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\mathcal{H}_∞ Control of Networked Control System With Data Packet Dropout via Observer-Based Controller

YANFENG WANG¹, PING HE^{2,3,6}, HENG LI³, XIAOYUE SUN¹, HAORYANG MI⁴, WEI WEI⁵, (Senior Member, IEEE), XINGZHONG XIONG⁶, AND YANGMIN LI⁷, (Senior Member, IEEE)

¹School of Engineering, Huzhou University, Huzhou 313000, China

²School of Intelligent Systems Science and Engineering (Institute of Physical Internet), Jinan University, Zhuhai 519070, China

³Department of Building and Real Estate, The Hong Kong Polytechnic University, Hong Kong

⁴National Engineering Research Center for Advanced Polymer Processing Technology, Zhengzhou University, Zhengzhou 450000, China

⁵School of Computer Science and Engineering, Xi'an University of Technology, Xi'an 710048, China

⁶Artificial Intelligence Key Laboratory of Sichuan Province, Sichuan University of Science and Engineering, Yibin 644004, China

⁷Department of Industrial and Systems Engineering, The Hong Kong Polytechnic University, Hong Kong

Corresponding author: Ping He (pinghecn@qq.com)

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ABSTRACT The \mathcal{H}_∞ control problem for networked control system with data packet dropout in both S-C link and C-A link via observer-based controller is researched in this paper. Firstly, the networked control system with data packet dropout in both S-C link and C-A link is modeled as a discrete Markov jump linear system. Secondly, the sufficient and necessary conditions on the stochastic stability of the closed-loop system is established, the solution method of the controller and observer gain matrix are also given on condition that the transition probability matrix is completely known and partly unknown, respectively. The minimal disturbance suppression performance index is also obtained. Finally, two simulation examples illustrate the validity of the proposed method.

INDEX TERMS Markov jump system, data packet dropout, observer, stochastic stability, closed-loop system.

I. INTRODUCTION

The data packet dropout and time-delay are known to be two main causes to performance deteriorations or even instability of networked control system (NCS) [1]–[5]. The control problem of NCS with data packet dropout and time-delay has attracted considerable research interests in the past decades [6]–[9]. This paper is concerned with the impact of data packet dropout on the controller design of NCS.

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In the existing literatures, the method of dealing with the data packet dropout phenomenon can be divided into three types. The first type of method is to treat the data packet dropout as an event, and the NCS is modeled as an asynchronous dynamical system (see, e.g., [10]–[12]). The \mathcal{H}_∞ filtering for NCS with time-delay longer than one sampling period and data packet dropout was researched. The sufficient conditions on the exponential stability of the closed-loop system were established by use of the theory of asynchronous dynamical systems [10]. The stability of iterative learning control problem with data packet dropout was researched.

By use of the super vector formulation, an iterative learning control system with data packet dropout was modeled as an asynchronous dynamical system with constraints on event rate in the iteration domain [11]. A controller design method was proposed for a class of NCS with uncertain time-varying delay and data packet dropout. When the data packet dropout occurred, the predicted state was used to replace the current object state. Combined with the state predictor, the NCS with long time-delay and data packet dropout was modeled as an asynchronous dynamic system with event rate constraints [12].

The second type of method is to model the phenomenon of data packet dropout as a binary switching sequence taking values of zero or one which is specified by a Bernoulli probability distribution (see, e.g., [13]–[17]). For a class of NCS with random data packet dropout, a novel robust model predictive control method with active compensation mechanism was proposed. The probability distribution of data packet dropout was described as the Bernoulli distributed white sequences. The sufficient existing conditions on the controller were derived [13]. The problem of fault detection for a kind of fuzzy NCS with quantization and data packet dropout was researched. The probability of data packet dropout was governed by an individual random Bernoulli distribution. The residual system was stochastically stable with a given \mathcal{H}_∞ performance under the designed fault filter [14]. The problem of robust integral sliding mode control for NCS with multiple data packet dropout was researched. The data packet dropout occurred in both the link from sensor to controller (S-C) and the link from controller to actuator (C-A) which was modeled by independent Bernoulli distributed sequences. An integral sliding mode controller was designed such that the reachability of the specified sliding mode domain was achieved [15]. The problem of iterative learning control was investigated for stochastic linear systems with data packet dropout modeled by a Bernoulli random variable. Under stochastic noises and random data packet dropout, the input sequences were proved to converge to the desired input in an almost sure sense [16]. The data packet dropout in S-C link and C-A link was described by two random variables obeying the Bernoulli distribution, respectively. The sufficient conditions on the existence of the controller were established by constructing the appropriate Lyapunov-Krasovskii functional [17].

In real communication network, the data packet dropout at the current time instant is related to the data packet dropout at the previous time instant. However, the first and second methods cannot describe this relationship. The third type of method is to model the data packet dropout as a finite Markov chain which can be used to describe the dependency between the data packet dropout at the current time instant and the data packet dropout at the previous time instant (see, e.g., [18]–[20]). For the NCS with time-delay and the data packet dropout in S-C link, the closed-loop system was modeled as a Markov jump linear system (MJLS) with two running modes. The design method of the state feedback controller was also obtained without the consideration of time-delay and the data

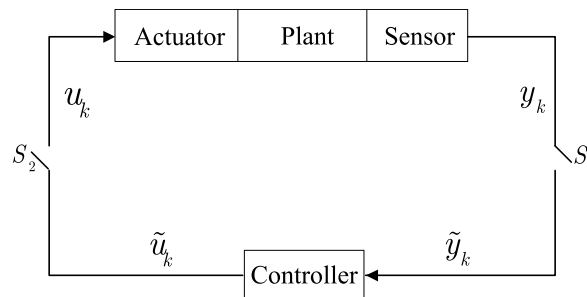


FIGURE 1. Structure of NCS with random data packet dropout.

packet dropout in C-A link [18]. The data packet dropout was model as a finite state Markov chain. Lyapunov-Krasovskii based approaches were applied to establish sufficient conditions on stochastic stability of closed-loop sampled-data bilateral teleportation system [19]. The robust model predictive tracking control problem for NCS with Markov data packet dropout was researched. By introducing a data packet dropout compensation strategy, the effects of data packet dropout on the system performance was considered [20].

Most existing literatures only considered Markov data packet dropout in S-C Link or C-A link. The \mathcal{H}_∞ control problem for NCS in the presence of data packet dropout in both S-C link and C-A link via observer-based controller needs to be further researched which motivates the current investigation. The main contributions of this paper can be presented as follows:

- 1) An observer is constructed for NCS with data packet dropout in S-C link and C-A link. Through the analysis of the system’s operating mode changing with the data packet dropout, the closed-loop system model is obtained.
- 2) The sufficient and necessary conditions on the stochastic stability for the closed-loop systems are established and the controller design method is derived on condition that the transition probability matrix is completely known and partly unknown, respectively.

The rest content of the paper is organized as follows. In Section II, the closed-loop system model is obtained through the analysis of the system’s operating mode change with the data packet dropout. In section III, stability analysis and controller design methods are given. In Section IV, two simulation examples are given to illustrate the effectiveness of the proposed controller. The conclusions are addressed in Section V.

II. PROBLEM FORMULATION

The structure of the NCS with random data packet dropout considered in this paper is shown in Figure 1, where the controlled plant is a linear system and the state equation of which is as follows:

$$\begin{cases} x_{k+1} = Ax_k + Bu_k + B_\omega\omega_k \\ y_k = Cx_k + D_\omega\omega_k \end{cases} \quad (1)$$

where x_k is the system state, u_k is the control input, ω_k is the external disturbance, y_k is the output; $A, B, B_\omega, C, D_\omega$ are known real constant matrices with appropriate dimensions.

The stochastic variable $\alpha_k(\beta_k)$ takes value from $\{0, 1\}$. When $\alpha_k(\beta_k) = 1$, it means that the switch $S_1(S_2)$ closes, and the data packet is transmitted successfully. When $\alpha_k(\beta_k) = 0$, it means that the switch $S_1(S_2)$ opens, and a data packet dropout occurs.

Construct the following observer at the controller side

$$\begin{cases} \hat{x}_{k+1} = A\hat{x}_k + B\tilde{u}_k + L(\tilde{y}_k - \alpha_k\hat{y}_k) \\ \hat{y}_k = C\hat{x}_k \end{cases} \quad (2)$$

where \hat{x}_k is the state of the observer, \hat{y}_k is the output of the observer, L is the observer gain matrix to be determined, \tilde{y}_k is the system output received by the observer and \tilde{u}_k is the control input of the observer which is expressed as

$$\tilde{u}_k = K\hat{x}_k \quad (3)$$

Due to the data packet dropout in S-C link, the system output obtained at the controller node at time instant k is as follows:

$$\tilde{y}_k = \alpha_k y_k \quad (4)$$

Because of the data packet dropout in C-A link, the control input acting on the controlled plant at time instant k is as follows:

$$u_k = \beta_k \tilde{u}_k \quad (5)$$

Define the following state estimation error and augmentation vector:

$$e_k = x_k - \hat{x}_k, \quad \zeta_k = [x_k^T \quad e_k^T]^T \quad (6)$$

The state equation of the closed-loop system can be obtained from equations (1)-(6):

$$\begin{cases} \zeta_{k+1} = \tilde{A}_{\alpha_k, \beta_k} \zeta_k + \tilde{B}_{\alpha_k, \beta_k} \omega_k \\ y_k = \tilde{C}_{\alpha_k, \beta_k} \zeta_k + D_\omega \omega_k \end{cases} \quad (7)$$

where

$$\begin{aligned} \tilde{A}_{\alpha_k, \beta_k} &= \begin{bmatrix} A + \beta_k BK & -\beta_k BK \\ (1 - \beta_k)BK & A + (1 - \beta_k)BK - \alpha_k LC \end{bmatrix}, \\ \tilde{B}_{\alpha_k, \beta_k} &= \begin{bmatrix} B_\omega \\ B_\omega - \alpha_k LD_\omega \end{bmatrix}, \quad \tilde{C}_{\alpha_k, \beta_k} = [I \quad 0]. \end{aligned}$$

The closed-loop system (7) consists of the following 4 subsystems:

- 1) When $\alpha_k = \beta_k = 0$, that is data packet dropout occur in both S-C link and C-A link, the model of system (7) is expressed as

$$\begin{cases} \zeta_{k+1} = \tilde{A}_{0,0} \zeta_k + \tilde{B}_{0,0} \omega_k \\ y_k = \tilde{C}_{0,0} \zeta_k + D_\omega \omega_k \end{cases} \quad (8)$$

where

$$\begin{aligned} \tilde{A}_{0,0} &= \bar{A} + M_1 K N_1, \quad \bar{A} = \begin{bmatrix} A & 0 \\ 0 & A \end{bmatrix}, \quad M_1 = \begin{bmatrix} 0 \\ B \end{bmatrix}, \\ N_1 &= [-I \quad I], \quad \tilde{B}_{0,0}^T = [B_\omega^T \quad B_\omega^T], \\ \tilde{C}_{0,0} &= [I \quad 0]. \end{aligned}$$

- 2) When $\alpha_k = 0, \beta_k = 1$, that is data packet dropout occur in S-C link, the model of system (7) is described as

$$\begin{cases} \zeta_{k+1} = \tilde{A}_{0,1} \zeta_k + \tilde{B}_{0,1} \omega_k \\ y_k = \tilde{C}_{0,1} \zeta_k + D_\omega \omega_k \end{cases} \quad (9)$$

where

$$\begin{aligned} \tilde{A}_{0,1} &= \bar{A} + M_2 K N_2, \quad M_2 = \begin{bmatrix} B \\ 0 \end{bmatrix}, \quad N_2 = [I \quad -I], \\ B_{0,1}^T &= [B_\omega^T \quad B_\omega^T], \quad \tilde{C}_{0,1} = [I \quad 0]. \end{aligned}$$

- 3) When $\alpha_k = 1, \beta_k = 0$, that is data packet dropout occur in C-A link, the model of system (7) is written as

$$\begin{cases} \zeta_{k+1} = \tilde{A}_{1,0} \zeta_k + \tilde{B}_{1,0} \omega_k \\ y_k = \tilde{C}_{1,0} \zeta_k + D_\omega \omega_k \end{cases} \quad (10)$$

where

$$\begin{aligned} \tilde{A}_{1,0} &= \bar{A} + M_3 K N_3 + E_3 L F_3, \quad M_3 = \begin{bmatrix} 0 \\ B \end{bmatrix}, \\ N_3 &= [-I \quad I], \quad E_3 = \begin{bmatrix} 0 \\ I \end{bmatrix}, \\ F_3 &= [0 \quad -C], \\ \tilde{B}_{1,0} &= \tilde{B}_{0,0} - E_3 L D_\omega, \quad \tilde{C}_{1,0} = [I \quad 0]. \end{aligned}$$

- 4) When $\alpha_k = 1, \beta_k = 1$, that is data packet dropout occur neither in S-C link nor in C-A link, the model of system (7) is as follows

$$\begin{cases} \zeta_{k+1} = \tilde{A}_{1,1} \zeta_k + \tilde{B}_{1,1} \omega_k \\ y_k = \tilde{C}_{1,1} \zeta_k + D_\omega \omega_k \end{cases} \quad (11)$$

where

$$\begin{aligned} \tilde{A}_{1,1} &= \bar{A} + M_4 K N_4 + E_4 L F_4, \quad M_4 = \begin{bmatrix} B \\ 0 \end{bmatrix}, \\ N_4 &= [-I \quad I], \quad E_4 = \begin{bmatrix} 0 \\ I \end{bmatrix}, \quad F_4 = [0 \quad -C], \\ \tilde{B}_{1,1} &= \tilde{B}_{0,0} - E_4 L D_\omega, \quad \tilde{C}_{1,1} = [I \quad 0]. \end{aligned}$$

As data packet dropout occurs, the closed-loop system (7) jumps among the 4 subsystems (8)-(11). Because the data packet dropout at the current time instant is related to the data packet dropout at the previous time instant, it is reasonable to model the closed-loop system (7) as a MJLS consisting 4 subsystems:

$$\begin{cases} \zeta_{k+1} = \tilde{A}_{r_k} \zeta_k + \tilde{B}_{r_k} \omega_k \\ y_k = \tilde{C}_{r_k} \zeta_k + D_\omega \omega_k \end{cases} \quad (12)$$

where $\{r_k, k \in Z\}$ is a discrete Markov chain which takes values in the set $\mathcal{M} = \{1, 2, 3, 4\}$, and $\tilde{A}_1 \triangleq \tilde{A}_{0,0}, \tilde{A}_2 \triangleq \tilde{A}_{0,1}, \tilde{A}_3 \triangleq \tilde{A}_{1,0}, \tilde{A}_4 \triangleq \tilde{A}_{1,1}, \tilde{B}_1 \triangleq \tilde{B}_{0,0}, \tilde{B}_2 \triangleq \tilde{B}_{0,1}, \tilde{B}_3 \triangleq \tilde{B}_{1,0}, \tilde{B}_4 \triangleq \tilde{B}_{1,1}, \tilde{C}_1 \triangleq \tilde{C}_{0,0}, \tilde{C}_2 \triangleq \tilde{C}_{0,1}, \tilde{C}_3 \triangleq \tilde{C}_{1,0}, \tilde{C}_4 \triangleq \tilde{C}_{1,1}$. The transition probability matrix of r_k is $\Pi = [\pi_{pq}]$, where π_{pq} is defined as $\pi_{pq} = \Pr\{r_{k+1} = q | r_k = p\}$, $\pi_{pq} \geq 0, \sum_{q=1}^4 \pi_{pq} = 1, p, q \in \mathcal{M}$.

It is necessary to introduce the notion of stochastic stability for the closed-loop system (12) before the main results are presented.

Definition 1 [21]: When $\omega_k = 0$, the closed-loop system (12) is said to be stochastically stable if for arbitrary initial mode $r_0 \in \mathcal{M}$ and initial state ζ_0 , there exists a positive-definite matrix $W > 0$ such that $E \left\{ \sum_{k=0}^{\infty} \|\zeta_k\|^2 | r_0, \zeta_0 \right\} < \zeta_0^T W \zeta_0$ holds.

Remark 1: Different from the traditional point to point control system, the control input of the observer \tilde{u}_k in (2) is different from the control input of the controlled plant u_k in (1), which brings difficulties in the controller design.

The objective of this paper is to design the observer (2) and the observer-based controller (3) for the controlled plant (1), such that, the closed-loop system (12) is stochastically stable in the presence of the random data packet dropout in both S-C link and C-A link and a certain \mathcal{H}_∞ performance is also achieved. Specifically, the closed-loop system (12) satisfies the following two requirements under the observer-based controller (3):

- 1) The closed-loop system (12) is stochastically stable.
- 2) Under the zero-initial condition, for all $\omega_k \neq 0$, the output y_k satisfies:

$$E \left\{ \sum_{k=0}^{\infty} \|y_k\|^2 \right\} < \gamma^2 E \left\{ \sum_{k=0}^{\infty} \|\omega_k\|^2 \right\} \quad (13)$$

where γ is the disturbance suppression performance index.

III. MAIN RESULTS

In this section, the sufficient and necessary conditions on the stochastic stability for the closed-loop systems (12) will be established and the controller design method will be derived on condition that the transition probability matrix Π is completely known and partly unknown, respectively.

Theorem 1: The closed-loop system (12) is stochastically stable, if and only if there exist positive-definite matrices $P_p > 0, P_q > 0$ and matrices K, L such that the following matrix inequality holds for all $p, q \in \mathcal{M}$. ■

$$\Theta = \tilde{A}_p^T \sum_{q \in \mathcal{M}} \pi_{pq} P_q \tilde{A}_p - P_p < 0 \quad (14)$$

Proof: Sufficiency: Define a Lyapunov function $V_k = \zeta_k^T P_{r_k} \zeta_k$, where $P_{r_k} > 0$.

From (12) with $\omega_k = 0$, one has:

$$\begin{aligned} E \{ \Delta V_k \} &= E \left\{ \zeta_k^T P_{r_k} \zeta_k | r_k = p \right\} - \zeta_k^T P_{r_k} \zeta_k \\ &= \zeta_k^T (\tilde{A}_{r_k}^T \sum_{q \in \mathcal{M}} \pi_{pq} P_{r_{k+1}} \tilde{A}_{r_k} - P_{r_k}) \zeta_k. \end{aligned}$$

Hence, if (14) holds, one has

$$\begin{aligned} E \{ \Delta V_k \} &\leq -\lambda_{\min}(-\Theta) \zeta_k^T \zeta_k \\ &= -\lambda_{\min}(-\Theta) \|\zeta_k\|^2. \end{aligned}$$

For any positive integer $N \geq 0$, the following holds:

$$\begin{aligned} E \left\{ \sum_{k=0}^N \|\zeta_k\|^2 \right\} &\leq \frac{1}{\lambda_{\min}(-\Theta)} (E \{V_0\} - E \{V_{N+1}\}) \\ &\leq \frac{1}{\lambda_{\min}(-\Theta)} E \{V_0\} \\ &= \frac{1}{\lambda_{\min}(-\Theta)} \zeta_0^T P_{r_0} \zeta_0. \end{aligned}$$

By Definition 1, the closed-loop systems (12) is stochastically stable.

Necessity: Assuming that the closed-loop system (12) is stochastically stable, one has

$$E \left\{ \sum_{k=0}^{\infty} \|\zeta_k\|^2 | r_0, \zeta_0 \right\} < \zeta_0^T W \zeta_0. \quad (15)$$

Consider the following function for $\zeta_k \neq 0$:

$$\zeta_k^T \tilde{P}_{r_k} \zeta_k \triangleq E \left\{ \sum_{t=k}^T \zeta_t^T Z_{r_t} \zeta_t | r_k, \zeta_k \right\}, \quad (16)$$

where $Z_{r_t} > 0$. From (15), it can be inferred that $\zeta_k^T \tilde{P}_{r_k} \zeta_k$ is bounded, and one has:

$$\begin{aligned} \zeta_k^T P_{r_k} \zeta_k &\triangleq \lim_{T \rightarrow \infty} \zeta_k^T \tilde{P}_{r_k} \zeta_k \\ &= \lim_{T \rightarrow \infty} E \left\{ \sum_{t=k}^T \zeta_t^T Z_{r_t} \zeta_t | r_k, \zeta_k \right\} \end{aligned}$$

Since (17) holds for any ζ_k , one has $P_{r_k} \triangleq \lim_{T \rightarrow \infty} \tilde{P}_{r_k}$. Because $Z_{r_t} > 0$, it can be obtained that $P_{r_k} > 0$ from (17). Moreover, one has:

$$\begin{aligned} E \left\{ \zeta_k^T \tilde{P}_{r_k} \zeta_k - \zeta_{k+1}^T \tilde{P}_{r_{k+1}} \zeta_{k+1} | r_k, \zeta_k \right\} \\ &= \zeta_k^T (\tilde{P}_p - \tilde{A}_p^T \sum_{q \in \mathcal{M}} \pi_{pq} \tilde{P}_q \tilde{A}_p) \zeta_k \\ &= \zeta_k^T Z_p \zeta_k \\ &> 0. \end{aligned}$$

Letting $T \rightarrow \infty$, one has $\Theta < 0$, and this completes the proof. □

Sufficient and necessary conditions on the existence of the observer-based controller are given in Theorem 1. Sufficient conditions such that not only the closed-loop system (12) is stochastically stable but also a certain \mathcal{H}_∞ performance is also achieved are exhibited in Theorem 2.

Theorem 2: If there exist positive-definite matrices $P_p > 0, Y_p > 0$ and matrices K, L such that

$$\begin{bmatrix} -Y_p & * & * & * \\ 0 & -\gamma^2 I & * & * \\ C_p & D_\omega & -I & * \\ \tilde{A}_p & \tilde{B}_p & 0 & -\tilde{P}_q \end{bmatrix} < 0 \quad (17)$$

$$Y_p P_p = I \quad (18)$$

where

$$\begin{aligned} \tilde{A}_p^T &= [\sqrt{\pi_{p1}}A_p, \dots, \sqrt{\pi_{p4}}A_p], \\ \tilde{B}_p^T &= [\sqrt{\pi_{p1}}B_p, \dots, \sqrt{\pi_{p4}}B_p], \\ \tilde{P}_q &= \text{Diag}\{P_1, \dots, P_4\}, \end{aligned}$$

hold for all $p, q \in \mathcal{M}$, the closed-loop system (12) is stochastically stable and \mathcal{H}_∞ performance (13) is also achieved. ■

Proof: For any $\omega_k \neq 0$, it follows from (12) that

$$\begin{aligned} &E\{\Delta V_k\} + y_k^T y_k - \gamma^2 \omega_k \\ &= x_k^T (\tilde{A}_p^T \sum_{q \in \mathcal{M}} \pi_{pq} P_q \tilde{A}_p + \tilde{C}_p^T \tilde{C}_p - P_p) x_k \\ &\quad + x_k^T (\tilde{A}_p^T \sum_{q \in \mathcal{M}} \pi_{pq} P_q \tilde{B}_p + \tilde{C}_p^T D_\omega) \omega_k \\ &\quad + \omega_k^T (\tilde{B}_p^T \sum_{q \in \mathcal{M}} \pi_{pq} P_q \tilde{A}_p + D_\omega^T \tilde{C}_p) x_k \\ &\quad + \omega_k^T (\tilde{B}_p^T \sum_{q \in \mathcal{M}} \pi_{pq} \tilde{B}_p + D_\omega^T D_\omega - \gamma^2 I) \omega_k \\ &= \zeta_k^T \Omega_p \zeta_k \end{aligned} \tag{19}$$

where

$$\begin{aligned} \Omega_p &= \begin{bmatrix} \Omega_{11} & * \\ \Omega_{21} & \Omega_{22} \end{bmatrix}, \\ \Omega_{11} &= \tilde{A}_p^T \sum_{q \in \mathcal{M}} \pi_{pq} P_q \tilde{A}_p + \tilde{C}_p^T \tilde{C}_p - P_p, \\ \Omega_{21} &= \tilde{B}_p^T \sum_{q \in \mathcal{M}} \pi_{pq} P_q \tilde{A}_p + D_\omega^T \tilde{C}_p, \\ \Omega_{22} &= \tilde{B}_p^T \sum_{q \in \mathcal{M}} \pi_{pq} \tilde{B}_p + D_\omega^T D_\omega - \gamma^2 I. \end{aligned}$$

Letting $Y_p = P_p^{-1}, p \in \mathcal{M}$, and by applying the Schur complement, $\Omega_{rk} < 0$ is equivalent to (17). Hence, it can be concluded from (17) and (19) that

$$E\{\Delta V_k\} + y_k^T y_k - \gamma^2 \omega_k < 0. \tag{20}$$

Summing up (20) from 0 to ∞ with respect to k yields

$$E\left\{\sum_{k=0}^{\infty} \|y_k\|^2\right\} < \gamma^2 E\left\{\sum_{k=0}^{\infty} \|\omega_k\|^2\right\} - E\{V_0\} - E\{V_\infty\}.$$

Since the closed-loop system (12) is stochastically stable with the zero-initial condition, (13) can be readily obtained, which completes the proof. □

The conditions presented in Theorem 2 are a set of LMIs with some matrices inverse constraints which can be solved by the cone complementary linearization (CCL) algorithm. The problem of solving the controller gain matrix K and the observer gain matrix L can be transformed into the following nonlinear minimization problem:

$$\text{Min tr}\left(\sum_{p=1}^4 P_p Y_p\right) \quad \text{s.t. (17) and (21).}$$

$$\begin{bmatrix} P_p & I \\ I & Y_p \end{bmatrix} > 0, \quad p \in \mathcal{M}. \tag{21}$$

The procedure for solving K , the observer gain matrix L and the minimal disturbance suppression performance index γ_{\min} is given in Algorithm 1 where τ is a proper positive scalar.

The controller and observer gain matrix K and L are derived in Theorem 2 on condition that all probabilities in Π are all available. However, it is usually difficult to obtain the all transition probabilities. It is necessary to design the controller without the information of all transition probabilities. Thus, the transition probabilities of the jumping process of r_k are considered to be partly unavailable in Theorem 3, i.e., some elements in matrix Π are unknown. For example, the transition probabilities matrix Π may be as follows

$$\Pi = \begin{bmatrix} ? & \pi_{12} & \pi_{13} & ? \\ \pi_{21} & \pi_{22} & ? & ? \\ ? & ? & ? & \pi_{34} \\ \pi_{41} & \pi_{42} & \pi_{43} & \pi_{44} \end{bmatrix}$$

where “?” represents the unknown elements. For notational clarity, the set \mathcal{M} can be denoted as $\mathcal{M} = \mathcal{M}_k^p + \mathcal{M}_{uk}^p$ with $\mathcal{M}_k^p = \{q : \pi_{pq} \text{ is known}\}$, $\mathcal{M}_{uk}^p = \{q : \pi_{pq} \text{ is unknown}\}$. Moreover, if $\mathcal{M}_k^p \neq \emptyset$, it can be further described as $\mathcal{M}_k^p = \{k_1^p, k_2^p, \dots, k_d^p\}$, $1 \leq d \leq 4$, where k_d^p represents the column subscript of the d th known element in the p th row of the matrix Π . \mathcal{M}_{uk}^p is described as $\mathcal{M}_{uk}^p = \{\bar{k}_1^p, \bar{k}_2^p, \dots, \bar{k}_{4-d}^p\}$, where \bar{k}_{4-d}^p represents column subscript of the $(4-d)$ th unknown element in the p th row of the matrix Π .

Theorem 3: The closed-loop system (12) is stochastically stable and \mathcal{H}_∞ performance (13) is also achieved, if there exist positive-definite matrices $P_p > 0, Y_p > 0$ and matrices K, L such that

$$\begin{bmatrix} -\tilde{\pi} Y_p & * & * & * \\ 0 & -\tilde{\pi} \gamma^2 I & * & * \\ \tilde{\pi} \tilde{C}_p & \tilde{\pi} D_\omega & -\tilde{\pi} I & * \\ \tilde{A}_p & \tilde{B}_p & 0 & -\tilde{P}_q \end{bmatrix} < 0 \tag{22}$$

$$\begin{bmatrix} -Y_p & * & * & * \\ 0 & -\gamma^2 I & * & * \\ C_p & D_\omega & -I & * \\ A_p & B_p & 0 & -P_q \end{bmatrix} < 0, \quad q \in \mathcal{M}_{uk}^p \tag{23}$$

$$Y_p P_p = I \tag{24}$$

where

$$\begin{aligned} \tilde{A}_p &= [\sqrt{\pi_{p1}}A_p, \dots, \sqrt{\pi_{pd}}A_p], \\ \tilde{B}_p &= [\sqrt{\pi_{p1}}B_p, \dots, \sqrt{\pi_{pd}}B_p], \\ \tilde{P}_q &= \text{Diag}\{P_1, \dots, P_d\}, \\ \tilde{\pi} &= \sum_{q \in \mathcal{M}_k^p} \pi_{pq}, \end{aligned}$$

hold for all $p, q \in \mathcal{M}$. ■

Algorithm 1 Procedure for Solving K, L and γ_{\min}

- 1: Set the maximal number of iterations R_{\max} and the disturbance suppression performance index $\gamma = \gamma_0$
- 2: Find a set of feasible solution (P_p^0, Y_p^0, K^0, L^0) satisfying (17) and (21), and let $k = 0$
- 3: Solve the following optimization problem for variables:

$$\text{Min tr} \left(\sum_{p=1}^4 (P_p^k Y_p + Y_p^k P_p) \right)$$
 s.t. (17) and (21)
- 4: Set $P_p^k = P_p, Y_p^k = Y_p, K^k = K, L^k = L$
- 5: **while** number of iterations $< R_{\max}$ **do**
- 6: **if** (17), (18) is satisfied **then**
- 7: $\gamma = \gamma - \tau, k = k + 1$, go to step 3
- 8: **else**
- 9: $k = k + 1$, go to step 3
- 10: **end if**
- 11: **end while**
- 12: **if** $\gamma < \gamma_0$ **then**
- 13: $\gamma_{\min} = \gamma + \tau$
- 14: **else**
- 15: this optimization problem has no solution within the given number of iterations R_{\max}
- 16: **end if**

Proof: It is noticed that $\sum_{q \in \mathcal{M}} \pi_{pq} = 1$, by the Schur complement, $\Omega_{r_k} < 0$ is equivalent to

$$\begin{aligned} & \begin{bmatrix} -Y_p & * & * \\ 0 & -\gamma^2 I & * \\ C_p & D_\omega & -I \end{bmatrix} + [A_p \quad B_p \quad 0]^T \\ & \times \sum_{q \in \mathcal{M}} \pi_{pq} P_{r_{k+1}} [A_p \quad B_p \quad 0] \\ & = \sum_{q \in \mathcal{M}_k^p} \pi_{pq} \begin{bmatrix} -Y_p & * & * \\ 0 & -\gamma^2 I & * \\ C_p & D_\omega & -I \end{bmatrix} + [A_p \quad B_p \quad 0]^T \\ & \times \sum_{q \in \mathcal{M}_k^p} \pi_{pq} P_{r_{k+1}} [A_p \quad B_p \quad 0] \\ & + \sum_{q \in \mathcal{M}_{uk}^p} \pi_{pq} \begin{bmatrix} -Y_p & * & * \\ 0 & -\gamma^2 I & * \\ C_p & D_\omega & -I \end{bmatrix} + [A_p \quad B_p \quad 0]^T \\ & \times \sum_{q \in \mathcal{M}_{uk}^p} \pi_{pq} P_{r_{k+1}} [A_p \quad B_p \quad 0] \\ & = \begin{bmatrix} -\tilde{\pi} Y_p & * & * \\ 0 & -\tilde{\pi} \gamma^2 I & * \\ \tilde{\pi} C_p & \tilde{\pi} D_\omega & -\tilde{\pi} I \end{bmatrix} + [A_p \quad B_p \quad 0]^T \\ & \times \sum_{q \in \mathcal{M}_k^p} \pi_{pq} P_{r_{k+1}} [A_p \quad B_p \quad 0] \\ & + \sum_{q \in \mathcal{M}_{uk}^p} \pi_{pq} \left(\begin{bmatrix} -Y_p & * & * \\ 0 & -\gamma^2 I & * \\ C_p & D_\omega & -I \end{bmatrix} + [A_p \quad B_p \quad 0]^T \right. \\ & \left. \times P_{r_{k+1}} [A_p \quad B_p \quad 0] \right) \\ & < 0. \end{aligned}$$

Applying Schur complement again, it can be concluded that $\Omega_{r_k} < 0$ if (22)-(24) holds. This ends the proof. \square

Remark 2: Similar to Algorithm 1, (22)-(24) in Theorem 3 can also be solved by the CCL algorithm. The detail algorithm is thus omitted.

Remark 3: Regarding the unknown probabilities, the method adopted in this paper is to separate the known probabilities from the unknown ones, and then discard the unknown ones. Another method is to separate the probabilities from the correlation matrices ([21], [22]), for example, $\sum_{q \in \mathcal{M}} \pi_{pq} P_q \leq \sum_{q \in \mathcal{M}} \pi_{pq} \sum_{q \in \mathcal{M}} P_q$ which greatly increases the conservatism of the results.

Remark 4: For the method of separating the known probabilities from the unknown ones, as the number of unknown probabilities increases, the number of matrix inequalities to be satisfied will increase. In Theorem 3, if all transition probabilities are known, the number of matrix inequalities to be satisfied is four; When all transition probabilities are unknown, the number of matrix inequalities to be satisfied is sixteen.

IV. NUMERICAL EXAMPLES

In this section, two examples are provided to demonstrate the effectiveness of the proposed method.

Example 1: Consider the angular positioning system in Figure 2, which consists of a rotating antenna at the origin of the plane driven by a motor, where φ is the angular position of the antenna, and φ_r is the angular position of the moving object [23]. The function of the system is to rotate the antenna to point the direction of the moving object by adjusting the input voltage of the motor.

The state variables of the system are chosen as $[\varphi \quad \dot{\varphi}]^T$, then the parameter of the angular positioning system are as

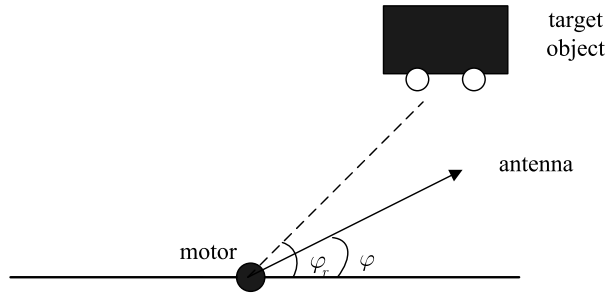


FIGURE 2. The angular positioning system.

follows:

$$A = \begin{bmatrix} 1 & 0.0995 \\ 0 & 0.99 \end{bmatrix}, \quad B = \begin{bmatrix} 0.0039 \\ 0.0783 \end{bmatrix}, \quad B_\omega = \begin{bmatrix} 0.005 \\ 0.003 \end{bmatrix},$$

$$C = \begin{bmatrix} 1.4 & 0.8 \\ -0.2 & 0.4 \end{bmatrix}, \quad D_\omega = \begin{bmatrix} 0.007 \\ 0.009 \end{bmatrix}.$$

The relevant parameters of the resulting closed-loop system (12) can be calculated as follows:

$$M_1^T = M_3^T = \begin{bmatrix} 0 & 0 & 0.0039 & 0.0783 \end{bmatrix},$$

$$M_2^T = M_4^T = \begin{bmatrix} 0.0039 & 0.0783 & 0 & 0 \end{bmatrix},$$

$$N_1 = N_3 = \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 1 & 0 & -1 \end{bmatrix},$$

$$N_2 = N_4 = \begin{bmatrix} -1 & 0 & 1 & 0 \\ 0 & -1 & 0 & 1 \end{bmatrix},$$

$$E_3^T = E_4^T = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

$$F_3^T = F_4^T = \begin{bmatrix} 0 & 0 & -1.5 & 0.7 \\ 0 & 0 & -0.2 & 0.4 \end{bmatrix}.$$

The close-loop system mode $r_k \in \{1, 2, 3, 4\}$, the transition probability matrix of which is as follows:

$$\Pi = \begin{bmatrix} 0.3 & 0.4 & 0.1 & 0.2 \\ 0.1 & 0.5 & 0.3 & 0.1 \\ 0.5 & 0.1 & 0.2 & 0.2 \\ 0.4 & 0.3 & 0.2 & 0.1 \end{bmatrix}.$$

By use of Theorem 2, the controller gain matrix K , the observer L and the minimal disturbance suppression performance index γ_{\min} are obtained as follows:

$$K = \begin{bmatrix} -4.0078 & -5.2012 \end{bmatrix},$$

$$L = \begin{bmatrix} 0.5670 & 0.4922 \\ 0.4005 & 1.6271 \end{bmatrix}, \quad \gamma_{\min} = 0.1703.$$

The initial states are assumed to be $x_0^T = [2 \ -1]$, $\hat{x}_0^T = [2.1 \ -1.1]$ and the disturbance input is $\omega_k = 1/k$. Figure 3 - Figure 5 show the system mode and the states curve of the closed-loop system.

Example 2: Consider the controlled the plant of which the parameters are given as follows:

$$A = \begin{bmatrix} 0.52 & -0.69 \\ 0 & 0.19 \end{bmatrix}, \quad B_u = \begin{bmatrix} 0.3 \\ 0.2 \end{bmatrix}, \quad B_\omega = \begin{bmatrix} 0.01 \\ 0.23 \end{bmatrix},$$

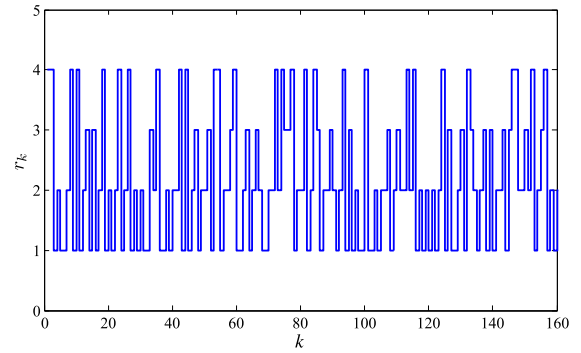


FIGURE 3. The mode of the angular positioning system σ_k .

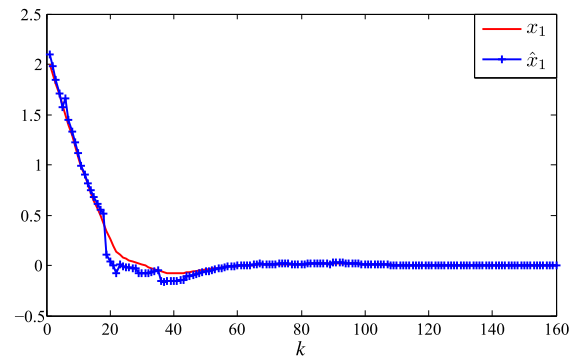


FIGURE 4. x_1 and its estimated value \hat{x}_1 of the angular positioning system.

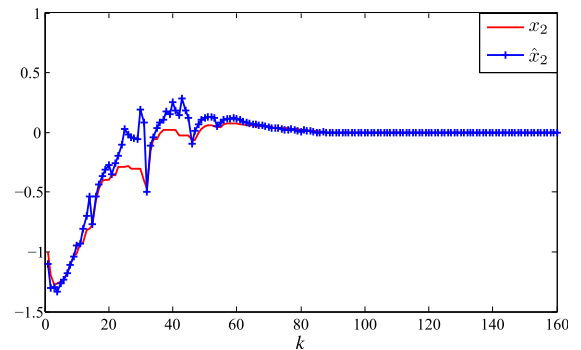


FIGURE 5. x_2 and its estimated value \hat{x}_2 of the angular positioning system.

$$C = \begin{bmatrix} 1.5 & 0.7 \\ 0.2 & 0.4 \end{bmatrix}, \quad D_\omega = \begin{bmatrix} 0.03 \\ 0.05 \end{bmatrix}.$$

The transition probability matrix of close-loop system mode r_k is as follows:

$$\Lambda = \begin{bmatrix} 0.3 & ? & ? & 0.2 \\ 0.1 & ? & 0.5 & ? \\ 0.5 & 0.1 & ? & ? \\ 0.4 & 0.3 & 0.2 & 0.1 \end{bmatrix}.$$

By use of Theorem 3, the controller gain matrix K , the observer L and the minimal disturbance suppression performance index γ_{\min} are obtained as follows:

$$K = \begin{bmatrix} -0.1866 & -0.5995 \end{bmatrix},$$

$$L = \begin{bmatrix} 0.694 & -2.6930 \\ -0.0559 & 0.2138 \end{bmatrix}, \quad \gamma_{\min} = 0.0837.$$

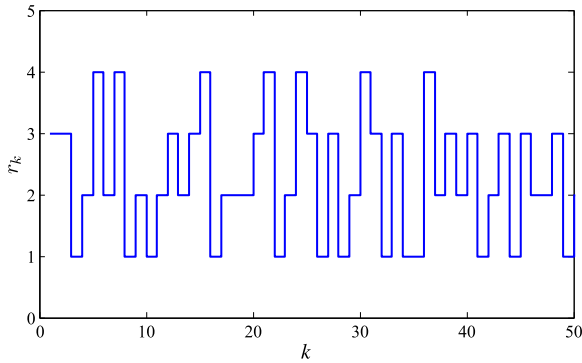


FIGURE 6. The system mode σ_k .

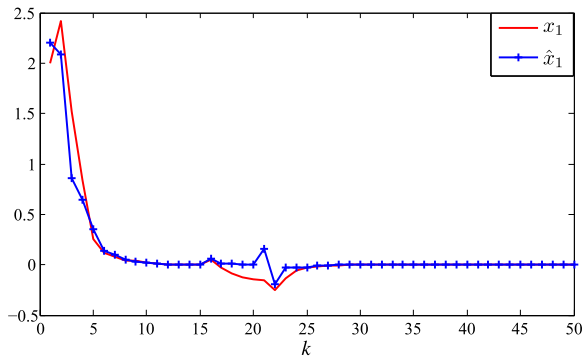


FIGURE 7. The state x_1 and its estimated value \hat{x}_1 .

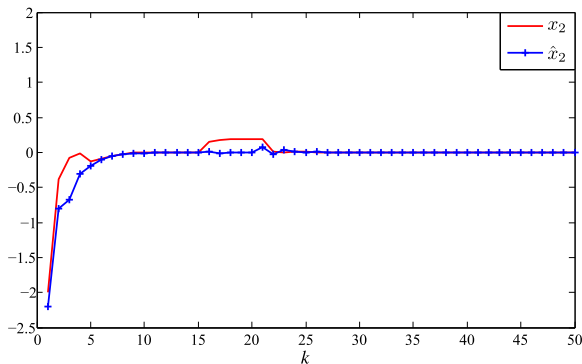


FIGURE 8. The state x_2 and its estimated value \hat{x}_2 .

The initial values of the system are assumed to be $x_0^T = [2 \ -2]$, $\hat{x}_0^T = [2.2 \ -2.2]$ and the disturbance input is

$$\omega_k = \begin{cases} 1, & k \in [15 \ 20] \\ 0, & \text{otherwise} \end{cases}$$

Figure 6 - Figure 8 show the system mode and the states curve of the closed-loop system.

By the method in [21] and [22], the controller gain matrix K , the observer L and the minimal disturbance suppression performance index γ_{\min} are obtained as follows:

$$K = \begin{bmatrix} -1.3822 & 1.3110 \end{bmatrix},$$

$$L = \begin{bmatrix} 0.1759 & -0.9068 \\ -0.0152 & 0.8021 \end{bmatrix},$$

$$\gamma_{\min} = 0.0775.$$

Obviously, the minimal disturbance suppression performance index γ_{\min} obtained by the proposed method is smaller than that in [21] and [22].

V. CONCLUSION

An observer-based \mathcal{H}_∞ control problem for networked control system with random data packet dropout has been investigated. Both the data packet dropout in S-C link and the data packet dropout in C-A link are taken into consideration. The sufficient conditions on the existence of the observer-based controller have been derived such that the closed-loop system is stochastically stable and achieves certain \mathcal{H}_∞ disturbance rejection level. Simulation results have demonstrated the feasibility of the proposed method.

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YANFENG WANG was born in Liaocheng, China, in 1980. He received the M.S. degree in operations research and cybernetics, and the Ph.D. degree in control theory and control engineering from Northeastern University, in 2007 and 2013, respectively.

He is currently an Associate Professor with the School of Engineering, Huzhou University, Huzhou, Zhejiang, China. He has been supported by the National Natural Science Funds of China and the Natural Science Funds of Zhejiang Province. He has authored three books and more than 30 articles. His main research areas are networked control systems, fault detection, and fault-tolerant control.



PING HE was born in Huilongya, Nanchong, China, in November 1990. He received the B.S. degree in automation from the Sichuan University of Science and Engineering, Zigong, Sichuan, China, in June 2012, the M.S. degree in control science and engineering from Northeastern University, Shenyang, Liaoning, China, in July 2014, and the Ph.D. degree in electromechanical engineering from the Universidade de Macau, Taipa, Macau, in June 2017.

From December 2015 to November 2018, he was an Adjunct Associate Professor with the Department of Automation, Sichuan University of Science and Engineering. From August 2017 to August 2019, he was a Postdoctoral Research Fellow with the Emerging Technologies Institute, The University of Hong Kong, and Smart Construction Laboratory, The Hong Kong Polytechnic University. Since December 2018, he has been a Professor with the School of Intelligent Systems Science and Engineering, Jinan University, Zhuhai, Guangdong, China. He has authored one book and more than 40 articles. His research interests include sensor networks, complex networks, multiagent systems, artificial intelligence, control theory, and control engineering. He is the Reviewer Member for *Mathematical Reviews* of the American Mathematical Society. He also serves as a Section Editor of *Automatika: Journal for Control, Measurement, Electronics, Computing, and Communications*, an Academic Editor of *PLOS ONE*, and an Associate Editor of the *Proceedings of the Institution of Mechanical Engineers, Part E: Journal of Process Mechanical Engineering* and *IET The Journal of Engineering*.

Dr. Ping was a recipient of the Liaoning Province of China Master's Thesis Award for Excellence, in March 2015, and the IEEE Robotics and Automation Society Finalist of Best Paper Award, in July 2018.



HENG LI was born in Hunan, China, in 1963. He received the B.S. and M.S. degrees in civil engineering from Tongji University, in 1984 and 1987, respectively, and the Ph.D. degree in architectural science from The University of Sydney, Australia, in 1993.

From 1993 to 1995, he was a Lecturer with James Cook University. From 1996 to 1997, he was a Senior Lecture with the Civil Engineering Department, Monash University. Since 1997, he was gradually promoted from Associate Professor to a Chair Professor of construction informatics with The Hong Kong Polytechnic University. He has authored two books and more than 500 articles. His research interests include building information modeling, robotics, functional materials, and the Internet of Things.

Dr. Li was a recipient of the National Award from Chinese Ministry of Education, in 2015, and the Gold Prize of Geneva Innovation, in 2019. He is also a Reviews Editor of *Automation in Construction*.



XIAOYUE SUN was born in Jiaxing, China, in 1996. She received the B.S. degree in engineering from Huzhou University, Huzhou, China, in June 2019, where she is currently pursuing the M.S. degree.

Her research interests include networked control system fault detection and fault tolerant control.



HAOYANG MI received the bachelor's and Ph.D. degrees from the College of Mechanical and Automotive, South China University of Technology, Guangzhou, China, in 2010 and 2015, respectively. He was a Postdoctoral Researcher with the University of Wisconsin–Madison, USA, from 2016 to 2018, and a Research Fellow with The Hong Kong Polytechnic University, from 2018 to 2019.

He is currently an Associate Professor with the National Engineering Research Center for Advanced Polymer Processing Technology, Zhengzhou University. He has published nearly 100 SCI journal publications so far, with a total citation more than 2000 and an H-index of 27. He has applied 17 U.S. and China patents, and composed a book chapter. His current research focuses on intelligent materials, artificial intelligence, detection technology, automation device, and flexible sensors.

Dr. Mi also directs several projects on artificial intelligence and flexible sensors, and serves as a Regular Reviewer for many journals.



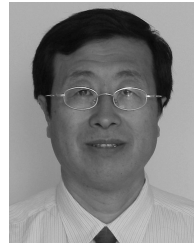
WEI WEI (Senior Member, IEEE) received the M.S. and Ph.D. degrees from Xi'an Jiaotong University, Xi'an, China, in 2005 and 2011, respectively. He is currently an Associate Professor with the School of Computer Science and Engineering, Xi'an University of Technology, Xi'an. He ran many funded research projects as a Principal Investigator and a Technical Member. He has published around 100 research articles in international conferences and journals. His current research

interests include the area of wireless networks, wireless sensor networks, image processing, mobile computing, distributed computing, and pervasive computing, the Internet of Things, and sensor data clouds. He is a Senior Member of the China Computer Federation (CCF). He is an Editorial Board Member of *Future Generation Computer System*, *IEEE ACCESS*, *Ad Hoc & Sensor Wireless Sensor Network*, *Journal of Institute of Electronics, Information and Communication Engineers*, and *KSH Transactions on Internet and Information Systems*. He is a TPC member of many conferences and a Regular Reviewer of the *IEEE TRANSACTIONS ON PARALLEL AND DISTRIBUTED SYSTEMS*, the *IEEE TRANSACTIONS ON IMAGE PROCESSING*, the *IEEE TRANSACTIONS ON MOBILE COMPUTING*, the *IEEE TRANSACTIONS ON WIRELESS COMMUNICATIONS*, the *Journal of Network and Computer Applications*, and so on.



XINGZHONG XIONG received the B.S. degree in communication engineering from the Sichuan University of Science and Engineering, Zigong, China, in 1996, and the M.S. and Ph.D. degrees in communication and information system from the University of Electronic Science and Technology of China (UESTC), in 2006 and 2009, respectively. In 2012, he completed a research assignment from the Postdoctoral Station of Electronic Science and Technology, UESTC. He is currently a Professor

with the School of Automation and Information Engineering, Sichuan University of Science and Engineering. His research interests include wireless and mobile communications technologies, intelligent signal processing, the Internet-of-Things technologies, and very large-scale integration (VLSI) designs.



YANGMIN LI (Senior Member, IEEE) received the B.S. and M.S. degrees in mechanical engineering from Jilin University, Changchun, China, in 1985 and 1988, respectively, and the Ph.D. degree in mechanical engineering from Tianjin University, Tianjin, China, in 1994.

He started his academic career, in 1994, as a Lecturer of the Mechatronics Department, South China University of Technology, Guangzhou, China. He was a Fellow of International Institute for Software Technology, United Nations University (UNU/IIST), from May to November 1996, a Visiting Scholar with the University of Cincinnati, in 1996, and a Postdoctoral Research Associate with Purdue University, West Lafayette, USA, in 1997. He was an Assistant Professor in 1997, an Associate Professor in 2001, and a Full Professor from 2007 to 2016 with the University of Macau. He is currently a Full Professor with the Department of Industrial and Systems Engineering, The Hong Kong Polytechnic University, Hong Kong. He has authored and coauthored more than 400 scientific articles in journals and conferences. His research interests include micro/nanomanipulation, compliant mechanism, precision engineering, robotics, and multibody dynamics and control.

Dr. Li is an Associate Editor of the *IEEE TRANSACTIONS ON AUTOMATION SCIENCE AND ENGINEERING*, *Mechatronics*, *IEEE ACCESS*, and the *International Journal of Control, Automation, and Systems*.

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