{\frac{1}{3}} < g < \frac{3\sqrt[4]{3}}{2^2}\frac{\pi_1}{\|\pi_2\|^{\frac{2}{3}}}$  and such a  $g$  exists if  $\pi_1 > \frac{2\sqrt[5]{6}2^2}{3^2}\|\pi_2\|$ . Thus  $\pi_1$  should be selected such that  $\pi_1 > \frac{2\sqrt[5]{6}2^2}{3^2}\|\pi_2\|$ . It can be noted that it also fulfills  $\pi_1 \geq \frac{2\sqrt[5]{6}2^2}{3}\|\pi_2\|$  required for  $V \geq 0$ . This completes the proof.  $\square$

**VI. SIMULATION**

We demonstrate the robustness of nonsmooth PI control for the third order uncertain chain of integrators containing constant or time-varying matched disturbances. Consider the following magnetic suspension system [1]

$$\begin{aligned} \dot{z}_1 &= z_2 \\ \dot{z}_2 &= -\frac{k_F}{m}z_2 + g_c - \frac{k_M}{2m}\left(\frac{z_3}{z_1 + q}\right)^2 \\ \dot{z}_3 &= -\frac{R}{L(z_1)}z_3 + \frac{k_M}{L(z_1)}\left(\frac{z_2z_3}{(z_1 + q)^2}\right) + \frac{u}{L(z_1)} \end{aligned} \quad (42)$$

where  $L(z_1) = L_1 + \frac{K_L}{q+z_1}$  with  $K_L = 0.01[H.m]$ ,  $q = 0.05[m]$ ,  $z_1 = \sigma \in \mathbb{R}_+$  is the vertical distance of the ball measured from the coil,  $z_2 = \dot{\sigma}$  is the velocity,  $z_3 = i$  is the electrical current and the control  $u$  is the voltage applied and the control objective is to bring the ball position to  $z_1 = 0.1[m]$ . Other model parameters are given in the Table 1.

**TABLE 1. Model parameters for magnetic-levitation system.**

Parameters	Symbols	Values
Winding Resistance	$R$	1 [ $\Omega$ ]
Winding Inductance	$L_1$	0.02[H]
Gravitational Acceleration	$g_c$	9.81[m/s <sup>2</sup> ]
Magnetic Force Constant	$k_M$	0.0005[mH]
Frictional Constant	$k_F$	0.01 [N/m/sec]
Ferromagnetic ball's mass	$m$	0.1 [kg]
Desired ball's position	$z_1$	0.1[m]

In order to convert system (42) into normal form following transformation is defined

$$x := \Theta(z) = \begin{bmatrix} \sigma(z) \\ \dot{\sigma}(z) \\ \ddot{\sigma}(z) \end{bmatrix} = \begin{bmatrix} z_1 \\ z_2 \\ -\frac{k_F}{m}z_2 + g_c - \frac{k_M}{2m}\left(\frac{z_3}{z_1 + q}\right)^2 \end{bmatrix} \quad (43)$$

where  $\sigma(z) := z_1$  is the output of system. It can be verified that  $\Theta(z)$  is a diffeomorphism in  $D := \{z_1 + q > 0 \text{ and } z_3 > 0\}$ . In the transformed co-ordinate system can be represented as

$$\begin{aligned} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= x_3 \\ \dot{x}_3 &= -\frac{k_F}{m}x_3 - \frac{k_M z_3}{mL(z_1)(z_1 + q)^2} \left[ -Rz_3 + \frac{L_1 z_2 z_3}{(z_1 + q)} + u \right] \end{aligned} \quad (44)$$

Now selecting control  $u$  as

$$u = Rz_3 - \frac{L_1 z_2 z_3}{(q + z_1)} + \frac{mL(z_1)(z_1 + q)^2}{k_M z_3} \left( v + \frac{k_F}{m}x_3 \right) \quad (45)$$

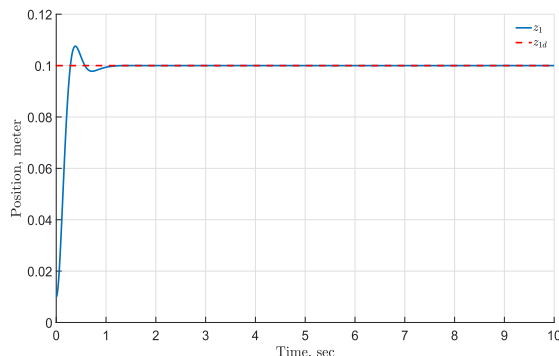
to obtain

$$\dot{x}_1 = x_2, \dot{x}_2 = x_3, \dot{x}_3 = v + d(t),$$

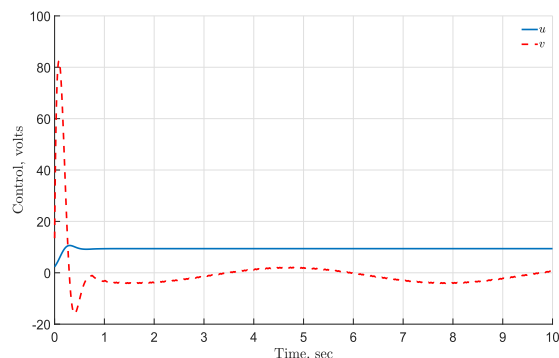
where  $d(t)$  is comes into picture due to uncertainties in gravity, systems parameters and external noise. For the current simulation we have considered  $d(t) = 0.5 + 0.1t + \sin(t)$  and controller  $v$  as

$$\begin{aligned} v := & -k_1(x_1 - 0.1) - k_2x_2 - k_3x_3 \\ & + \int_0^t -k_4\text{sign}(k_1(x_1 - 0.1) + k_2x_2 + k_3x_3)d\tau \end{aligned} \quad (46)$$

in order to track  $x_1 = z_1 := z_{1d} = 0.1$ , where  $k_1 = 2000$ ,  $k_2 = 400$ ,  $k_3 = 30$ , and  $k_4 = 10$ . In order to simulate the system (42), the initial conditions are chosen as  $Z_1 = 0.01$ ,  $z_2 = 0$ , and  $z_3 = 2.2$ . Tracking of position  $z_1 = 0.1$  is shown in the Fig. 3 using nonsmooth PI in the presence of disturbance  $d = 0.5 + 0.1t + \sin(t)$ . It is also confirmed from the simulation shown in Fig. 4, that the control is continuous.



**FIGURE 3. Evolution of position with respect to time.**



**FIGURE 4. Evolution of control with respect to time.**

**VII. CONCLUSION**

The stabilization of systems with nonsmooth PI controller under uncertainty is studied in this paper. The proposed method completely rejects the Lipschitz matched disturbances. The insensitivity to the disturbances is obtained by



incorporating the nonsmooth part in the controller. The stability of the proposed nonsmooth PI controller for an uncertain chain of an integrator is established for first order system via non-trivial strict Lyapunov function; then it is extended to an uncertain chain of an integrator. Finally, the performances of the controller are demonstrated using Matlab simulations of a magnetic suspension system.

## REFERENCES

- [1] H. K. Khalil, *Nonlinear System*. Upper Saddle River, NJ, USA: Prentice-Hall, 2002.
- [2] J. Alvarez-Ramirez, G. Fernandez, and R. Suarez, "A PI controller configuration for robust control of a class of nonlinear systems," *J. Franklin Inst.*, vol. 339, no. 1, pp. 29–41, Jan. 2002.
- [3] M.-T. Ho and C.-Y. Lin, "PID controller design for robust performance," *IEEE Trans. Autom. Control*, vol. 48, no. 8, pp. 1404–1409, Aug. 2003.
- [4] C. Zhao and L. Guo, "PID controller design for second order nonlinear uncertain systems," *Sci. China Inf. Sci.*, vol. 60, no. 2, pp. 1–13, Feb. 2017.
- [5] M. Krstic, "On the applicability of PID control to nonlinear second-order systems," *Nat. Sci. Rev.*, vol. 4, no. 5, p. 668, 2017.
- [6] V. Utkin, *Sliding Mode Control in Electro-Mechanical Systems* (Automation and Control Engineering), 2nd ed. Boca Raton, FL, USA: CRC Press, 2009.
- [7] A. Isidori, *Nonlinear Control Systems*. Berlin, Germany: Springer-Verlag, 1995.
- [8] A. Isidori, *Nonlinear Control Systems II*. London, U.K.: Springer-Verlag, 1999.
- [9] S. Kamal, A. Chalanga, J. A. Moreno, L. Fridman, and B. Bandyopadhyay, "Higher order super-twisting algorithm," in *Proc. 13th Int. Workshop Variable Struct. Syst.*, Nantes, France, Jun./Jul. 2014, pp. 1–5, doi: 10.1109/VSS.2014.6881129.
- [10] S. Kamal, A. Chalanga, V. Thorat, and B. Bandyopadhyay, "A new family of continuous higher order sliding mode algorithm," in *Proc. 10th Asian Control Conf. (ASCC)*, Kota Kinabalu, Malaysia, May/June. 2015, pp. 1–6, doi: 10.1109/ASCC.2015.7244591.
- [11] J. A. Moreno, "On strict Lyapunov functions for some non-homogeneous super-twisting algorithms," *J. Franklin Inst.*, vol. 351, no. 4, pp. 1902–1919, 2014.
- [12] R. E. Kalman, "Mathematical description of linear dynamical system," *J. SIAM Control*, vol. 1, no. 2, pp. 152–192, 1963.
- [13] A. Levant, "Sliding order and sliding accuracy in sliding mode control," *Int. J. Control*, vol. 58, no. 6, pp. 1247–1263, Dec. 1993.
- [14] A. Levant, "Higher-order sliding modes, differentiation and output-feedback control," *Int. J. Control*, vol. 76, nos. 9–10, pp. 924–941, Jan. 2003.
- [15] L. Fridman, "Sliding mode enforcement after 1990: Main results and some open problems," in *Sliding Modes After the First Decade of the 21st Century*. Berlin, Germany: Springer, 2012, pp. 3–57.
- [16] V. Utkin, "On convergence time and disturbance rejection of super-twisting control," *IEEE Trans. Autom. Control*, vol. 58, no. 8, pp. 2013–2017, Aug. 2013.
- [17] A. K. Pal, S. Kamal, S. K. Nagar, B. Bandyopadhyay, and L. Fridman, "Design of controllers with arbitrary convergence time," *Automatica*, vol. 112, Feb. 2020, Art. no. 108710, doi: 10.1016/j.automatica.2019.108710.
- [18] S. Kamal, P. Ramesh Kumar, A. Chalanga, J. K. Goyal, B. Bandyopadhyay, and L. Fridman, "A new class of uniform continuous higher-order sliding mode controllers," *J. Dyn. Syst., Meas., Control*, vol. 142, no. 1, Jan. 2020, Art. no. 011005, doi: 10.1115/1.4044952.
- [19] A. F. Filippov, *Differential Equations with Discontinuous Righthand Sides: Control Systems*. Dordrecht, The Netherlands: Kluwer, 1988.
- [20] S. P. Bhat and D. S. Bernstein, "Geometric homogeneity with applications to finite-time stability," *Math. Control, Signals, Syst.*, vol. 17, no. 2, pp. 101–127, Jun. 2005.
- [21] S. Kamal, A. Chalanga, M. K. Bera, and B. Bandyopadhyay, "State estimation and non vanishing unmatched disturbance reconstruction using modified super twisting algorithm," in *Proc. 7th Int. Conf. Electr. Comput. Eng.*, Dhaka, Bangladesh, Dec. 2012, pp. 941–944.
- [22] D. Luo, X. Xiong, S. Jin, and S. Kamal, "Adaptive gains of dual level to super-twisting algorithm for sliding mode design," *IET Control Theory Appl.*, vol. 12, no. 17, pp. 2347–2356, Nov. 2018, doi: 10.1049/iet-cta.2018.5380.
- [23] X. Xiong, S. Kamal, and S. Jin, "Adaptive gains to super-twisting technique for sliding mode design," *Asian J. Control*, early access, Aug. 2019, doi: 10.1002/asjc.2202.
- [24] J. J. E. Slotine and W. Li, *Applied Nonlinear Control*, vol. 199, no. 1. Englewood Cliffs, NJ, USA: Prentice-Hall, 1999.
- [25] A. Sachan, S. Kamal, D. Singh, and X. Xiong, "A robustness consideration in continuous time  $[\mathcal{K}, \mathcal{KL}]$  sector for nonlinear system," *IEEE Access*, vol. 7, pp. 30628–30636, 2019, doi: 10.1109/ACCESS.2019.2901806.
- [26] X. Xiong, R. Kikuuwe, S. Kamal, and S. Jin, "Implicit-euler implementation of super-twisting observer and twisting controller for second-order systems," *IEEE Trans. Circuits Syst. II, Exp. Briefs*, early access, Dec. 3, 2019, doi: 10.1109/TCSII.2019.2957271.



**SHARAT CHANDRA MAHTO** (Member, IEEE) received the bachelor's degree in electrical engineering from OUAT, Bhubaneswar, India, and the master's degree in control systems from the Indian Institute of Technology (BHU), Varanasi, India, in 2011, where he is currently pursuing the Ph.D. degree in control engineering with the Department of Electrical Engineering. His research interests include nonlinear control theory, event triggered control, and time-delay systems.



**DURGESH KUMAR** (Member, IEEE) is currently pursuing the Integrated Dual Degree (B.Tech. and M.Tech.) in electrical engineering with the Indian Institute of Technology (BHU), Varanasi, India. His research interests include nonlinear control theory, sliding mode control, and timedelay systems.



**SHYAM KAMAL** (Member, IEEE) received the bachelor's degree in electronics and communication engineering from Gurukula Kangri Vishwavidyalaya, Haridwar, India, in 2009, and the Ph.D. degree in systems and control engineering from the Indian Institute of Technology Bombay, India, in 2014. He is currently working as an Assistant Professor at the Department of Electrical Engineering, Indian Institute of Technology (BHU), Varanasi, India. He has published one monograph and more than 60 journal articles and conference papers. His research interests include fractional-order systems, contraction analysis, and discrete and continuous higher order sliding mode control.



**ASIF CHALANGA** received the bachelor's degree in electrical engineering from the University of Bhavnagar, India, in 2007, the M.Tech. degree in control systems from the College of Engineering Pune, India, in 2010, and the Ph.D. degree in systems and control engineering from the Indian Institute of Technology Bombay, India, in 2015. His research interests include the areas of discrete and continuous higher order sliding mode control and application aspects of the sliding mode to real time systems.



**XIAOGANG XIONG** (Member, IEEE) received the Ph.D. (Eng.) degree in mechanical and science engineering from Kyushu University, Fukuoka, Japan, in 2014. From 2014 to 2015, he was a Researcher with the Kyushu Institute of Technology, Izuka, Japan. From 2015 to 2016, he was a Research Fellow with the Singapore Institute of Manufacturing Technology, Singapore. He is currently an Assistant Professor at the Department of Mechanical Engineering and Automation, Harbin Institute of Technology (Shenzhen), Shenzhen, China. His research interests include human–robot coordination, nonsmooth systems, such as multibody dynamics and dc–dc converter, intelligent robots, and robot real-time control.



**SHANHAI JIN** (Member, IEEE) received the B.E. degree from the Changchun University of Technology, China, in 2005, the M.E. degree from Yanbian University, China, in 2008, and the Ph.D. degree from Kyushu University, Japan, in 2013. From 2013 to 2016, he was a Research Assistant Professor at Kyushu University, Japan. He is currently an Associate Professor at the School of Engineering, Yanbian University, China. His research interests include nonlinear filtering, sliding mode control, welfare assistive robotics, power converter, and image processing. He received the Advanced Robotics Best Paper Award from the Robotics Society of Japan, in 2013.



**SHYAM KRISHNA NAGAR** (Member, IEEE) was born in Varanasi, India, in May 1955. He received the B.Tech. and M.Tech. degrees in electrical engineering from the Indian Institute of Technology (IIT) (BHU), in 1976 and 1978, respectively, and the Ph.D. degree in electrical engineering from the University of Roorkee, Roorkee, India, under Quality Improvement Programme (QIP). He joined IIT (BHU), in 1980, as a Lecturer, and promoted to a Reader, in 1993. He joined IIT (BHU), in 2001, as a Professor of electrical engineering, and is continuing as a Professor at the Department of Electrical Engineering, IIT (BHU). His fields of interests include model reduction, digital control, and discrete event systems. He has supervised five Ph.D. theses in the area of model reduction and controller design. He has published 20 articles in regular journals and presented 40 papers in national and international conferences. He is a Life Member of System Society of India and a Fellow of Institution of Engineers. He was a National Advisory Committee Member of the National System Conference, in 2008 (NSC-2008), and a Technical Program Committee Member of the Student's Conference on Engineering and Systems (SCES-2014). He received the Best Paper Award at National System Conference (NSC-2011).

...