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# Improvements in the Explicit Estimation of Pollutant Dispersion Coefficient in Rivers by Subset Selection of Maximum Dissimilarity Hybridized With ANFIS-Firefly Algorithm (FFA)

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**ABSTRACT** In this paper, a new hybrid model is proposed using Subset Selection by Maximum Dissimilarity (SSMD) and adaptive neuro-fuzzy inference system (ANFIS) hybridized with the firefly algorithm (FFA) to predict the longitudinal dispersion coefficient ( $K_x$ ). The proposed framework (ANFIS-FFA), combines the specific structures and strengths of both ANFIS and FFA approaches. The FFA is used to derive the optimum ANFIS parameters. The  $K_x$  data set includes 503 cross-sectional data point from small to large rivers. For pre-processing of the data set, the SSMD method is used, which is superior to the classical trial and error method. The database covers a wide range of river width (0.2-867m), and depths (0.034-19.9 m). Fifteen different combinations of river width (B), depth (H), flow velocity (U) and shear velocity  $(U_*)$  are implemented as inputs to create fifteen estimative models. The output of the ANFIS-FFA model is compared with the ANFIS and previously published equations to check the performance of the proposed model. The results show that the highest accuracy is attained by the M1 model, with all geometric and hydrodynamic parameters as input variables in comparison with ANFIS and previous equations. The R<sup>2</sup> value, RMSE, MAE and NSE for ANFIS-FFA model are 0.67, 113.14 m<sup>2</sup>/s, 48 m<sup>2</sup>/s, and 0.63 for proposed dimensional model, and 0.35, 874.5, 520.8, and 0.1 in non-dimensional ANFIS-FFA model, respectively. These values were 0.37, 463.34 m<sup>2</sup>/s, 85.69 m<sup>2</sup>/s, and -5.19 for dimensional ANFIS model, and 0.11, 3269.88, 1932.09 and -11.54 for non-dimensional ANFIS model, respectively. Overall, hybridization caused 81%, 75%, 76% improvement in  $\mathbb{R}^2$ , RMSE and MAE. In another contribution of the paper, by using the matrix form of developed ANFIS-FFA optimized parameters, a novel explicit calculation procedure for estimation of  $K_x$  is derived. Based on the results, the proposed ANFIS-FFA model exhibits significant improvements than the classical ANFIS and highlights that optimizing by nature-inspired optimization algorithms plays a critical role in strengthening the ANFIS estimations generality.

**INDEX TERMS** Longitudinal dispersion coefficient, ANFIS-FFA, maximum dissimilarity method, natural rivers, adaptive neuro-fuzzy inference system.

## I. INTRODUCTION

Water is a necessary element in the world, for human life and survival. Most rivers are polluted nowadays, and these pollutants are transported in the river flow. River flow and

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pollutant transport studies are necessary for several applications such as analysis of water intake, sediment deposition, contamination control, and pollutant risk assessment [1]–[4]. The fundamental law of mass diffusion in water was first introduced by Fick (1855) [5] as  $q = -D\frac{\partial c}{\partial x}$ , where *q* is the mass flux of pollutant, *D* is the diffusion coefficient, and  $\frac{\partial c}{\partial x}$  is the gradient of the mass concentration (*c*) in x distance along the longitudinal direction [6], [7]. The diffusion coefficient is generally referred to the longitudinal dispersion coefficient [6], [8]. The injected pollutants are dispersed by advection and dispersion processes in longitudinal, vertical, and transverse directions [9], [10]. The longitudinal dispersion process becomes the main mechanism, when the mixing process in the lateral direction is fully developed [11], [12]. The longitudinal dispersion coefficient was first presented by Taylor [13], [14] as a measure of the one-dimensional dispersion process by the conventional advection-dispersion equation:

$$\frac{\partial C}{\partial t} + u \frac{\partial C}{\partial x} = K_x \frac{\partial^2 C}{\partial^2 x} \tag{1}$$

where *C* is the average of mass concentration in crosssection, *t* is the time, *u* is the velocity, *x* is the longitudinal coordinate, and  $K_x$  is longitudinal dispersion coefficient [15]. Fischer (1967) [16] developed the following integral expression [17] for  $K_x$  in rivers:

$$K_x = -\frac{1}{A} \int_0^B hu' \int_0^y \frac{1}{\varepsilon_t h} \int_0^y hu' dy \, dy \, dy \tag{2}$$

where A is the area of river cross-section, B is the river width, h is the flow depth, u' is the differences of the depth-averaged flow velocity at specified local y from average velocity over the cross-section of river, y is the location in the lateral direction, and  $\varepsilon_t$  is the local transverse mixing coefficient [9].

Longitudinal dispersion coefficient ( $K_x$ ) has a significant effect on contaminants and mass transport in large rives [18]. Consequently, estimation of the longitudinal dispersion coefficient could be useful in the management of water quality in rivers and optimal pollution control strategies [19], [20]. Seo and Cheong [11] stated that the  $K_x$  is affected by three groups of factors, including hydraulic river features, vegetation, fluid properties and geometric patterns of river reach [21], [22]. The longitudinal dispersion coefficient measurements showed that the most effective parameters are channel width (B), flow depth (H), bed shear velocity ( $U^*$ ) and cross-sectional average flow velocity (U) [23].  $K_x$  can be expressed as the following functional expression:

$$K_x = f(H, B, U, U^*) \tag{3}$$

Several researchers tried to develop empirical and mathematical equations for calculating  $K_x$  based on Equation 2. The first researchers who investigated the theoretical method for estimation of  $K_x$  were Taylor [13], [14] and Fischer [16]. Also, Elder [24] studied the  $K_x$  in non-uniform flow and proposed the empirical equations. McQuivey and Keefer [25] integrated linear one-dimensional flow with dispersion equations for estimating  $K_x$ . Fischer [26], Liu [27], Iwasa [28] and Koussis and Rodriguez-Mirasol [29] accounted the impact of lateral flow velocity gradient on  $K_x$  and developed simple equations. Seo and Cheong [11] suggested a one-step regression method using hydraulic and geometric field data from

26 rivers for estimating  $K_x$ . Deng *et al.* [30] derived a theoretical equation of  $K_x$  for  $\frac{B}{H} > 10$ . Kashefipour and Falconer [31] also proposed two-step regression models for estimating  $K_x$ using 81 data sets measured in natural streams of the USA. Seo and Baek [19] and Papadimitrakis and Orphanos [32] extended several empirical equations for estimating  $K_x$  in various ranges of  $\frac{B}{H}$  values. These equations have several limitations, such as narrow calibration data, a small range of applicability, non-generality of collected data, and weak estimates over unseen data. Furthermore, most of the reported empirical and theoretical equations were developed using particular assumptions and channels features. The performance of these equations changes broadly for their calibrated flow ranges and stream condition, and for smaller or more extensive ranges of flow have not accurate results [17], [33]. Hence, it is crucial to develop a model that would have an appropriate application in the global range of river and flow conditions.

Data-driven techniques for over a decade have been used to evaluate many hydraulic and hydrologic problems. Regarding the  $K_x$  estimation, the most frequently data-driven tools are ANN [17], [34], [35], ANFIS [15], [23], [36], genetic programming [37]–[39], SVM [36], [40], particle swarm optimization [41], differential evolution [42], Granular Computing Model [43], Polynomial regression [44] and regression kriging [18]. These studies are some of the recently published researches that have been widely carried out to estimate  $K_x$  based on a limited number of data and a small range of applicability. High accuracy and less uncertainty in  $K_x$  estimations have been observed using ANFIS technique in comparison with the other models and equations [15], [20], [23], [34], [39].

Recently, Nature-inspired optimization systems have been used in different fields of model optimization. In the field of artificial intelligence, these algorithms provide a solution to achieve improved performance of non-optimized models [45]. Firefly algorithm (FFA) is a novel meta-heuristic optimization algorithm that has provided the desired enhancement and improvement in the modeling accuracy. The FFA imitates the flashing behavioral patterns of fireflies [46] based on their frequency, duration, and brightness [45]. The FFA structure can effectively and simultaneously found the local and global optima in the dataset and solve multimodal optimization problems [47]–[50].

The FFA hybridized with ANFIS model is used to progress the accuracy of estimations, such as estimating the roller length of a hydraulic jump [51] and monthly streamflow forecasting [45]. These studies have proved that the FFA approach is able to eliminate the inaccuracy in estimation of extremely shallow stream flows. Furthermore, FFA have been used effectively in different studies such as estimating the minimum velocity in sewer pipes [52], [53], estimating field capacity and permanent wilting point in soil samples [54], forecasting electrical load [49], optimization of Van-Genuchten model parameters in soil-water characteristic curve [55] and selection of relevant attributes [56]. Their results have shown more robustness of FFA compared to the other optimization methods. The significant shortcomings of the previous studies over longitudinal dispersion estimation and the implemented methodologies are small range of used data, narrow calibration data, small range of applicability, non-generality of collected data, weak estimates over unseen data and ANFIS learning by mathematical methods. By considering all of these shortcomings, this research aims to provide further improvements for inferring the embedded mechanism in an extended database of K<sub>x</sub> by hybridizing the nature-inspired algorithm FFA with traditional ANFIS. This will improve the accuracy of the ANFIS technique as it adjusts and optimizes the modeling parameters based on a global database of Kx. In this research, the functional form of equation (3) is used for developing a novel accurate methodology of ANFIS-FFA technique to estimate K<sub>x</sub> in natural rivers based on a global database. Also, for the first time, SSMD is hybridized with the ANFIS-FFA for the best subset selection of the train and test sets. The observed Kxvalues of different worldwide rivers are collected and used for evaluating the fitness of models. The proposed ANFIS-FFA model presents the relation between K<sub>x</sub> as output, and hydraulic and geometric parameters as inputs. There is no need for assumptions on the hydraulic and geometric parameters of flow in the ANFIS-FFA model. The rest of the paper is organized as follows: Section II represents the datasets and preprocessing, ANFIS, FFA, and hybrid models implemented in the simulations and evaluation criteria. Section III contains the results and discussions about the proposed model. Finally, in Section IV, the conclusions were drawn.

## **II. MATERIAL AND METHODS**

### A. LONGITUDINAL DISPERSION DATA COLLECTION

There is an extensive set of the hydrodynamic and geometric parameters affecting the K<sub>x</sub> values in natural streams. Among all, channel width (B), flow depth (H), flow velocity (U), and bed shear velocity  $(U^*)$  strongly affect the K<sub>x</sub> [20], [39]. U affects the driving force of flow and U\* increases the longitudinal transfer of pollutant. B and H are geometrical parameters of the river cross-section that define and magnify the transverse distribution of longitudinal flow components and produce transverse velocity gradients as the main agent of dispersion. Also, vertical mixing is related to the flow depth H and can affect the dispersion process. Both dimensional and non-dimensional combinations of these parameters have been used for  $K_x$  estimation in previous studies. As the dimensional value of K<sub>x</sub> is utilized in practical applications and numerical models, in this paper, a dimensional estimation is carried out. For this purpose, a field data bank, including 503 data points from different worldwide rivers are collected from the literature [27], [30], [31], [57]-[69] (Appendix 1). Table 1 represents the statistical features of subsets, which are selected by SSMD (discussed in the next section). Table 1 shows that the river width varies from 0.2 to 867 meters, flow depth varies from 0.034 to 19.6 meters, and  $K_x$  varies from 0.005 to 1798.60 m<sup>2</sup>/s, which declares the

TABLE 1. Statistical characteristics of t	the dataset variables (	(after Riahi-Madvar <i>et al.</i> 2019).
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Data Set	Parameter	Min	Max	Mean	SD	Skewness	Kurtosis
	<b>B</b> (m)	0.2	867	56.49	110.87	4.86	28.37
	H (m)	0.034	19.9	1.42	2.31	4.60	27.43
Total	U (m/s)	0.022	1.74	0.49	0.31	1.26	2.25
(503 data)	<b>U</b> <sup>*</sup> ( <b>m</b> / <b>s</b> )	0.001	0.99	0.066	0.07	7.098	74.00
	K (m <sup>2</sup> /s)	0.005	1798.60	71.56	191.99	5.55	36.85
	B (m)	0.2	867	63.89	118.13	4.46	23.68
	H (m)	0.034	19.9	1.56	2.46	4.44	25.018
Train (351 data)	U (m/s)	0.022	1.74	0.47	0.33	1.29	1.876
(,	U*(m/s)	0.001	0.99	0.07	0.08	7.07	69.49
	K (m <sup>2</sup> /s)	0.004	1798.60	78.76	194.22	5.27	34.374
	B (m)	0.19	857	40.19	90.75	6.49	51.66
	H (m)	0.058	16.76	1.10	1.88	5.09	34.86
Test	U (m/s)	0.023	1.71	0.53	0.27	1.48	4.49
(1320818)	<b>U</b> <sup>*</sup> ( <b>m</b> / <b>s</b> )	0.003	0.51	0.07	0.05	5.18	41.10
	K (m <sup>2</sup> /s)	0.008	1490	54.71	186.92	6.47	46.04

generality of collected database and their extensive ranges. In this research, four variables, including B, H, U and U<sup>\*</sup> are considered as input vector of the estimative models and  $K_x$  assigned as the output of the models. All possible combinations (fifteen) of four input variables are used. Fifteen different model structures were used, and analysis of the results were carried out to show the sensitivity of each parameter on the model output in the train, test and overall data. For this purpose, 15 possible input combinations that are represented in Table 2 are considered.

TABLE 2.	<b>Different input vecto</b>	r combinations	used for	<b>ANFIS-FFA</b>
developm	ents.			

Model	input parameter(s)
1	B, H, U, U*
2	B, H, U
3	H, U, U*
4	B, H, U*
5	В, Н
6	U,U*
7	B,U
8	B,U*
9	U,H
10	U*,H
11	В
12	U*
13	Н
14	U
15	B,U,U*

### **B. DATA PRE-PROCESSING BY SSMD**

For a robust estimation, it is necessary to calibrate and train the model appropriately by selecting a suitable training set. The training performance highly depends on the dataset that is utilized for train purpose. There is no unique method for selecting the training and testing datasets. Trial and error and cross-validation methods were used in subset selection in previous studies of artificial intelligence [15], [70], [71]. In this research, we explore a robust algorithm to divide data into subsets and extract proper training set. One of the main factors in train and test subset selection is that the statistical characteristics of both training and testing subsets must be approximately identical. For example, if the train subset does not include the extreme values, but the test subset has several extreme values, the model could not be able to accurately estimate the extreme values and vice versa. This reduces the global applicability of trained models. To remedy this problem, in this research, SSMD method [72] was used for finding optimum subsets and random data manipulation to categorize training and testing subsets. In general, the SSMD method is capable of selecting the training and testing subsets in such a way that the statistical characteristics of subsets, including the maximum, minimum, mean, and standard deviation are stable, which guarantee a reliable estimation. The SSMD was first introduced by Kennard and Stone (1969) [73]. Based on SSMD, the data with the highest dissimilarity to others in the data set are selected [74] to characterize the overall behavior of the dataset. To remove the scale effects, before subset selection, the data are normalized as follows [6]:

$$x_n = \frac{x_i - x_{\min}}{x_{\max} - x_{\min}} \tag{4}$$

Then subsets are de-normalize as:

$$x_i = x_n \left( x_{\max} - x_{\min} \right) + x_{\min} \tag{5}$$

In this research, 70% and 30% of the whole dataset are selected automatically by SSMD as training and testing subsets, respectively. For more details on the SSMD method, one can refer to [6], [7], [39], [73]–[76]. Table 1 represents the statistical features of selected subsets. Also, Figure 1 shows the distribution of selected subsets. From Table 1 and Figure 1, it can be concluded that the SSMD is capable of propagating the extreme values in training and testing subsets equally, which eliminates the trial and error subset selection and improve the applicability and reliability of estimations. Figure 1 shows that the scattering of the training subset contains the borders of the database, and the members of the testing subset are positioned within the training subset. Subsequently, it expects that the trained models with SSMD suitably can realize the outliers' behavior in the database. Based on the results in this figure, the changes of variables in the train subset are greater than the test subset, and this increase the generalization of extrapolation models. The critical distinctiveness of the SSMD is that it spreads the extreme values in the train and test sets and does not eliminate them from modeling. For a global database as used in this paper, The SSMD, by extending the cover limits of the train set, strengthens the global uses of established estimations.

As Figure 1 shows, although the training set includes the upper and lower limits of the database, also there are some extreme values in test sets, and both of the selected datasets have a uniform pattern of variables that avoids the overfitting of the model. Indeed by using the SSMD, the selection process is progressed in such a way that there will be maximum dissimilarity between the members of an individual set and the same values will not occur in one set.

### C. ADAPTIVE NEURO-FUZZY INFERENCE SYSTEM (ANFIS)

The Fuzzy logic (FL) developed by Zadeh [77] is based on semantic uncertainty, which effectively used in various environmental and water resources problems [78]. Fuzzy inference system is a rule-based structure with three conceptual mechanisms, including a rule-based structure, a database of models and an inference system. The first component is based on if-then rules, while the second defines the membership function, and the third is the combination of the rules







FIGURE 1. The coverage and distribution of train and test subsets.

and producing the results [79], [80]. An automatic procedure for the optimization of membership function features and adjusting parameters is needed [79], [81], [82]. ANFIS, which is the integration of fuzzy logic and artificial neural network (ANN) is used to overcome this problem [83], [84]. Generally speaking, ANFIS is a multi-layer feed-forward network based on the ANN learning capabilities and fuzzy thinking [79], [85]–[87]. Tsumoto, Mamdani and Sugeno are three categories of ANFIS, while the Sugeno is the most popular [88], [89] and used in this research. Also, there are several membership functions (including Trapezoidal, Gaussian, Sigmoid, Triangular, Generalized bell-shaped, etc.) for ANFIS [90]. The selection of the membership function is a crucial part of ANFIS modeling. A Sugeno first-order fuzzy model with four inputs and one output is described here to show how the ANFIS system works. In this research,

geometric and hydrodynamic parameters of flow are the input and longitudinal dispersion coefficient  $(K_x)$  is the output variables. The rules for the ANFIS system are presented in equations (6) and (7):

Rule 1: IF H is  $A_1$ , U<sup>\*</sup> is  $B_1$ , U is  $C_1$  and B is  $D_1$  then

$$K_{X_1} = a_1 H + b_1 U^* + c_1 U + d_1 B + r_1 \tag{6}$$

Rule 2: IF H is  $A_2$  and U<sup>\*</sup> is  $B_2$ , U is  $C_2$  and B is  $D_2$  then

$$K_{X_2} = a_2 H + b_2 U^* + c_2 U + d_2 B + r_2 \tag{7}$$

In which  $a_i$ ,  $b_i$ ,  $c_i$  and  $d_i$  are the parameters which would be optimized by the FFA during the training procedure,  $K_{xi}$  is the output of the fuzzy system, and  $A_i$ ,  $B_i$ ,  $C_i$  and  $D_i$  are the fuzzy sets. Figure 2 shows the schematic ANFIS model, which is used in this study. Based on Figure 2, there are five layers in ANFIS modeling, which briefly discussed here.



FIGURE 2. The architecture of ANFIS in K<sub>x</sub> estimation.

*Layer 1:* The input layer adopts the activation function on input variables.

$$O_{1,i} = \mu_{Ai}(x) \quad for \ i = 1, 2, \ or$$
  
$$O_{1,i} = \mu_{Bi-2}(y) \quad for \ i = 3, 4 \tag{8}$$

where one of the B, H, U and U<sup>\*</sup> is the input to each node and  $A_i$  or  $B_{i-2}$  is related linguistic label and  $O_{1,i}$  is the membership grade of fuzzy sets. In this step, several membership functions are tested and finally, Gaussian membership function is used.

$$\mu_{Ai}(x,\sigma,c) = e^{\frac{-(x-c)^2}{2\sigma^2}}$$
(9)

In which  $\sigma$  and care membership function of variables set. So the output of the first layer is as follows:

$$\mathcal{O}_{1,i=}\mu_{Ai}(x) = e^{\frac{-(x_i - c_i)^2}{2\sigma_i^2}}$$
(10)

*Layer 2:* This layer determines the membership degree of inputs.

$$O_{2,i} = \mu_{Ai}(x)\mu_{Bi}(y) \quad i = 1, 2 \tag{11}$$

Layer 3: This layer calculates the relative weights of inputs.

$$O_{3,i} = \bar{w}_i = \frac{w_i}{w_1 + w_2} \quad i = 1, 2 \tag{12}$$

Layer 4: This layer adopts inputs with relative weights.

$$O_{4,i} = \bar{w}_i K_{x_i} = \bar{w}_i (a_i H + b_i U^* + C_i U + D_i B + r_i)$$
(13)

Layer 5: This layer calculates the final output of the model.

$$O_{5,i} = \sum_{i} \bar{w}_i K_{x_i} = \frac{w_1 K_{x_1} + w_2 K_{x_2}}{w_1 + w_2} \tag{14}$$

In general, ANFIS has a high capability in learning and classifying input-output data. However, training the ANFIS model to obtain optimal membership function and parameters is time-consuming. So, in this research, The Firefly Optimization Algorithm (FFA) was utilized to solve this problem

### D. FIREFLY ALGORITHM AND HYBRIDIZING ANFIS-FFA

In the present paper, the firefly optimization algorithm (FFA) was utilized to find the optimum values of parameters for the membership function. FFA was introduced by Yang [48], which is based on firefly behavior and flashing features. The mata-heuristic algorithms such as FFA need proper setting of parameters and need several iterations to find the optimal response. In reverse, faster convergence and low probability of entrapping in local optima are two main advantages of these algorithms.

The flashing features are categorized into three rules [48]:

- The fireflies assumed to be unisex and as a result, attracting to other fireflies is not based on the sex.
- The attractiveness is relative to the brightness and in the case that no one is brighter, the movement is random.The brightness is proportional to the light emission.

Based on these three rules, the brightness and the intensity of light emission can be the objective function [45]. The firefly



FIGURE 3. The flowchart of integrated SSMD with ANFIS-FA modeling.

light intensity and attractiveness were formulated as follows:

$$I = I_0 e^{-\gamma r}$$
  
$$\beta = \beta_0 e^{-\gamma r^2}$$
(15)

where *I* and  $\beta$  are firefly light intensity and attractiveness, respectively.  $I_0$  and  $\beta_0$  represent the original light intensity and attractiveness at r=0, r is the distance of two fireflies and  $\gamma$  is the light absorption coefficient. The Cartesian distance between two fireflies introduces as [48]:

$$r_{ij} = \|x_i - x_j\|_2 \tag{16}$$

The distance is not to be Cartesian distance and also can be the time delay and, etc. [48]. Also the movement of one firefly by another one is defined as [48]:

$$x_i = x_i + \beta_0 e^{-\lambda r_{ij}^2} \left( x_j - x_i \right) + \alpha \varepsilon_i$$
(17)

where  $\alpha$  and  $\varepsilon_i$  are randomization coefficient (between 0 and 1) and random number vector, respectively [45].

In this paper, 15 models with different input variables that have only 1 output parameter of  $K_x$  are developed (Table 2). The ANFIS-FFA uses root-mean-square error (RMSE) as the cost function in the optimization of the ANFIS parameters.

The limits of parameters that are optimized by the cost function in FFA should be identified first. In the hybrid optimization flowchart, as presented in Figure 3, each firefly includes a set of two types of optimization parameters, antecedent and consequent parameters given in equations 9, 10 and 13. In this paper in the M1 model, as the best one from 15 models, B, H, U and U<sup>\*</sup> are used as input vector, and the associated output parameter ( $K_x$ ) is estimated. If the input vector has three fuzzy membership functions of Gaussian MFs, then the IF–THEN rules can be written as:

Rule s: IF B is  $F_1^i(s_{1i}, c_{1i})$  and H is  $F_2^i(s_{2i}, c_{2i})$  and U is  $F_3^i(s_{3i}, c_{3i})$  and U<sup>\*</sup> is  $F_4^i(s_{4i}, c_{4i})_1$  then

$$K_{xs} = a_s B + b_s H + c_s U + d_s U^* + r_s$$
(18)

The parameters of ANFIS that should be optimized are  $(s_{ji}, c_{ji}, a_s, b_s, c_s, d_s, r_s)$  and these parameters are decision variables in the optimization problem. These parameters for all of the associated rules and MFs need to be determined. The primary firefly population is selected randomly, and each firefly is imagined into the ANFIS parameters set. According to each firefly's light intensity, the attractiveness (cost) of each firefly (ANFIS parameter) is calculated and assessed,

and fireflies (parameter values) with the lowest light move toward parameters with the highest cost (brightness). Consequently, the cost function is calculated. The cost function in this paper is the minimization of root mean square error (RMSE) of estimations in regard to decision variables. This procedure cycles until the maximum generation value or minimum preferred cost function are derived. Figure 3 shows the flowchart of hybrid SSMD with ANFIS–FFA that is used in this paper to estimate  $K_x$ .

# E. EVALUATION CRITERIA

There are several statistical performance evaluation criteria for model assessment. In this paper, eight statistical evaluation criteria, including the root mean square error (RMSE), the coefficient of determination ( $\mathbb{R}^2$ ), mean absolute error (MAE), the Nash-Sutcliffe Efficiency (NSE), index of agreement (d), persistence index (PI), confidence index (CI) and relative absolute error (RAE) were utilized for model evaluation. The explanation of these criteria was presented elsewhere [80], [91], [92]. Also, visualize approaches, including scatter plot, Taylor diagram [93], ellipse confidence bounds, and the probability distribution of revised discrepancy ratio (RDR) are used to evaluate the model results.

Beside these criteria, a revised discrepancy ratio (RDR) was used. Discrepancy ratio (DR) was introduced by White *et al.* [94] to examine the model robustness:

$$DR = Log\left(\frac{\text{Predicted Value}}{\text{Observed Value}}\right)$$
(19)

However, this form of DR is not applicable to zero or negative values. Noori *et al.* [95] proposed a new index (DDR) based on the DR to remedy this problem. However, the logarithmic base of the DR is eliminated in DDR:

$$DDR = \frac{Forecasted Value}{Observed Value} - 1$$
(20)

Because of these shortcomings, RDR was proposed by Memarzadeh *et al.* [76] as a new index which is capable of using for all negative, positive values and the logarithmic base of DR remains and calculates the normalized error of estimated values as follows:

$$RDR = Sign (\text{Estimated}.K_x - \text{Measured}.K_x) \\ \times \left| \log \left| \frac{\text{Estimated}.K_x}{\text{Measured}.K_x} \right| \right|$$
(21)

In the case of over estimation of model results, the value of RDR >0, in the case of underestimation, RDR<0, and for exact estimations, RDR is equal to zero.

### **III. RESULTS AND DISCUSSION**

The results of ANFIS-FFA and previously published equations are presented in this section. To evaluate the results of models and compare their capability versus existing equations, some graphical and statistical indices are used. In next subsection the results of ANFIS-FFA with different input parameters and comparing the best ANFIS-FFA model with existing equations are presented respectively.

### A. RESULTS OF ANFIS-FFA MODEL

The ANFIS model is trained by Firefly Algorithm using 503 data points, which are collected from previously published data. The SSMD approach is used to select the training and testing data subset of models, as described previously. The 351 number of  $K_x$  values contains the training data set, whereas 152 remaining ones are used in the testing stage. The primary comparative analysis in this research shows that the input vector in the dimensional state is superior to dimensionless values. So in this research, the dimensional parameters of U(m/s), U\*(m/s), B(m) and H(m) were used. The input layer of the ANFIS model has a different combination of these 4 parameters, and by this way, 15 models are trained using FFA. The output layer of ANFIS-FFA includes a single variable as Kx. As described previously in the ANFIS structure, each input parameter has several parameters in terms of rules, and furthermore, each rule contains several parameters of membership functions. The membership function type, the number of clusters, and type of FIS are determined by trial and errors. It was found that the best is the Gaussian membership function with two parameters, 8 clusters (number of membership functions for each variable) and genfis3. In this research, the FIS structure (genfis3) is of the specified type, Sugeno and 8 numbers of clusters to be generated by fuzzy c-means (FCM) clustering. The input and output membership function types are 'gaussmf' and 'linear', respectively. The symmetric Gaussian function depends on two parameters sigma and c (Eq.10). The linear output function has 5 parameters (Eq. 13). So the input parameters that should be determined are 4. In this research, each parameter has 8 rules (membership functions), and each rule contains 2 parameters. In the largest input vector, there are 64 (4 variable  $\times$ 8 rules  $\times$ 2 parameters) parameters that must be optimized by the firefly algorithm in layer 2. In layer 3, this combination produces  $4^8$  nodes and in layer 5, there are  $2^3 \times 5$  unknown parameters within the de-fuzzifcation process. So, we have 104 ANFIS parameters that should be determined and optimized by the firefly algorithm. In other cases with a reduced number of input variables (Table 2), the numbers of optimization parameters are reduced proportionally.

In this paper, all possible combinations of U, U\*, B and H variables are used (Table 2). The FFA is used in all 15 combinations of input vector (Table 2) for the optimization of ANFIS parameters over the training data set selected by SSMD. In Figure 4, the variation of the best cost function with generations in the M1 model of ANFIS-FFA is shown. It shows the trend of cost reduction as a function of iteration over the firefly optimization process, and it was found that after 500 generations, the best solution was achieved and the model converged to the optimized parameters of ANFIS. The final results of 15 ANFIS-FFA models are summarized in Figures 5-9 and Tables 3-5. Figure 5 visualizes the Taylor diagram of Kx estimated by ANFIS-FFA with different input parameters in the train, test and overall of the data. The Taylor diagram visually compares the quantitative performance of 15 ANFIS-FFA models for the train, test and all

	M1	M2	M3	M4	M5	M6	M7	M8	M9	M10	M11	M12	M13	M14	M15
RSQ	0.72	0.76	0.71	0.62	0.61	0.70	0.56	0.63	0.53	0.71	0.42	0.31	0.28	0.53	0.76
RMSE(m <sup>2</sup> /s)	102.25	95.34	104.47	119.72	121.49	106.61	128.90	117.06	131.97	103.42	147.69	160.77	164.16	132.66	95.16
MAE	51.42	49.11	56.65	54.46	56.28	60.61	59.43	52.95	60.09	53.84	63.79	85.05	74.95	68.80	44.58
PI	0.86	0.88	0.86	0.81	0.81	0.85	0.79	0.82	0.77	0.86	0.72	0.67	0.65	0.77	0.88
RAE	0.52	0.50	0.57	0.55	0.57	0.61	0.60	0.54	0.61	0.54	0.65	0.86	0.76	0.70	0.45
d	0.91	0.92	0.91	0.87	0.86	0.90	0.84	0.88	0.82	0.91	0.74	0.66	0.63	0.82	0.93
NSE	0.72	0.76	0.71	0.62	0.61	0.70	0.56	0.63	0.53	0.71	0.42	0.31	0.28	0.53	0.76
CI	0.66	0.70	0.64	0.53	0.52	0.63	0.46	0.55	0.44	0.65	0.31	0.20	0.18	0.44	0.70

TABLE 3. Results of ANFIS-FFA models for estimation of K<sub>x</sub> over training data.



FIGURE 4. Convergence process and best cost variations of ANFIS-FFA over generation.

of the data. This figure evaluates the quantitative accuracy of ANFIS-FFAs comparatively and shows that the nearest estimations to the observed values of  $K_x$  are reproduced in M1. As it is expected, the models with one or two inputs had the worst performance.

Tables 3-5 shows that by increasing the number of input parameters, the model result improved. The  $R^2$  values of the M1 model in the train, test and overall data are 0.72, 0.67 and 0.7, respectively and MAE values are 51.72, 48,

50.6 and NSE are 0.72, 0.63 and 0.7, respectively. These values show the superiority of the M1 model over the others. Figure 6 shows the RDR distribution of the best 6 models in the test step, including M1, M2, M5, M7, M9 and M14, and M1, M2, M4, M5 M6 and M7 for overall data. In these graphs, further inclination in RDR spreading to the centerline and higher values of the maximum RDR are related to more accuracy. Based on this figure, the selected models in regard to RDR have some positive skewness, but in comparison with wide ranges of input and output values in Table 1, the overall performances are valuable.

Observed and predicted  $K_x$  and associated errors in the training and testing steps for M1 using ANFIS-FFA are drawn in Figures 7 and 8, respectively. It is noticeable that the estimated and measured values have the same trends, and the measured and estimated  $K_x$  values have approximately similar patterns. The model estimations are accurate, particularly at small or large  $K_x$  values, and have an acceptable correlation with measurements. From these figures, it is finding out that ANFIS-FFA accurately can inference the inherent relationships between four hydraulic and geometric features of natural rivers (U, U<sub>\*</sub>, B, H) with  $K_x$ . It must be noted that the main aim of the research was to improve ANFIS capabilities in



FIGURE 5. Taylor diagram for training, testing and overall data for all combinations of variables in ANFIS-FFA.

#### TABLE 4. Results of ANFIS-FFA models for estimation of K<sub>x</sub> over testing data.

	M1	M2	мз	M4	M5	M6	M7	M8	M9	M10	M11	M12	M13	M14	M15
BSO	0.67	0.64	0.24	0.57	0.71	0.11	0.72	0.22	0.71	0.07	0.52	0.02	0.25		0.22
ĸsų	0.07	0.04	0.24	0.57	0.71	0.44	0.72	0.22	0.71	0.07	0.52	0.02	0.35	0.04	0.23
RMSE(m <sup>2</sup> /s)	113.14	146.63	285.55	127.55	100.05	162.49	98.63	191.73	104.04	207.65	132.88	231.15	157.53	118.93	183.80
MAE	48.00	45.99	75.63	42.28	39.99	61.78	36.99	58.03	44.08	63.82	45.18	103.24	52.52	60.80	49.22
PI	0.82	0.70	-0.13	0.77	0.86	0.63	0.86	0.49	0.85	0.40	0.75	0.26	0.66	0.80	0.53
RAE	0.66	0.63	1.04	0.58	0.55	0.85	0.51	0.80	0.61	0.88	0.62	1.42	0.72	0.84	0.68
d	0.85	0.87	0.60	0.78	0.91	0.80	0.91	0.64	0.89	0.42	0.76	0.30	0.54	0.83	0.64
NSE	0.63	0.38	-1.35	0.53	0.71	0.24	0.72	-0.06	0.69	-0.24	0.49	-0.54	0.28	0.59	0.03
CI	0.53	0.33	-0.81	0.42	0.65	0.19	0.65	-0.04	0.61	-0.10	0.37	-0.16	0.15	0.49	0.02

TABLE 5. Results of ANFIS-FFA models for estimation of K<sub>x</sub> over all data.

	M1	M2	M3	M4	M5	M6	M7	M8	M9	M10	M11	M12	M13	M14	M15
RSQ	0.69	0.68	0.41	0.59	0.63	0.59	0.60	0.47	0.57	0.47	0.43	0.16	0.28	0.54	0.57
RMSE(m <sup>2</sup> /s)	107.70	115.08	180.21	123.92	117.40	127.69	122.47	145.06	126.05	144.34	144.96	185.85	163.56	130.42	129.97
MAE	51.43	49.21	63.36	51.85	52.45	62.00	53.76	5`5.51	56.34	57.86	59.26	91.53	69.28	67.45	47.01
Ы	0.85	0.83	0.58	0.80	0.82	0.79	0.80	0.72	0.79	0.73	0.73	0.55	0.65	0.78	0.78
RAE	0.55	0.53	0.68	0.55	0.56	0.66	0.57	0.59	0.60	0.62	0.63	0.98	0.74	0.72	0.50
d	0.90	0.90	0.78	0.85	0.88	0.87	0.86	0.81	0.84	0.81	0.75	0.56	0.62	0.83	0.86
NSE	0.69	0.64	0.12	0.59	0.63	0.56	0.60	0.43	0.57	0.44	0.43	0.07	0.28	0.54	0.54
CI	0.62	0.58	0.10	0.50	0.55	0.49	0.51	0.35	0.48	0.35	0.32	0.04	0.17	0.45	0.47



FIGURE 6. RDR values for the best ANFIS-FFA models using A) test and B) all of the data.

global conditions of natural rivers without clustering the data based on variable ranges, where will reduce the generality of estimation model and causes the over fitting challenges in artificial model estimations.

Figure 9 shows the regression plots of the ANFIS-FFA estimation versus the measured  $K_x$  values in the training, testing steps and all of dataset. The correlation coefficient (R), as an index of the linear correlation between the estimated and measured  $K_x$ , was calculated and presented for M1 using

the ANFIS-FFA model in these figures. The results show acceptable agreement with the high R (0.84 and 0.85) and the 95% confidence ellipse of estimations. The blue points are those beyond the 95% bound of observations, and the green points are those inside the 95% confidence bound. From Figure 9, it is clear that in train step, 17 points of 352 number of observations (4.8%), in test step, 5 of 151 (3.3%) and over all data, 22 of 503 (4.4%) estimations are outside of the 95% ellipse bounds. It is concluded that the M1 model



FIGURE 7. Comparing observed K<sub>x</sub> versus predicted M1 ANFIS-FFA in train phase.



FIGURE 8. Comparing observed  $K_x$  versus predicted M1ANFIS-FFA in the test phase.



FIGURE 9. Scatter plot of observed Kx versus ANFIS-FFA predictions and 95% confidence ellipse for the best-selected model.

in ANFIS-FFA shows a satisfactory relationship between the estimated and observed  $K_x$  for most of the data points and the greatest part of the data points placed alongside the imagined unique line. Indeed, it is realized that in M1 using ANFIS-FFA, the number of both overestimation or underestimation of  $K_x$  is limited. Therefore, it is apparent that the  $K_x$ estimated by ANFIS-FFA benefits from the uppermost level of accuracy. **TABLE 6.** Empirical equations used in K<sub>x</sub> estimations.

Model	Formula
Fischer (1975)	$K_x = .011 \left(\frac{U}{U^*}\right)^2 \left(\frac{B}{H}\right)^2 HU^*$
Liu (1977)	$K_x = .18 \left(\frac{U}{U^*}\right)^{0.05} \left(\frac{B}{H}\right)^2 H U^*$
Seo and Cheong (1998)	$K_x = 5.92 \left(\frac{U}{U^*}\right)^{1.43} \left(\frac{B}{H}\right)^{.62} HU^*$
Deng et al. (2002)	$K_{x} = \frac{0.15}{8\varepsilon_{t}} \left(\frac{U}{U^{*}}\right)^{2} \left(\frac{B}{H}\right)^{1.67} HU^{*} \varepsilon_{t} = 0.145 + \frac{\left(\frac{U}{U^{*}}\right) \left(\frac{B}{H}\right)^{1.38}}{3520}$
	$K_x = 10.612 \left(\frac{U}{U^*}\right)^2 H U^*$ For $\frac{B}{H} > 50$
Kashefipour and Falconer (2002)	$K_{x} = \left[7.428 + 1.775 \left(\frac{B}{H}\right)^{.62} \left(\frac{U}{U^{*}}\right)^{.572} \right] \left(\frac{U}{U^{*}}\right)^{2} HU^{*} \text{ For } \frac{B}{H} < 50$
Sattar and Gharabaghi (2015)	$K_{x} = 8.45 \left(\frac{U}{U^{*}}\right)^{1.65} \left(\frac{B}{H}\right)^{0.5 - 0.514 F_{r}^{0.516} + \frac{U}{U^{*}} 0.42^{\frac{U}{U^{*}}}} HU^{*}$
Wang et al. (2017)	$K_{x} = \left(0.718 + 47.9\frac{H}{B}\right)\left(\frac{U}{U^{*}}\right)\left(\frac{B}{H}\right)HU^{*}$
Alizadeb et al. $(2017)$	$\frac{K}{HU^*} = 5.319 \left(\frac{U}{U^*}\right)^{0.075} \left(\frac{B}{H}\right)^{1.206} \text{ For } \frac{B}{H} \le 28$
Alizadeli et al. (2017)	$\frac{K}{HU^*} = 9.93  l \left(\frac{U}{U^*}\right)^{1.802} \left(\frac{B}{H}\right)^{0.187} \text{ For } \frac{B}{H} > 28$

# B. COMPARING ANFIS-FFA WITH ANFIS AND EMPIRICAL EQUATIONS

To evaluate the robustness of the ANFIS-FFA model in regard to empirical equations, the K<sub>x</sub> was calculated for the test and all of the data using eight formulas that were developed in previous studies. The empirical equations are presented in Table 6. Also, the ANFIS model is developed to compare its results with ANFIS-FFA. A comprehensive evaluation of the M1 results by ANFIS-FFA with results of equations and conventional ANFIS over the test and all of the dataset are presented in Tables 7 and 8 for both dimensional and nondimensional results. Indeed, these tables present the values of the statistical indices used to validate the applicability of published existing equations in estimating K<sub>x</sub> for extended data from small to large rivers. The best results that are presented in Tables 7 and 8 are for equation Alizadeh et al. [41] with  $R^2 = 0.20$ , NSE=0.17 in test data and  $R^2 =$ 0.16, NSE = -0.02 over all of the data, respectively in dimensional results. In the Non-dimensional values, the best results are derived by the Seo and Cheong [11], equation with  $R^2 = 0.37$  and NSE = -0.32 in the test set and  $R^2 =$ 0.24 and NSE = -0.38 over all of the data. These values show the limitation and weakness of empirical equations in the new database of  $K_x$ . After that, the equations of Sattar and Ghorbani [38] and Kashefipour and Falconer [31] have more accurate estimations for dimensional values among the existing K<sub>x</sub> equations and have better results in comparison with the Seo and Cheong [11], Wang et al., Fischer [26] and Deng et al. [30] equations. However, all of these equations have very low accuracy and high error than the ANFIS-FFA and ANFIS. The estimated values represented in these tables show that the collected data are very global, general and scattered, in such a way that nearly all of the equations have high error, and even the best equations do not yield reasonable estimations of K<sub>x</sub>. According to these results, the ANFIS-FFA model is superior to the existing equations and conventional ANFIS model. In ANFIS model, the statistical parameters for the test step are  $R^2 = 0.37$ , RMSE = 463.34, MAE=85.69,

TABLE 7.	Results of	equations fo	r estimation	of K <sub>x</sub>	over	testing data	
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Parameters	Statistics	Fischer (1975)	Liu (1977)	Seo and Cheong (1998)	Deng et al. (2002)	Kashefipour and Falconer (2002)	Sattar and Gharabaghi (2015)	Alizadeh et al. (2017)	Wang et al. (2017)	ANFIS	ANFIS- FFA
	$\mathbf{R}^2$	0.22	0.19	0.22	0.35	0.14	0.15	0.20	0.24	0.37	0.67
	RMSE(m <sup>2</sup> /s)	1685.56	169.31	575.47	1008.02	687.33	516.97	169.14	198.92	463.34	113.14
Dimensional Values	MAE	275.05	44.00	92.15	628.76	234.62	87.34	55.40	50.88	85.69	48.00
	PI	-38.49	0.60	-3.60	-13.12	-5.57	-2.71	0.60	0.45	-1.98	0.82
	RAE	3.78	0.60	1.27	8.64	3.22	1.20	0.76	0.70	1.18	0.66
	d	0.18	0.50	0.40	0.30	0.31	0.37	0.58	0.65	0.54	0.85
	NSE	-80.95	0.17	-8.55	-28.31	-12.63	-6.71	0.17	-0.14	-5.19	0.63
	CI	-14.24	0.09	-3.42	-8.62	-3.93	-2.51	0.10	-0.09	-2.79	0.53
	<b>R</b> <sup>2</sup>	0.26	0.15	0.37	0.001	0.03	0.15	0.01	0.16	0.11	0.35
	RMSE	5836.35	934.24	1060.62	53123.56	8862.50	1054.34	1418.09	870.93	3269.88	874.50
	MAE	1516.55	365.90	638.99	30357.72	5382.46	666.86	975.77	541.76	1932.09	520.80
Non-	PI	-18.91	0.49	0.34	-1648.46	-44.91	0.35	-0.18	0.56	-5.25	0.55
Values	RAE	3.36	0.81	1.42	67.27	11.93	1.48	2.16	1.20	4.28	1.15
	d	0.25	0.56	0.71	0.01	0.03	0.57	0.24	0.51	0.34	0.73
	NSE	-38.96	-0.02	-0.32	-3309.36	-91.13	-0.30	-1.36	0.11	-11.54	0.10
	CI	-9.92	-0.01	-0.23	-35.13	-2.57	-0.17	-0.32	0.06	-3.96	0.07

**TABLE 8.** Results of equations for estimation of K<sub>x</sub> over all data.

Parameters	Statistics	fisher 1975	Liu 1977	Seo and Cheong (1998)	Kashefipour and Falconer (2002)	Sattar and Gharabagh i (2015)	Wang et al. (2017)	Alizadeh et al. (2017)	Deng et al. (2002)	ANFIS	ANFIS- FFA
	$\mathbf{R}^2$	0.03	0.05	0.17	0.01	0.11	0.20	0.16	0.10	0.12	0.69
Dimensional Values	RMSE(m <sup>2</sup> /s)	6248.99	273.47	594.01	2334.09	541.67	214.27	194.71	1751.11	323.86	107.70
	MAE	760.85	73.20	132.68	526.90	117.46	66.86	72.80	941.77	67.33	51.43
	PI	0.51	0.51	0.51	0.51	0.51	0.51	0.51	0.51	-0.39	0.85
	RAE	8.24	0.79	1.44	5.70	1.27	0.72	0.79	10.19	0.73	0.55
	d	0.02	0.38	0.37	0.04	0.34	0.62	0.58	0.13	0.48	0.90
	NSE	-1061.96	-1.04	-8.60	-147.30	-6.99	-0.25	-0.03	-82.47	-1.86	0.69
	CI	-21.77	-0.40	-3.17	-6.21	-2.37	-0.16	-0.02	-10.91	-0.89	0.62
	$\mathbf{R}^2$	0.21	0.18	0.24	0.001	0.04	0.22	0.08	0.08	0.30	0.58
	RMSE	634057.13	11631.18	3814.20	86063.96	3331.35	2874.61	3491.63	190431.23	2715.07	2108.27
	MAE	42067.93	1769.93	1379.35	11897.21	1267.98	950.54	1455.22	62288.78	987.23	783.95
Non- Dimensional	PI	0.52	0.52	0.52	0.52	0.52	0.52	0.52	0.52	0.52	0.52
Values	RAE	32.61	1.37	1.07	9.22	0.98	0.74	1.13	48.29	0.77	0.61
	d	0.01	0.34	0.65	0.00	0.32	0.55	0.47	0.02	0.66	0.85
	NSE	-38012.63	-11.79	-0.38	-699.37	-0.05	0.22	-0.15	-3427.93	0.30	0.58
	CI	-354.61	-4.00	-0.25	-2.83	-0.02	0.12	-0.07	-75.08	0.20	0.49

NSE = -5.19, and CI = -2.79 and for all of the data are  $R^2 = 0.41$ , RMSE=259.68, MAE=48.43, NSE = -0.84, and CI = -0.59 for the M1 which show the low accuracy in estimations by the ANFIS in comparison with the ANFIS-FFA. According to the results, comparing ANFIS with ANFIS-FFA, ANFIS-FFA in M1 has the highest accuracy. This result and the superiority of ANFIS-FFA versus ANFIS were approved by Azimi *et al.* [51] in calculating the roller length of a hydraulic jump on a rough channel bed. Also,

Yaseen *et al.*, [45] stated the ANFIS-FFA model shows higher accuracy in results over than the non-optimized ANFIS model in forecasting the streamflow. Therefore, new strengthen models such as ANFIS-FFA are capable of estimating  $K_x$  precisely and can be implemented in pollution modeling.

After all the aforementioned quantitative and graphical evaluations, the superiority of the hybridized ANFIS-FFA model in estimating of  $K_x$  is distinct and can combine with numerical pollutant modeling.

TABLE 9. Gaussian parameters for weights calculation in eq. 22, optimized by ANFIS-FFA, with an example calculation.

									Ou	tput MFs=ex	$p\left[-\left(\frac{\left(X_{i}-c_{j}\right)^{2}}{2\sigma_{j}^{2}}\right)\right]$	Pj=∏ $_{j=1}^4 OMf_j$	Relative Weight $w_j = \frac{P_j}{\Sigma^8 - P_j}$	
	B(I	m)	H()	n)	U(m	/s)	U*(n	1/s)						$\sum_{j=1}^{I} j$
mf <sub>i</sub>	Sigma	c	Sigma	c	Sigma	c	Sigma	с	B=53.3	H=2.09	U=0.79	U*=0.11	Pj	Wj
mfl	35.70	309.90	-1.48	-1.82	1.13	2.11	0.04	0.18	6.24E-12	3.05E-02	5.05E-01	1.43E-01	1.38E-14	4.14E-04
mf2	185.30	-808.90	6.62	-8.61	3.07	12.13	-0.06	-0.84	1.99E-05	2.71E-01	1.69E-04	3.31E-50	3.02E-59	9.08E-49
mf3	50.24	78.73	-0.01	0.34	-0.26	-1.57	0.11	0.35	8.80E-01	0.00E+00	1.29E-18	9.07E-02	0.00E+00	0.00E+00
mf4	-296.40	-211.50	-2.39	-24.60	0.90	0.95	0.00	0.52	6.71E-01	8.31E-28	9.84E-01	0.00E+00	0.00E+00	0.00E+00
mf5	90.50	-816.60	1.74	35.00	1.46	2.54	-0.15	-0.68	3.57E-16	2.09E-78	4.88E-01	4.66E-07	1.69E-100	5.09E-90
mf6	326.10	936.20	1.23	3.81	-0.13	-6.33	0.26	-1.17	2.56E-02	3.72E-01	0.00E+00	5.46E-06	0.00E+00	0.00E+00
mf7	-132.20	31.93	-1.36	-0.45	-0.42	2.17	-0.08	-0.36	9.87E-01	1.74E-01	4.53E-03	4.29E-08	3.32E-11	1.00E+00
mf8	-775.50	-2301.10	-0.20	4.85	0.11	<b>-</b> 6.64	0.00	-0.58	9.95E-03	9.56E-01	0.00E+00	0.00E+00	0.00E+00	0.00E+00
												Sum	3.33E-11	

 $\begin{array}{l} \text{Out.}\,\mathrm{mf}(B) = \mathrm{EXP}[-\left(\frac{(53.3-309.9)^2}{2(35.7^2)}\right)]^* = 6.24\mathrm{E} - 12;\\ \text{Out.}\,\mathrm{mf}(H) = \mathrm{EXP}[-\left(\frac{(0.79-2.11)^2}{2(-1.48^2)}\right)]^* = 3.05\mathrm{E} - 2;\\ \text{Out.}\,\mathrm{mf}(U) = \mathrm{EXP}[-\left(\frac{(0.79-2.11)^2}{2(1.13^2)}\right)]^* = 5.05\mathrm{E} - 1;\\ \text{Out.}\,\mathrm{mf}(U *) = \mathrm{EXP}[-\left(\frac{(0.11-0.18)^2}{2(0.04^2)}\right)]^* = 1.38\mathrm{E} - 14.24\mathrm{E} - 14.24\mathrm$ 

TABLE 10. Consequent parameters in the estimative equation of Kx by ANFIS-FFA, with an example calculation.

$\mathbf{mf}_{\mathbf{j}}$		(	Consequent Para	meters		Output Consequents	Weighted Output
	ai	b <sub>i</sub>	ci	di	r <sub>i</sub>		
$mf_1$	0.48	65.56	472.90	124.99	-329.20	0.48*53.3+65.56*2.09+472.90*0.79+124.99*0.11-329.20 = 221.09	9.15E-02
$mf_2$	5.51	-102.50	-478.90	306.31	463.30	197.59	1.79E-46
$mf_3$	6.62	100.83	1759.70	2997.03	495.60	2778.95	0.00E+00
$mf_4$	6.50	18.00	-286.20	2953.30	433.70	916.50	0.00E+00
$mf_5$	-6.63	62.90	-1686.40	2799.40	-246.92	-1491.56	-7.59E-87
$mf_6$	-6.63	-7.02	53.97	10.67	7.94	1276.14	0.00E+00
$mf_7$	0.38	-7.02	53.97	-10.67	7.94	54.61	5.46E+01
$mf_8$	2.98	-58.63	-1125.40	-2997.00	-495.60	-1677.51	0.00E+00
						Predicted Kx, Sum=54.68	

# C. EXPLICIT CALCULATION PROCEDURE OF Kx BY ANFIS-FFA OPTIMIZED PARAMETERS

As mentioned previously, the ANFIS model is a black box system that has not provided the algebraic form explicitly. Another novel contribution of this research is hybridizing the FFA procedure with ANFIS model in the explicit calculation of Kx, using an extended database. The ANFIS models can be used as a trained program with its optimized inherent parameter values. ANFIS usually is used in a subprogram that receives input vector and produces corresponding output rather than the algebraic form. However, the algebraic form of the best model (M1) in matrix format is provided. The algebraic form of ANFIS-FFA for Kx estimations based on the eq. 14 is derived:

$$K_x = \sum_{\substack{j=1\\ nmf=8\\ m_j^n f_j = \sum_{j=1}^{nmf=8} \left[ w_j^n \left( B \times a_j + H \times b_j + U \times c_j + U \times d_j + r_j \right) \right]$$
(22)

where a<sub>j</sub>, b<sub>j</sub>, c<sub>j</sub>, d<sub>j</sub> and r<sub>j</sub> are the optimized consequent parameters that are given in Table 9.  $\boldsymbol{w}_{j}^{n}$  is the normalized matrix of weights derived by the membership degree from Gaussian function parameters and provided in Table 10.

The normalized weights are calculated using equations 9-12, and they are used in equation 22 to calculate the Kx value.

The main focus of the current study is providing an explicit calculation procedure for Kx based on the optimized ANFIS that has not yet reported in the previous studies clearly. An example of calculation procedure is provided in Tables 9 and 10. In this example H=2.09m; B=53.3m; U=0.79m/s; U\* = 0.11m/s. The calculation steps for calculating the output of optimized ANFIS model for these values are as follows:

- 1- Use parameters of membership functions: The columns 2-9 in Table 9 give the s and c parameters of each membership function for each input parameter that are optimized and determined by FFA.
- 2- Calculate the output of membership functions: by using the optimized values of c and s in equation 10, the output of each membership function for every input parameter calculates, as the example calculations are provided bellow the Table 9. The output of each membership function in each parameter of B=53.3m; H=2.09 m; U=0.79 m/s; U\* =0.11 m/s is calculated in columns 10-13 in Table 9.
- 3- Calculate the product of membership function outputs by using Eq.11: by multiplying the output of each membership function the product value is calculated in column 14 in Table 9.
- 4- Calculate the relative weight of each membership function by using Eq.12: this is calculated by dividing each row in column 14 to the total sum of column 14 and the results are given in column 15 in Table 9.
- 5- Use the optimized consequent parameters of each membership function. These FFA based optimized values are provided in column 2-6 in Table 10.
- 6- Calculate the consequent outputs, the second part that are in parentheses in Eq.13; these values are calculated in column 7 in Table 10.

# TABLE 11. The raw data set used in ANFIS-FFA model development.

Kx(m2/s)	0.44	30.19	45.1	0.02	0.04	447.6	0.08	11	143.8	65	36.9	13.84	1490	8	143.8	0.01	6.8	41.8	11.48	0.04	111.5	0.12	0.07	12.93	288.5	24.38	0.03	5.9	0.06	0.33
U*(m/s)	0.02	0.04	0.07	0.03	0.07	0.06	0.04	0.12	0.03	0.18	0.11	0.06	0.08	0.06	0.07	0.04	0.24	0.12	0.05	0.04	0.1	0.07	0.01	0.07	0.08	0.04	0.02	0.04	0.07	0.02
U(m/s)	0.04	0.35	0.48	0.42	0.6	1.42	0.63	0.32	0.61	0.82	0.66	0.37	1.71	0.41	0.31	0.34	0.48	0.88	0.63	0.75	0.43	0.63	0.11	0.28	0.64	0.12	0.44	0.66	0.6	0.04
H(m)	1.77	0.55	0.81	0.1	0.1	16.76	0.12	0.48	1.6	2.5	2.4	0.41	3.05	0.75	4.82	0.09	0.6	1.1	2.82	0.07	2.33	0.15	2.62	0.86	4.85	0.21	0.07	1.6	0.1	1.77
W(m)	35	67.06	253.6	0.4	0.4	867	0.2	9.94	253.6	34.1	53.2	15.8	184	11.4	248.1	0.4	13	59.4	39.96	0.2	70.1	2.42	34.08	46.9	127.4	7.62	0.2	24.7	0.4	35
row	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180
Kx(m2/s)	0	0.07	0.15	6.97	140	3	90.0	0.06	5.92	162.6	26.8	32.51	18	53.3	1.26	0.09	14.7	0.05	0.04	11.2	223.8	131.3	0.02	0.02	501.4	0.02	40.2	19.52	12.48	20.9
U*(m/s)	0.03	0.01	0	0.04	0.03	0.02	0.06	0.04	0.04	0.17	0.05	0.08	0.1	0.07	0.11	0	0.03	0.04	0.03	0.11	0.04	0.05	0.03	0.07	0.04	0.02	0.07	0.08	0.03	0.05
U(m/s)	0.33	0.1	0.04	0.31	0.45	0.27	0.48	0.86	0.66	1.55	0.16	6£.0	0.83	0.68	0.77	0.05	0.23	0.75	0.58	6.83	0.24	0.58	0.5	0.57	0.41	0.36	0.4	0.21	0.41	0.46
H(m)	0.1	2.53	1.98	0.25	3.66	8.07	0.08	0.09	1.54	2.2	0.85	1.13	1.57	0.76	0.13	3.53	0.5	0.07	60.0	2.09	3.4	1.7	0.12	0.12	0.53	0.13	0.91	0.49	0.25	0.42
W(m)	0.4	30.36	27.74	12.5	152.4	48.8	0.4	0.2	24.99	68.6	28.44	65.53	25	59.44	0.6	30.36	12.2	0.2	0.2	53.3	232	116.4	0.2	0.4	46.02	1.1	36.6	15.9	12.34	50.9
row	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150
Kx(m2/s)	17.41	0.06	0.03	11.5	0.09	41.8	166.9	0.07	37.16	41.4	51.7	52	104.1	0.13	80.0	32.5	9.9	1486	13.94	29	38.62	0.06	40.5	20.9	54.7	32.52	145.5	30.19	0.09	39.48
$U^{*}(m/s)$	0.03	0.02	0.07	0.12	0.04	0.1	0.09	0.02	0.07	0.05	0.02	0.06	0.06	0.04	0.03	0.07	0.12	0.08	0.04	0.05	0.07	0.03	0.1	0.09	0.04	0.09	0.11	0.04	0.04	0.04
U(m/s)	0.41	0.47	0.57	0.62	0.75	0.62	0.52	0.42	0.44	0.16	0.17	0.69	0.13	0.68	0.7	0.34	0.16	1.55	0.29	0.64	0.34	0.58	0.75	0.43	0.1	0.45	0.79	0.35	0.75	0.21
H(m)	0.55	0.09	0.12	1.92	0.07	0.85	2.4	0.17	0.88	0.71	3.4	2.6	0.61	0.07	0.45	0.9	0.4	3.29	0.41	2	0.84	0.09	2.5	0.66	2.07	1.2	2.19	0.55	0.07	0.98
W(m)	30.66	0.2	0.4	20	0.2	16.27	91.9	2.42	47.55	92.96	259	85	21.06	0.4	0.0	25.9	19	182.9	19.8	120	25.9	0.2	57.9	11.89	37.49	19.5	53.3	67.1	0.2	35.1
row	91	92	93	94	95	96	76	98	66	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120

# TABLE 11. (Continued.) The raw data set used in ANFIS-FFA model development.

# TABLE 11. (Continued.) The raw data set used in ANFIS-FFA model development.

row	W(m)	H(m)	U(m/s)	U*(m/s)	Kx(m2/s)	row	W(m)	H(m)	U(m/s)	U*(m/s)	Kx(m2/s)	row	W(m)	H(m)	U(m/s)	U*(m/s)	Kx(m2/s)
181	0.2	0.09	0.86	0.04	0.06	211	12.8	0.3	0.42	0.06	17.5	241	29.9	0.4	0.34	0.02	44
182	300	0.4	0.97	0.03	183.4	212	35.05	0.98	0.21	0.04	39.48	242	0.4	0.12	0.54	0.06	0.05
183	0.2	0.06	0.51	0.03	0.04	213	201.2	3.56	1.27	0.08	836.1	243	53.34	2.09	0.46	0.11	46.45
184	17.5	0.5	0.32	0.02	5.8	214	36.6	0.49	0.32	0.05	13.94	244	0.2	0.12	0.63	0.04	0.07
185	27.57	2.04	0.21	0.03	0.24	215	31.39	1.43	0.13	0.04	24.2	245	1.5	0.14	0.33	0.1	1.9
186	85.95	2.93	1.2	0.53	153.3	216	40.53	0.41	0.43	0.05	11.53	246	0.2	0.13	0.5	0.03	0.03
187	40.54	0.41	0.23	0.04	66.5	217	59.7	0.42	0.15	0.08	2.41	247	18.29	1.22	0.11	0.01	1.31
188	0.6	0.13	0.31	0.06	0.15	218	537.4	8.9	1.51	0.1	341.1	248	30.18	2.1	0.59	0.07	12
189	1.1	0.09	0.21	0.03	0.05	219	26.52	1.83	0.03	0	0.06	249	0.2	0.09	0.86	0.04	0.07
190	34.08	0.53	0.38	0.04	162.9	220	15.85	0.41	0.37	0.06	13.94	250	64	0.8	0.67	0.27	34.8
191	0.4	0.05	0.41	0.02	0.02	221	127	8.3	1.07	0.05	15.7	251	24.08	0.98	0.59	0.1	101.5
192	103.4	1.9	0.61	0.04	57.65	222	16	0.49	0.26	0.08	15.5	252	31.11	1.8	0.02	0	0.06
193	0.2	0.14	0.52	0.03	0.02	223	6.1	0.49	0.25	0.06	69	253	21.3	0.9	0.36	0.04	24.2
194	59.4	2.43	0.86	0.1	203.9	224	20.4	0.61	0.52	0.08	24.55	254	75	1.6	0.22	0.99	11.8
195	19.4	1.1	0.05	0.05	9.3	225	28.7	0.6	0.35	0.07	10.7	255	0.4	0.13	0.54	0.06	0.01
196	259	3.3	0.17	0.02	50.9	226	537.4	8.9	1.51	0.1	374.1	256	65.5	1.13	0.39	0.08	32.52
197	9.36	0.61	0.39	0.13	10.35	227	11	0.29	0.35	0.06	2.7	257	0.2	0.09	0.86	0.04	0.04
198	0.4	0.08	0.44	0.06	0.04	228	35.2	0.31	0.17	0.04	4.29	258	36	0.58	0.21	0.05	8.1
199	0.4	0.12	0.54	0.06	0.02	229	0.2	0.12	0.63	0.04	0.07	259	34.14	2.46	0.82	0.18	65.03
200	187	6.3	0.37	0.03	12.2	230	0.2	0.09	0.58	0.03	0.04	260	152.4	3.7	0.45	0.06	227.6
201	1.1	0.07	0.27	0.01	0.01	231	19.81	0.58	0.24	0.02	6.5	261	161.5	3.96	0.29	0.02	13
202	42.98	1.28	0.26	0.07	45.1	232	34.08	2.62	0.08	0	0.14	262	42.37	0.8	0.42	0.07	30.19
203	76	1.2	1.41	0.06	115.7	233	19.8	0.42	0.43	0.07	14.15	263	11.28	0.29	0.34	0.06	2.82
204	36	0.58	0.3	0.05	8.08	234	0.4	0.14	0.73	0.08	0.03	264	30	1.1	0.38	0.03	8
205	12	0.3	0.33	0.05	1.32	235	50.29	1.37	0.67	0.07	80.34	265	36.8	0.9	0.13	0.05	15.5
206	0.2	0.06	0.51	0.03	0.03	236	102	4.4	0.17	0.01	50.5	266	0.4	0.05	0.96	0.04	0.06
207	500.8	5.14	1.02	0.08	922.1	237	5	0.28	0.26	0.21	7.2	267	155.1	1.7	0.47	0.04	177.7
208	0.4	0.06	0.64	0.03	0.03	238	0.2	0.09	0.58	0.03	0.05	268	20.92	0.89	0.4	0.08	57.56
209	37.19	0.91	0.42	0.03	24.3	239	35.66	0.32	0.1	0.04	350	269	12.95	0.3	0.16	0.1	12.75
210	0.4	0.11	0.62	0.07	0.06	240	20	0.4	0.19	0.18	6.5	270	36.1	0.34	0.21	0.04	4.65

| 25.9 $0.94$ $004$ $007$ $21.3$ $0.4$ $0.12$ $0.69$ $0.08$ $0.0$ $9$ $0.3$ $0.37$ $0.15$ $8.4$ $59.4$ $2.13$ $0.94$ $0.1$ $11.$ $24.4$ $1.56$ $0.71$ $0.04$ $17.$ $711.2$ $19.9$ $0.56$ $0.04$ $237$ $0.4$ $0.1$ $0.55$ $0.07$ $0.0$ $0.4$ $0.1$ $0.55$ $0.07$ $0.0$ $19.6$ $0.8$ $0.49$ $0.1$ $20.$ $19.5$ $0.8$ $0.13$ $0.04$ $12.$ | 2.5.9 $0.94$ $034$ $001$ $2.7.7$ $0.4$ $0.12$ $0.69$ $0.08$ $0.05$ $9$ $0.3$ $0.37$ $0.15$ $8.4$ $59.4$ $2.13$ $0.94$ $0.1$ $11.1$ $24.4$ $1.56$ $0.71$ $0.04$ $17.7$ $21.2$ $19.9$ $0.56$ $0.04$ $17.7$ $711.2$ $19.9$ $0.56$ $0.04$ $237.7$ $711.2$ $19.9$ $0.56$ $0.04$ $237.7$ $19.6$ $0.1$ $0.55$ $0.07$ $0.05$ $19.6$ $0.8$ $0.49$ $0.1$ $237.7$ $19.6$ $0.8$ $0.49$ $0.1$ $20.8$ $21.3$ $0.5$ $0.13$ $0.04$ $10.2$ $30.6$ $0.86$ $0.1$ $23.8$ $23.8$ $30.6$ $0.86$ $0.1$ $53.8$ $23.8$ $30.6$ $0.81$ $0.72$ $0.07$ <th>2.5.9 <math>0.94</math> <math>04</math> <math>012</math> <math>0.69</math> <math>0.01</math> <math>2.13</math> <math>9</math> <math>03</math> <math>0.37</math> <math>0.16</math> <math>0.08</math> <math>0.01</math> <math>59.4</math> <math>2.13</math> <math>0.94</math> <math>0.1</math> <math>11.1</math> <math>24.4</math> <math>1.56</math> <math>0.71</math> <math>0.04</math> <math>17.1</math> <math>24.4</math> <math>1.56</math> <math>0.71</math> <math>0.04</math> <math>17.1</math> <math>711.2</math> <math>19.9</math> <math>0.56</math> <math>0.04</math> <math>17.1</math> <math>0.4</math> <math>0.1</math> <math>0.55</math> <math>0.07</math> <math>0.01</math> <math>19.6</math> <math>0.8</math> <math>0.49</math> <math>0.1</math> <math>20.8</math> <math>19.6</math> <math>0.8</math> <math>0.79</math> <math>0.07</math> <math>20.8</math> <math>21.3</math> <math>0.5</math> <math>0.13</math> <math>0.04</math> <math>12.8</math> <math>21.3</math> <math>0.5</math> <math>0.13</math> <math>0.04</math> <math>12.8</math> <math>30.6</math> <math>0.86</math> <math>0.22</math> <math>0.06</math> <math>40.8</math> <math>59.4</math> <math>2.13</math> <math>0.86</math> 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| 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           336         711.2         199           337         0.4         0.1           338         19.6         0.1           339         21.3         0.5                         | 332     0.4     0.12       333     9     0.3       334     59.4     2.13       335     24.4     1.56       335     24.4     1.56       335     711.2     19.9       336     711.2     19.9       337     0.4     0.1       338     19.6     0.8       339     21.3     0.5       339     21.3     0.69       340     43.28     0.69       341     59.4     2.13       342     30.6     0.81       343     54.6     2.45   
   
   | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         711.2         19.9           337         0.4         0.1           338         19.6         0.8           339         21.3         0.5           339         21.3         0.5           339         21.3         0.5           340         43.28         0.69           341         59.4         2.13           342         30.6         0.81           343         54.6         2.49           343         54.6         2.49           343         54.6         2.49           345         10.8         0.4 | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.51           335         24.4         1.99           335         24.4         1.90           335         24.4         1.90           335         24.4         0.1           337         0.4         0.1           337         0.4         0.1           339         19.6         0.8           339         21.3         0.5           339         21.3         0.5           340         43.28         0.69           341         59.4         2.13           342         30.6         0.81           343         54.6         2.49           344         7.6         3.45           345         10.8         0.4           345         10.8         0.56           346         25         0.56           347         37.8         1.89 | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         0.1           337         0.4         0.1           338         19.6         0.8           339         21.3         0.5           340         43.28         0.69           341         59.4         2.13           342         30.6         0.81           343         54.6         2.49           344         7.6         3.45           345         10.8         0.4           345         10.8         0.4           345         25         0.56           347         37.8         1.86           348         0.4         0.14           348         0.4         0.1           349         20.7         1.35 | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.51           335         24.4         1.51           335         24.4         1.99           335         24.4         1.96           335         24.4         0.1           333         19.6         0.8           333         19.6         0.8           334         21.3         0.5           339         21.3         0.69           340         43.28         0.69           341         59.4         2.13           342         30.6         0.81           343         54.6         2.49           344         7.6         3.45           345         10.8         0.4           345         25         0.56           346         25         0.56           347         37.8         1.89           349         20.4         0.14           349         20.2         1.35           349 | 332         0.4         0.12           333         9         0.3           334         59.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           337         0.4         0.1           333         19.6         0.8           333         19.6         0.8           333         19.6         0.8           334         21.3         0.5           340         43.28         0.69           341         59.4         2.13           342         30.6         0.81           343         7.6         0.81           344         7.6         3.45           345         10.8         0.4           345         10.8         0.4           346         2.55         0.56           347         37.8         1.89           348         0.4         0.14           349         20.27         1.35           350  
  | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         21.12         19.9           333         19.6         0.8           333         19.6         0.8           333         21.3         0.5           334         21.3         0.5           334         21.3         0.6           341         59.4         2.13           341         59.4         2.13           342         30.6         0.81           344         7.6         3.45           345         10.8         0.4           345         37.8         1.89           346         25         0.56           346         25         0.56           347         37.8         1.89           348         0.4         0.1           349         20.   
  | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         54.4         1.56           335         24.4         1.56           335         24.4         1.56           335         711.2         19.9           335         711.2         19.9           335         21.3         0.1           333         19.6         0.1           333         19.6         0.1           333         21.3         0.5           334         19.6         0.8           334         21.3         0.5           341         59.4         2.13           342         30.6         0.81           344         7.6         2.49           345         10.8         0.6           345         30.6         0.81           345         7.6         2.13           345         2.6         0.56           345         37.8         1.89           345         37.8         1.89           346         2.1         3.45           347   | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         19.6         0.8           333         19.6         0.8           333         19.6         0.8           333         19.6         0.8           334         19.6         0.8           334         21.3        
0.5           340         21.3         0.5           341         59.4         2.13           342         30.6         0.8           343         54.6         2.49           344         7.6         3.45           345         2.6         0.6           346         2.7         1.89           346         2.7         1.89           346         2.7         1.89           346         2.7         1.89           347         37.8 </td <td>332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.51           335         24.4         1.51           335         24.4         1.51           335         24.4         1.51           335         21.1.2         19.9           337         0.4         0.1           333         19.6         0.8           333         19.6         0.8           334         21.3         0.5           340         43.28         0.69           341         59.4         2.13           342         30.6         0.81           344         7.6         3.45           344         7.6         3.45           345         10.8         0.4           346         255         0.56           347         37.8         1.89           346         20.4         0.14           347         37.8         1.89           346         20.5         0.56           347         &lt;</td> <td>332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         54.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         21.3         0.5           339         19.6         0.8           333         19.6         0.8           333         21.3         0.5           334         19.6         0.8           339         21.3         0.5           340         43.28         0.6           341         59.4         2.13           342         30.6         0.8           344         7.6         3.45           345         26.7         0.6           346         25         0.6           347         37.8         1.89           348         0.4         0.1           349         20.7         1.36           348         0.4         0.1           350         31.13<!--</td--><td>332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         711.2         19.9           335         711.2         19.9           337         0.4         0.1           338         19.6         0.8           339         21.3         0.5           339         21.3         0.5           339         21.3         0.6           340         43.28         0.69           341         59.4         2.13           342         30.6         0.81           343         54.6         2.49           344         7.6         3.45           345         30.6         0.81           346         25         0.66           346         25         0.67           346         25         0.61           346         25         0.66           346         25         0.66           357         17.6&lt;</td><td>332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.51           335         24.4         1.51           335         24.4         1.51           335         24.4         1.56           337         0.4         0.1           333         19.6         0.8           333         19.6         0.8           333         19.6         0.8           333         19.6         0.8           333         21.3         0.5           340         21.3         0.5           341         59.4         2.13           342         30.6         0.8           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           345         3.46         0.46           346         2.10<!--</td--></td></td>  | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.51           335         24.4         1.51           335         24.4         1.51           335         24.4         1.51           335         21.1.2         19.9           337         0.4         0.1           333         19.6         0.8           333         19.6         0.8           334         21.3         0.5           340         43.28         0.69           341         59.4         2.13           342         30.6         0.81           344         7.6         3.45           344         7.6         3.45           345         10.8         0.4           346         255         0.56           347         37.8         1.89           346         20.4         0.14           347         37.8         1.89           346         20.5         0.56           347         <   
                               | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         54.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         21.3         0.5           339         19.6         0.8           333         19.6         0.8           333         21.3         0.5           334         19.6         0.8           339         21.3         0.5           340         43.28         0.6           341         59.4         2.13           342         30.6         0.8           344         7.6         3.45           345         26.7         0.6           346         25         0.6           347         37.8         1.89           348         0.4         0.1           349         20.7         1.36           348         0.4         0.1           350         31.13 </td <td>332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         711.2         19.9           335         711.2         19.9           337         0.4         0.1           338         19.6         0.8           339         21.3         0.5           339         21.3         0.5           339         21.3         0.6           340         43.28         0.69           341         59.4         2.13           342         30.6         0.81           343         54.6         2.49           344         7.6         3.45           345         30.6         0.81           346         25         0.66           346         25         0.67           346         25         0.61           346         25         0.66           346         25         0.66           357         17.6&lt;</td> <td>332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.51           335         24.4         1.51           335         24.4         1.51           335         24.4         1.56           337         0.4         0.1           333         19.6         0.8           333         19.6         0.8           333         19.6         0.8           333         19.6         0.8           333         21.3         0.5           340         21.3         0.5           341         59.4         2.13           342         30.6         0.8           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           345         3.46         0.46           346         2.10<!--</td--></td>                | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.56           335         24.4         1.56           335         711.2         19.9           335         711.2         19.9           337         0.4         0.1           338         19.6         0.8           339         21.3         0.5           339         21.3         0.5           339         21.3         0.6           340         43.28         0.69           341         59.4         2.13           342         30.6         0.81           343         54.6         2.49           344         7.6         3.45           345         30.6         0.81           346         25         0.66           346         25         0.67           346         25         0.61           346         25         0.66           346         25         0.66           357         17.6<   | 332         0.4         0.12           333         9         0.3           334         59.4         2.13           335         24.4         1.56           335         24.4         1.51           335         24.4         1.51           335         24.4         1.51           335         24.4         1.56           337         0.4         0.1           333         19.6         0.8           333         19.6         0.8           333         19.6         0.8           333         19.6         0.8           333         21.3         0.5           340         21.3         0.5           341         59.4         2.13           342         30.6         0.8           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           344         7.6         3.45           345         3.46         0.46           346         2.10 </td   |
| 0.04         333         9           0.06         334         59.4           14.14         335         24.4           0.03         336         711.2           0.03         337         0.4           194         333         21.3   | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.5         342         30.6           100.7         343         54.6   
   
   | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.2         343         54.6           100.2         343         7.6           100.2         345         10.8   | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         24.4           0.03         336         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           190.2         343         54.6           100.2         343         7.6           100.2         343         7.6           169.5         346         25           33.8         346         25           346         25         54.6           668.9         347         37.8                         | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         3356         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         333         19.6           194         333         19.6           194         333         19.6           195         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         7.6           100.2         343         7.6           100.2         345         10.8           169.5         345         37.8           15.1         348         0.4           15.1         348         0.4           15.1         349         20.7                      | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         54.6           100.2         343         7.6           100.2         344         7.6           169.5         346         255           668.9         347         37.8           15.1         348         0.4           15.1         349         202.7           37.16         34.9         202.7                                | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         335         711.2           308.9         335         711.2           308.9         335         711.2           308.9         335         71.6           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         54.6           100.2         343         7.6           100.2         343         7.6           169.5         345         10.8           33.8         346         25           668.9         347         37.8           15.1         348         0.4           37.16         37.1         37.8   
  | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         19.6           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         54.6           100.2         343         54.6           100.2         343         7.6           169.5         343         7.6           169.5         344         7.6           169.5         343         7.6           15.1         348         0.4           37.16         349         20.7           37.16         349         20.7           3  
  | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         7.6           100.2         344         7.6           100.2         344         7.6           169.5         344         7.6           15.1         346         2.7           169.5         344         7.6           15.1         348         0.4           15.1         348         0.4           15.1         348         0.6           15.1 <td>0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         54.6           100.2         343         7.6           100.2         343         7.6           169.5         344         7.6           15.1         348         0.4           37.16         349         20.7           37.16         349         20.7           37.16         349         20.7           15.1         348         0.4           1</td> <td>0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         54.6           100.2         343         54.6           100.2         344         7.6           169.5         347         7.8           15.1         348         0.4           15.1         348         0.4           15.1         348         0.4           15.1         348         0.4           15.1         349         20.7           15.1&lt;</td> <td>0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         7.6           100.2         343         7.6           100.2         344         7.6           100.2         344         7.6           100.2         344         7.6           15.1         346         2.5           169.5         347         37.8           15.1         348         0.4           15.1         348         0.6           15.1         347         37.8           15.1<!--</td--><td>0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           194         338         19.6           195.9         341         59.4           193.9         341         59.4           193.9         341         54.6           193.9         341         59.4           100.2         341         59.4           32.53         345         10.8           100.2         344         7.6           100.2         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15</td><td>0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         711.2           308.9         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         54.6           100.2         343         7.6           100.2         344         7.6           100.2         344         7.6           15.1         346         25.7           33.8         346         25.7           15.1         348         0.4           15.1         348         0.4           15.1         346         25.7           15.1         347         37.8           15.</td></td> | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9        
341         59.4           193.9         341         59.4           100.2         343         54.6           100.2         343         7.6           100.2         343         7.6           169.5         344         7.6           15.1         348         0.4           37.16         349         20.7           37.16         349         20.7           37.16         349         20.7           15.1         348         0.4           1  | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         54.6           100.2         343         54.6           100.2         344         7.6           169.5         347         7.8           15.1         348         0.4           15.1         348         0.4           15.1         348         0.4           15.1         348         0.4           15.1         349         20.7           15.1<   
                              | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         7.6           100.2         343         7.6           100.2         344         7.6           100.2         344         7.6           100.2         344         7.6           15.1         346         2.5           169.5         347         37.8           15.1         348         0.4           15.1         348         0.6           15.1         347         37.8           15.1 </td <td>0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           194         338         19.6           195.9         341         59.4           193.9         341         59.4           193.9         341         54.6           193.9         341         59.4           100.2         341         59.4           32.53         345         10.8           100.2         344         7.6           100.2         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15</td> <td>0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         711.2           308.9         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         54.6           100.2         343         7.6           100.2         344         7.6           100.2         344         7.6           15.1         346         25.7           33.8         346         25.7           15.1         348         0.4           15.1         348         0.4           15.1         346         25.7           15.1         347         37.8           15.</td> | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         24.4           0.03         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           194         338         19.6           195.9         341         59.4           193.9         341         59.4           193.9         341         54.6           193.9         341         59.4           100.2         341         59.4           32.53         345         10.8           100.2         344         7.6           100.2         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15.1         347         37.8           15  | 0.04         333         9           0.06         334         59.4           14.14         335         24.4           14.14         335         711.2           308.9         336         711.2           308.9         337         0.4           194         335         711.2           308.9         337         0.4           194         338         19.6           5.5         339         21.3           99.89         340         43.28           193.9         341         59.4           193.9         341         59.4           193.9         341         59.4           100.2         343         54.6           100.2         343         7.6           100.2         344         7.6           100.2         344         7.6           15.1         346         25.7           33.8         346         25.7           15.1         348         0.4           15.1         348         0.4           15.1         346         25.7           15.1         347         37.8           15.   |
| 0.06         334         59           14.14         335         24           0.03         336         71           308.9         337         0           308.9         337         0           194         338         15           5.5         339         21   | 0.06         334         59           14.14         335         24           14.14         335         24           0.03         336         71           308.9         337         0           308.9         337         0           308.9         337         0           194         338         15           5.5         339         21           99.89         340         43           193.9         341         55           32.52         342         36           100.7         343         54   
   
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| 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339  | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         92.89         340           09         193.9         341           09         193.9         341           07         32.52         342           03         100.2         343   
   
   | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         5.5         339           09         5.5         339           09         9.89         340           09         193.9         341           09         193.9         341           07         32.52         342           03         100.2         343           06         0.02         344           03         100.2         343           03         100.2         343  | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         5.5         339           09         99.89         340           09         193.9         341           07         32.52         342           07         32.52         343           07         32.52         343           07         32.52         343           08         0.02         343           03         100.2         343           06         33.8         346           08         6.68.9         347  | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         5.5         339           09         5.5         339           09         5.5         339           09         5.5         339           09         5.5         340           09         193.9         341           07         32.52         342           07         32.52         343           07         32.52         345           08         100.2         345           08         169.5         345           08         15.1         348           07         33.8         346           08         15.1         348           07         37.16         349   | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         5.5         339           09         194         338           09         193.9         341           07         32.52         342           07         32.52         343           07         32.52         343           07         32.52         343           07         32.52         343           03         100.2         343           06         0.02         344           07         32.52         343           08         169.5         345           08         668.9         346           08         15.1         348           07         37.16         349           07         37.16         349           07         37.16         349   | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         194         338           09         99.89         340           09         193.9         341           07         32.52         342           03         100.2         343           03         100.2         343           06         33.8         346           08         668.9         347           08         169.5         345           07         33.8         346           08         169.5         347           08         668.9         347           07         37.16         349           07         37.16         349           07         37.16         349           07         37.16         349           07         37.16         349           07         37.16         349 <tr td="">         349      <tr td=""></tr></tr>  
  | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         5.5         339           09         99.89         340           09         193.9         341           07         32.52         343           07         32.52         343           07         32.52         343           07         32.52         343           08         190.2         344           07         32.52         343           08         190.2         345           08         0.02         344           03         169.5         345           08         66.9         347           08         15.1         348           07         37.16         349           07         37.16         349           07         37.16         349           07         37.16         349           07         0.06         3  
  | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         5.5         339           09         9.89         340           09         5.5         349           07         32.52         343           07         32.52         343           07         32.52         343           07         32.52         345           08         190.2         345           08         169.5         345           08         15.1         348           07         37.16         348           07         37.16         349           07         37.16         349           07         37.16         349           07         37.16         348           07         37.16         349           07         37.16         348           07         0.02         351           07         0.02         351   | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         5.5         339           09         99.89         340           09         193.9         341           07         32.52         343           07         32.52         343           07         32.52         343           07         32.52         343           08         190.2         343          
07         32.52         343           08         100.2         343           08         0.02         344           03         169.5         345           08         169.5         346           08         15.1         348           07         37.16         349           07         37.16         349           07         37.16         349           07         37.16         349           07         0.02   | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           08         99.89         341           09         193.9         341           07         5.5         339           08         99.89         340           09         193.9         341           07         32.52         343           07         32.52         343           07         32.52         343           07         32.52         343           08         100.2         344           03         100.2         343           06         33.8         346           08         15.1         348           07         37.16         349           07         37.16         349           07         37.16         349           07         37.16         350           07         0.02         351           07         0.02         352           08         59.3   
                             | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         5.5         339           09         5.5         339           09         5.5         339           09         5.5         339           09         5.5         340           07         32.52         343           07         32.52         343           07         32.52         343           08         190.2         343           03         100.2         343           03         169.5         346           03         169.5         346           03         169.5         345           04         0.02         351           05         14.81         350           06         37.16         351           07         37.16         351           07         0.02         352           05         14.7         353   | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         5.5         339           09         95.89         340           07         5.5         349           07         5.5         343           07         32.52         343           07         32.52         343           07         32.52         343           07         32.52         343           08         190.2         343           03         169.5         343           03         169.5         346           03         169.5         345           03         169.5         345           04         9.0         37.16         349           05         14.181         350           06         37.16         351           07         37.16         354           07         0.02         355           05         14.  | 07         14.14         335           03         0.03         336           05         308.9         337           04         194         338           09         5.5         339           09         5.5         339           09         5.5         339           09         194         338           09         193.9         341           07         5.5         349           08         99.89         340           09         193.9         341           07         32.52         343           08         190.2         343           07         32.52         343           08         190.2         344           07         32.52         343           08         169.5         344           03         160.2         344           03         169.5         345           04         0.02         346           05         37.16         349           07         37.16         349           07         0.02         357           08         59.3         356<   |
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| 0.03         0.03           0.05         308.9           0.04         194           0.09         5.5   | 0.03         0.03         0.03           0.05         308.9         308.9           0.04         194         5.5           0.09         5.5         99.89           0.09         193.9         90.09           0.09         193.9         193.9           0.07         32.52         0.03           0.03         100.2         100.2  
   
   | 0.03         0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.08         99.89           0.09         5.5           0.09         5.5           0.09         5.5           0.09         33.52           0.07         32.52           0.03         109.2           0.06         0.02           0.03         100.2   | 0.03         0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         193.9           0.07         32.52           0.03         193.9           0.04         193.9           0.05         193.9           0.06         193.9           0.07         32.52           0.03         100.2           0.04         0.02           0.05         33.8           0.06         33.8           0.08         668.9  | 0.03         0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         193.9           0.07         32.52           0.03         100.2           0.04         193.9           0.05         100.2           0.06         33.8           0.07         32.52           0.06         33.8           0.07         32.53           0.06         33.8           0.08         169.5           0.08         668.9           0.08         15.1           0.07         37.16   | 0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.08         99.89           0.09         5.5           0.09         193.9           0.07         32.52           0.03         190.2           0.04         193.9           0.05         100.2           0.06         33.8           0.06         33.8           0.06         33.8           0.06         33.8           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16   | 0.03         0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.08         99.89           0.09         5.5           0.09         5.5           0.09         5.5           0.09         193.9           0.07         32.52           0.03         190.2           0.04         193.9           0.05         193.9           0.06         33.8           0.07         32.52           0.08         169.5           0.08         668.9           0.08         15.1           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.04         0.06  
  | 0.03         0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         193.9           0.07         32.52           0.03         100.2           0.03         100.2           0.04         32.8           0.05         33.8           0.06         33.8           0.07         37.16           0.08         668.9           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         0.02           0.07         0.02           0.07         0.02           0.07         0.02           0.07         0.02 <td>0.03         0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.55           0.07         32.52           0.03         193.9           0.04         193.9           0.05         33.52           0.06         193.9           0.07         32.52           0.03         100.2           0.04         0.02           0.05         169.5           0.08         15.1           0.08         15.1           0.07         37.16           0.08         15.1           0.07         37.16           0.12         11.81           0.04         0.06           0.05         14.7           0.05         14.7           0.05         14.7</td> <td>0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         193.9           0.07         32.52           0.03         100.2           0.04         32.52           0.05         100.2           0.06         33.8           0.07         32.52           0.08         668.9           0.08         668.9           0.08         668.9           0.08         15.1           0.08         668.9           0.08         668.9           0.08         15.1           0.07         37.16           0.08         14.7           0.07         0.02           0.05         14.7           0.05         14.7           0.05         16.66           0.05        
16.66</td> <td>0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.55           0.09         193.9           0.07         32.52           0.03         193.9           0.04         32.52           0.05         193.9           0.06         193.9           0.07         32.52           0.06         100.2           0.07         32.52           0.08         169.5           0.08         15.1           0.08         15.1           0.08         15.1           0.07         37.16           0.08         15.1           0.07         37.16           0.12         41.81           0.07         37.16           0.07         37.16           0.07         37.16           0.07         0.02           0.07         0.02           0.07         0.02</td> <td>0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         193.9           0.01         32.52           0.02         193.9           0.03         100.2           0.04         33.55           0.05         100.2           0.06         33.8           0.08         15.1           0.08         15.1           0.08         15.1           0.07         37.16           0.08         15.1           0.04         0.06           0.05         14.7           0.05         14.7           0.06         3.8           0.08         59.3           0.08         0.63           0.08         0.63</td> <td>0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         193.9           0.03         193.9           0.04         193.5           0.05         190.2           0.06         33.8           0.07         32.52           0.08         668.9           0.08         668.9           0.08         668.9           0.08         169.5           0.08         668.9           0.08         14.1           0.04         0.06           0.05         14.7           0.05         14.7           0.05         14.7           0.05         14.66           0.05         14.7           0.05         16.66           0.06         8.8           0.06         8.8           0.07&lt;</td> <td>0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.08         99.89           0.09         5.55           0.03         193.9           0.04         32.52           0.05         193.9           0.06         193.9           0.07         32.52           0.03         100.2           0.04         0.02           0.05         169.5           0.06         33.8           0.07         37.16           0.08         15.1           0.08         15.1           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         0.02           0.07         0.02           0.08         59.3           0.06         8.8           0.07         0.05           <td< td=""></td<></td> | 0.03         0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.55           0.07         32.52           0.03         193.9           0.04         193.9           0.05         33.52           0.06         193.9           0.07         32.52           0.03         100.2           0.04         0.02           0.05         169.5           0.08         15.1           0.08         15.1           0.07         37.16           0.08         15.1           0.07         37.16           0.12         11.81           0.04         0.06           0.05         14.7           0.05         14.7           0.05         14.7  | 0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         193.9           0.07         32.52           0.03         100.2           0.04         32.52           0.05         100.2           0.06         33.8           0.07         32.52           0.08         668.9           0.08         668.9          
0.08         668.9           0.08         15.1           0.08         668.9           0.08         668.9           0.08         15.1           0.07         37.16           0.08         14.7           0.07         0.02           0.05         14.7           0.05         14.7           0.05         16.66           0.05         16.66   | 0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.55           0.09         193.9           0.07         32.52           0.03         193.9           0.04         32.52           0.05         193.9           0.06         193.9           0.07         32.52           0.06         100.2           0.07         32.52           0.08         169.5           0.08         15.1           0.08         15.1           0.08         15.1           0.07         37.16           0.08         15.1           0.07         37.16           0.12         41.81           0.07         37.16           0.07         37.16           0.07         37.16           0.07         0.02           0.07         0.02           0.07         0.02   
                                 | 0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         193.9           0.01         32.52           0.02         193.9           0.03         100.2           0.04         33.55           0.05         100.2           0.06         33.8           0.08         15.1           0.08         15.1           0.08         15.1           0.07         37.16           0.08         15.1           0.04         0.06           0.05         14.7           0.05         14.7           0.06         3.8           0.08         59.3           0.08         0.63           0.08         0.63  | 0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         193.9           0.03         193.9           0.04         193.5           0.05         190.2           0.06         33.8           0.07         32.52           0.08         668.9           0.08         668.9           0.08         668.9           0.08         169.5           0.08         668.9           0.08         14.1           0.04         0.06           0.05         14.7           0.05         14.7           0.05         14.7           0.05         14.66           0.05         14.7           0.05         16.66           0.06         8.8           0.06         8.8           0.07<  | 0.03         0.03           0.05         308.9           0.04         194           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.09         5.5           0.08         99.89           0.09         5.55           0.03         193.9           0.04         32.52           0.05         193.9           0.06         193.9           0.07         32.52           0.03         100.2           0.04         0.02           0.05         169.5           0.06         33.8           0.07         37.16           0.08         15.1           0.08         15.1           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         37.16           0.07         0.02           0.07         0.02           0.08         59.3           0.06         8.8           0.07         0.05 <td< td=""></td<>   |
| 0.02         0.05           1.06         0.05           0.54         0.04           0.46         0.09  | 0.05         0.05           1.06         0.05           0.54         0.04           0.46         0.09           0.78         0.08           0.43         0.09           0.34         0.07           0.46         0.09   
   
   | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$   
  | 0.54 $0.05$ $1.06$ $0.05$ $0.46$ $0.09$ $0.78$ $0.09$ $0.73$ $0.09$ $0.44$ $0.07$ $0.44$ $0.03$ $0.41$ $0.03$ $0.44$ $0.03$ $0.44$ $0.03$ $0.44$ $0.03$ $0.44$ $0.03$ $0.44$ $0.03$ $0.44$ $0.03$ $0.74$ $0.03$ $0.74$ $0.03$ $0.74$ $0.03$ $0.74$ $0.03$ $0.74$ $0.03$ $0.74$ $0.03$ $0.74$ $0.03$ $0.74$ $0.03$ $0.74$ $0.012$ $0.78$ $0.012$ $0.78$ $0.012$ $0.78$ $0.012$ $0.78$ $0.012$ $0.78$ $0.012$ $0.78$ $0.012$ $0.78$ $0.012$ $0.78$ $0.012$ $0.78$ $0.012$ $0.78$ $0.012$ $0.74$ $0.052$  
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| 2.32         1.06           0.67         0.54           0.83         0.46  | 2.32     1.06       2.67     0.54       2.83     0.46       2.34     0.78       2.34     0.78       0.76     0.45       0.79     0.46   
   
   | 2.32     1.06       5.67     0.54       5.83     0.46       5.34     0.78       2.34     0.43       0.76     0.43       0.79     0.46       0.13     0.46       0.13     0.46       0.13     0.41       2.19     0.41   | 2.32     1.06       5.67     0.54       0.83     0.46       2.34     0.78       2.34     0.78       0.76     0.43       0.79     0.46       0.79     0.46       0.13     0.41       1.1     0.32       1.1     0.32       4.75     0.64   | 2.32     1.06       5.67     0.54       0.83     0.46       2.34     0.78       0.756     0.43       0.79     0.46       0.13     0.46       0.13     0.44       0.13     0.41       0.13     0.41       0.13     0.46       0.13     0.46       0.13     0.41       0.13     0.41       0.13     0.41       0.13     0.41       0.13     0.41       0.13     0.41       0.5     0.27       0.5     0.27       0.87     0.44   | 2.32     1.06       5.67     0.54       5.83     0.46       5.34     0.78       5.34     0.73       5.79     0.46       0.13     0.46       0.13     0.41       1.1     0.32       1.1     0.32       4.75     0.64       0.5     0.27       0.5     0.27       0.87     0.41       1.1     0.32       1.1     0.32       1.1     0.32       0.5     0.64       0.5     0.64       1.1     0.88       1.1     0.88  | 2.32     1.06       5.67     0.54       5.83     0.46       5.34     0.78       5.34     0.78       5.34     0.34       0.79     0.46       0.13     0.46       0.13     0.46       0.13     0.44       0.13     0.41       0.13     0.41       0.13     0.41       0.13     0.41       0.11     0.32       0.5     0.64       0.5     0.64       0.75     0.64       0.87     0.41       1.1     0.32       0.87     0.64       0.91     0.64   
  | .5.32         1.06           .167         0.54           .183         0.46           .183         0.46           .234         0.78           .244         0.34           .194         0.34           .194         0.34           .195         0.46           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.36           .12         0.44           .11         0.32           .12         0.44           .13         0.44           .14         0.44           .15         0.44           .16         0.44           .17         0.44           .18         0.44           .19         0.44           .10         0.44 <td>2.32     1.06       5.67     0.54       5.83     0.46       2.34     0.78       2.34     0.73       3.75     0.46       3.79     0.46       3.13     0.44       3.13     0.44       3.13     0.44       3.13     0.44       3.13     0.44       3.13     0.44       3.13     0.41       3.13     0.41       3.13     0.41       3.13     0.41       3.11     0.32       0.5     0.64       0.5     0.64       1.1     0.32       3.87     0.44       1.1     0.86       0.11     0.86       0.11     0.86       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.53     0.33</td> <td>.3.2         1.06           .167         0.54           .183         0.46           .183         0.46           .234         0.78           .24         0.34           .176         0.46           .179         0.46           .194         0.34           .195         0.46           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.32           0.55         0.64           0.57         0.64           0.57         0.64           0.57         0.64           0.57         0.64           0.57         0.64           0.57         0.64           0.53         0.64           0.11         0.88           0.12         0.68           0.12         0.64           0.13         0.64           0.13         0.64           0.13         0.63           0.63         0.63           0.63         0.63</td> <td>2.32     1.06       5.67     0.54       5.83     0.46       2.34     0.78       2.34     0.73       0.79     0.46       0.13     0.44      
0.13     0.41       0.13     0.41       0.13     0.41       0.13     0.41       0.13     0.41       0.13     0.41       1.1     0.32       0.5     0.27       0.5     0.41       1.1     0.32       0.86     0.44       1.1     0.88       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.53       0.53     0.53       0.53     0.53       0.53     0.53       0.53     0.53</td> <td></td> <td>.5.32         1.06           .167         0.54           .183         0.46           .234         0.78           .234         0.78           .246         0.34           .79         0.46           .179         0.46           .179         0.44           .179         0.41           .11         0.32           .111         0.32           .111         0.32           .111         0.32           .111         0.32           0.55         0.64           0.57         0.64           0.53         0.64           0.55         0.64           0.55         0.64           0.12         0.86           0.12         0.86           0.12         0.58           0.12         0.63           0.12         0.63           0.12         0.63           0.13         0.63           0.13         0.53           0.13         0.63           0.13         0.63           0.13         0.63           0.13         0.63           0.13<td>2.32<math>1.06</math><math>5.7</math><math>0.54</math><math>1.83</math><math>0.46</math><math>2.34</math><math>0.78</math><math>2.76</math><math>0.43</math><math>2.79</math><math>0.46</math><math>1.13</math><math>0.44</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.11</math><math>0.32</math><math>0.09</math><math>0.86</math><math>0.12</math><math>0.63</math><math>0.12</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.64</math><math>0.19</math><math>0.46</math></td></td>  | 2.32     1.06       5.67     0.54       5.83     0.46       2.34     0.78       2.34     0.73       3.75     0.46       3.79     0.46       3.13     0.44       3.13     0.44       3.13     0.44       3.13     0.44       3.13     0.44       3.13     0.44       3.13     0.41       3.13     0.41       3.13     0.41       3.13     0.41       3.11     0.32       0.5     0.64       0.5     0.64       1.1     0.32       3.87     0.44       1.1     0.86       0.11     0.86       0.11     0.86       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.53     0.33   | .3.2         1.06           .167         0.54           .183         0.46           .183         0.46           .234         0.78           .24         0.34           .176         0.46           .179         0.46           .194         0.34           .195         0.46           .11         0.32           .11         0.32           .11         0.32           .11         0.32           .11         0.32           0.55         0.64           0.57         0.64           0.57         0.64           0.57         0.64           0.57      
  0.64           0.57         0.64           0.57         0.64           0.53         0.64           0.11         0.88           0.12         0.68           0.12         0.64           0.13         0.64           0.13         0.64           0.13         0.63           0.63         0.63           0.63         0.63  | 2.32     1.06       5.67     0.54       5.83     0.46       2.34     0.78       2.34     0.73       0.79     0.46       0.13     0.44       0.13     0.41       0.13     0.41       0.13     0.41       0.13     0.41       0.13     0.41       0.13     0.41       1.1     0.32       0.5     0.27       0.5     0.41       1.1     0.32       0.86     0.44       1.1     0.88       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.58       0.12     0.53       0.53     0.53       0.53     0.53       0.53     0.53       0.53     0.53   
                             |  | .5.32         1.06           .167         0.54           .183         0.46           .234         0.78           .234         0.78           .246         0.34           .79         0.46           .179         0.46           .179         0.44           .179         0.41           .11         0.32           .111         0.32           .111         0.32           .111         0.32           .111         0.32           0.55         0.64           0.57         0.64           0.53         0.64           0.55         0.64           0.55         0.64           0.12         0.86           0.12         0.86           0.12         0.58           0.12         0.63           0.12         0.63           0.12         0.63           0.13         0.63           0.13         0.53           0.13         0.63           0.13         0.63           0.13         0.63           0.13         0.63           0.13 <td>2.32<math>1.06</math><math>5.7</math><math>0.54</math><math>1.83</math><math>0.46</math><math>2.34</math><math>0.78</math><math>2.76</math><math>0.43</math><math>2.79</math><math>0.46</math><math>1.13</math><math>0.44</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.19</math><math>0.41</math><math>2.11</math><math>0.32</math><math>0.09</math><math>0.86</math><math>0.12</math><math>0.63</math><math>0.12</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.63</math><math>0.13</math><math>0.64</math><math>0.19</math><math>0.46</math></td>  | 2.32 $1.06$ $5.7$ $0.54$ $1.83$ $0.46$ $2.34$ $0.78$ $2.76$ $0.43$ $2.79$ $0.46$ $1.13$ $0.44$ $2.19$ $0.41$ $2.19$ $0.41$ $2.19$ $0.41$ $2.19$ $0.41$ $2.19$ $0.41$ $2.19$ $0.41$ $2.19$ $0.41$ $2.19$ $0.41$ $2.19$ $0.41$ $2.11$ $0.32$ $0.09$ $0.86$ $0.12$ $0.63$ $0.12$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.63$ $0.13$ $0.64$ $0.19$ $0.46$  |
| 5.63 0.67<br>9.9 0.83  | .63         0.67           0.9         0.83           9.4         2.34           2.9         0.76           5.91         0.94           1.49         0.79   
   
   | .63         0.67           0.9         0.83           9.4         2.34           2.9         0.76           5.91         0.94           0.49         0.79           0.49         0.79           1.49         0.13   | .63         0.67           0.9         0.83           9.4         2.34           2.9         0.76           5.91         0.94           5.91         0.94           0.49         0.79           0.49         0.79           1.49         0.79           0.4         0.13           0.4         0.13           0.4         0.13           0.4         0.13           0.4         0.13           0.4         0.13           7.5         1.1           7.5         1.1   | (63         0.67           19         0.83           9.4         2.34           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           1.1         2.19           1.5         2.19           1.5         2.19           7.5         1.1           7.5         0.5           5.8         0.5           5.8         0.5  | .63         0.67           19         0.83           9.4         2.34           2.9         0.76           2.9         0.76           3.91         0.94           2.9         0.76           1.1         2.19           7.5         1.1           7.5         1.1           7.5         1.1           7.5         0.87           7.5         0.87           7.5         0.87           7.5         0.87           7.5         0.87           7.5         0.87           7.5         0.87           7.5         0.87   | .63         0.67           19         0.83           9.4         2.34           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           1.1         2.19           1.1.5         2.19           1.1.5         2.19           7.5         1.1           7.5         0.87           7.5         0.87           7.5         0.87           7.5         0.87           0.2         0.09  
  | .63         0.67           19         0.83           9.4         2.34           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           1.5         2.19           7.5         1.1           7.5         1.1           7.5         0.87           7.5         0.87           7.5         0.87           7.5         0.87           7.5         0.87           7.5         0.13           0.4         0.12           0.4         0.12           0.4         0.12           0.4         0.12  
  | (63         0.67           (9         0.83           9.4         2.34           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           1.5         2.19           7.5         1.1           7.5         1.1           7.5         0.87           7.5         0.87           0.74         1.1           0.2         0.09           0.4         0.13           1.1         7.5           0.44         1.1           0.2         0.09           0.4         0.12           0.4         0.12           0.4         0.12           0.4         0.12           0.3         0.63   | (63         0.67           19         0.83           9.4         2.34           2.9         0.76           5.91         0.94           5.91         0.94           5.91         0.94           1.49         0.79           1.5         2.19           7.5         1.1           7.5         0.87           7.5         0.87           7.44         1.1           7.5         0.87           0.5         0.5           5.8         0.5           7.5         0.87           0.44         1.1           0.2         0.09           0.44         1.1        
  0.2         0.09           0.44         1.13           0.2         0.09           0.4         0.12           8.29         0.63           8.29         0.63           8.29         0.63   | (63         0.67           (9         0.83           9.4         2.34           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           1.5         2.19           7.5         1.1           7.5         0.87           7.5         0.87           7.5         0.87           0.4         1.1           0.2         0.09           0.4         1.1           0.2         0.09           0.4         1.1           0.2         0.63           8.29         0.63           8.29         0.63           43         1.23           0.6         0.13  
                            | (63         0.67           (9         0.83           9.4         2.34           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           1.1         2.19           7.5         1.1           7.5         0.87           7.5         0.87           0.4         1.1           0.2         0.09           0.4         1.1           0.2         0.09           0.4         1.1           0.2         0.09           0.4         0.12           0.4         0.12           0.4         0.12           1.23         1.23           0.6         0.13           0.6         0.13   | (63         0.67           (9         0.83           9.4         2.34           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.1         0.79           1.5         2.19           7.5         1.1           7.5         0.87           7.5         0.87           7.5         0.12           7.4         4.75           5.8         0.5           7.4         1.1           7.5         0.09           0.4         1.1           0.2         0.03           0.4         0.12           3.2         1.23           8.29         0.63           43         1.23           0.2         0.13           0.2         0.7           0.2         0.7           0.4         0.09   | (63         0.67           (9         0.83           9.4         2.34           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           2.9         0.76           1.5         2.19           7.5         1.1           7.5         0.87           7.5         0.87           0.4         1.1           0.2         0.09           0.4         1.1           0.2         0.06           0.4         1.1           0.2         0.63           8.29         0.63           8.29         0.63           0.2         0.13           0.4         0.03           0.4         0.04           0.5         0.7  |
| 0.0 <u>0.0</u>   | 70.0         70.0           10         9.9           11         12.9           312         25.91           313         31.49  
   
   | count         count           009         9.9           110         79.4           111         12.9           112         25.91           113         31.49           114         0.4           115         211.5   | Count         Count           009         9.9           110         79.4           111         12.9           112         25.91           113         31.49           114         0.4           115         211.5           116         97.5           117         127.4  | Count         Count           100         79.4           111         79.4           111         12.9           111         12.9           111         25.91           112         25.91           113         31.49           114         0.4           115         211.5           116         97.5           117         127.4           118         15.8           118         15.8           151         47.5  | Construct         Construct           100         79.4           111         12.9           111         12.9           111         12.9           111         25.91           113         31.49           114         0.4           115         211.5           116         97.5           117         127.4           118         15.8           119         47.5           119         47.5           119         59.44   | Constraint         Constraint           10         79.4           111         12.9           111         12.9           111         12.9           111         25.91           113         31.49           114         0.4           115         211.5           116         97.5           117         127.4           118         15.8           119         47.5           119         64.5           119         97.5           110         97.5           111         127.4           112         127.4           113         15.8           119         47.5           120         59.44           121         0.2           121         0.2   
  | Construct         Construct           100         79.4           111         12.9           111         12.9           111         12.9           111         25.91           1113         31.49           114         0.4           115         211.5           116         97.5           117         127.4           118         15.8           119         127.4           117         127.4           118         15.8           119         47.5           120         59.44           10.2         53.1           110         127.4           112         127.4           118         15.8           119         27.5           110         0.2           112         0.4           112         0.4           112         0.4           112         0.4           112         0.4           112         0.4           112         0.4           113         0.4   
  | Constraint         Constraint           10         79.4           111         12.9           111         12.9           111         12.9           112         25.91           113         31.49           114         0.4           115         211.5           116         97.5           117         127.4           118         15.8           119         127.4           118         15.8           119         127.4           121         127.4           121         127.4           123         0.4           123         0.2           123         0.2           123         0.4           123         17.37           17.37         17.37   | Construct         Construct           110         79.4           111         12.9           112         25.91           113         31.49           114         0.4           115         2511.5           116         97.5           117         127.4           118         15.8           1519         47.5           320         59.44           321         0.2           321         0.2           321         0.2           322         0.4           323         17.37           324         18.29           325         43                      
   | Construct         Construct           100         79.4           111         12.9           111         12.9           111         12.9           112         25.91           113         31.49           114         0.4           115         211.5           116         97.5           117         127.4           118         15.8           119         47.5           120         59.44           121         127.4           123         10.2           124         127.4           127.4         127.4           128         15.8           117.37         127.4           123         17.37           123         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37   
                            | Constraint         Constraint           110         79.4           111         12.9           111         12.9           112         25.91           113         31.49           114         0.4           115         211.5           117         127.4           118         15.8           119         127.4           118         15.8           119         127.4           118         15.8           119         127.4           121         127.4           1318         15.8           149         0.4           150         59.44           161         0.2           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           132         17.37           132         17.37           132         17.37           132         17.37           132         17.37           132         17.37           132         17.37           132         17.37 <td< td=""><td>Constraint         Constraint           110         79.4           111         12.9           111         12.9           112         25.91           113         31.49           114         0.4           115         211.5           117         127.4           118         15.8           119         47.5           121         0.2           321         0.2           321         0.2           321         0.2           321         0.2           323         17.37           324         18.29           325         0.4           325         0.4           326         0.6           327         40.2           328         0.4</td><td>2000         2000           100         79.4           111         12.9           111         12.9           111         12.9           111         12.9           112         25.91           113         31.49           114         0.4           115         211.5           116         97.5           117         127.4           118         15.8           119         47.5           119         47.5           119         47.5           121         127.4           119         127.4           121         127.4           119         127.4           110         0.2           117.37         127.4           110         0.4           121         0.4           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37&lt;</td></td<>   | Constraint         Constraint           110         79.4           111         12.9           111         12.9           112         25.91           113         31.49           114         0.4           115         211.5           117         127.4           118         15.8           119         47.5           121         0.2           321         0.2           321         0.2           321         0.2           321         0.2           323         17.37           324         18.29           325         0.4           325         0.4           326         0.6           327         40.2           328         0.4  | 2000         2000           100         79.4           111         12.9           111         12.9           111         12.9           111         12.9           112         25.91           113         31.49           114         0.4           115         211.5           116         97.5           117         127.4           118         15.8           119         47.5           119         47.5           119         47.5           121         127.4           119         127.4           121         127.4           119         127.4           110         0.2           117.37         127.4           110         0.4           121         0.4           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37         17.37           17.37<   |
| 56 309   | 56         309           07         310           0.3         311           .13         312           .13         312           .07         313   
   
   | 56         309           07         310           0.3         311           0.3         312           0.3         312           0.3         312           0.2         313           0.9         314           0.9         314           0.7         313           0.8         314   | 56         309           07         310           03         311           03         313           13         312           02         313           09         314           09         314           07         315           07         315           99         314           99         314           91         315           92         316   | 56         309           07         310           03         311           1.13         312           1.13         312           02         313           99         314           07         315           99         314           99         314           99         314           91         315           92         314           93         314           93         314           93         314           93         315           94         317           93         318           93         318           93         318   | 56         309           07         310           .13         311           .13         312           .02         313           .03         314           .04         315           .05         313           .09         314           .09         315           .09         315           .09         316           .01         315           .02         316           .03         316           .04         317           .05         319           .06         318           .07         318           .08         317   | 56         309           07         310           1.3         311           1.3         312           02         313           99         314           99         314           99         314           99         315           99         314           99         314           91         315           92         316           93         314           91         315           91         315           92         319           93         318           93         318           94         317           95         319           95         319           93         319           93         319           94         317           95         320           96         321           97         321  
  | 56         309           07         310           1.3         311           .13         312           .13         313           02         313           99         314           99         314           99         314           99         314           99         314           99         315           99         316           99         316           91         315           92         319           93         316           94         317           94         317           95         319           95         319           95         319           91         319           92         319           93         320           93         321           19         322           19         323   
  | 56         309           07         310           1.3         311           1.3         312           02         313           99         314           99         314           99         314           99         314           99         314           99         314           91         315           92         314           93         314           94         317           91         318           92         318           93         318           93         318           94         317           95         318           95         320           93         320           94         321           95         320           96         321           97         323           1.9         323           1.1         324  | 56         309           07         310           03         311           13         312           13         313           99         314           99         314           99         314           99         315           99         314           99         314           91         315           92         316           93         314           94         321           19         323           19         322           19         323           19         321           94         325  
   | 56         309           07         310           13         311           13         312           13         313           99         314           99         314           99         314           99         314           99         314           99         315           99         315           91         315           92         314           93         314           94         317           99         320           91         320           93         320           94         325           94         325           94         325   
                            | 56         309           07         310           1.13         311           1.13         312           02         313           99         314           07         315           99         314           07         315           99         314           99         314           07         315           99         314           99         314           91         315           92         318           93         318           94         317           93         318           94         317           95         318           95         320           91         322           1.1         324           1.1         324           94         325           94         325           94         326           94         325           94         326           94         326           94         326           94         326           94         326 <td>56         309           07         310           03         311           13         312           02         313           99         314           07         315           07         313           13         312           13         313           13         314           13         315           14         315           15         314           16         315           94         317           95         319           95         319           95         318           96         318           97         318           98         320           99         321           91         322           19         323           19         324           94         325           97         326           97         326           97         327           97         326           97         327           97         326           97         327</td> <td>56         309           07         310           1.3         311           1.3         312           1.3         313           99         314           99         314           99         315           99         314           99         315           99         315           91         315           92         314           93         314           94         317           95         320           96         321           97         323           93         321           94         325           94         325           94         325           94         325           94         325           97         326           97         328           97         328           97         328           97         328           97         328           97         328           97         328           97         328           97         328</td>   | 56         309           07         310           03         311           13         312           02         313           99         314           07         315           07         313           13         312           13         313           13         314           13         315           14         315           15         314           16         315           94         317           95         319           95         319           95         318           96         318           97         318           98         320           99         321           91         322           19         323           19         324           94         325           97         326           97         326           97         327           97         326           97         327           97         326           97         327  | 56         309           07         310           1.3         311           1.3         312           1.3         313           99         314           99         314           99         315           99         314           99         315           99         315           91         315           92         314           93         314           94         317           95         320           96         321           97         323           93         321           94         325           94         325           94         325           94         325           94         325           97         326           97         328           97         328           97         328           97         328           97         328           97         328           97         328           97         328           97         328  |
|  | 03 0.07<br>08 10.3<br>06 18.13<br>03 0.02   
   
   | 03         0.07           08         10.3           06         18.13           03         0.02           03         0.02           03         0.02           03         0.02           03         0.02  | 03         0.07           08         10.3           06         18.13           03         0.02           52         1799           03         0.07           03         0.07           66         98.22           08         13.94  | 03         0.07           08         10.3           06         18.13           05         0.02           03         0.02           03         0.02           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           06         98.22           08         13.94           03         0.05   | 03         0.07           08         10.3           06         18.13           05         0.02           03         0.02           03         0.02           03         0.07           03         0.07           03         0.07           03         0.07           06         98.22           08         13.94           08         13.94           03         0.05           03         0.05           03         0.05           03         0.05           03         0.05           03         0.05   | 03         0.07           08         10.3           06         18.13           05         18.13           03         0.02           52         1799           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.05           03         0.05           03         0.05           03         0.05           03         0.05           03         0.05           03         0.05           03         0.05           03         0.05           03         0.05           04         0.05  
  | 03         0.07           08         10.3           06         18.13           05         18.13           03         0.02           55         1799           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           04         98.22           05         239           05         239           05         315.9           07         0.05           07         10.9           08         10.9           07         10.9           08         891.9           05         37.8           05         37.8   
  | 03         0.07           08         10.3           06         18.13           05         18.13           06         18.13           07         0.02           03         0.02           03         0.02           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.05           03         0.05           03         0.05           03         0.05           04         91.9           05         37.8           05         37.8           05         37.8           05         37.8           05         37.8           05         37.8           06         0.1   | 03         0.07           08         10.3           06         18.13           05         18.13           05         18.13           05         18.13           05         98.22           06         98.22           08         13.94           55         2.9           07         0.05           08         13.94           55         2.9           07         0.05           08         13.94           07         0.05           08         10.9           07         10.9           08         891.9           07         0.1           08        
13.94           08         10.9           08         891.9           08         891.9           08         10.9           08         13.94           08         13.94  | 03         0.07           08         10.3           06         18.13           05         18.13           03         0.02           55         1799           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           04         98.22           05         315.9           05         315.9           05         315.9           05         315.9           06         891.9           07         0.1           08         13.94           08         13.94           08         19.9           08         19.9           08         19.9           08         19.9           08         19.9           08         13.94           08         13.94           08         13.94           08         13.94           08         13.94           08         13.94  
                            | 03         0.07           08         10.3           06         18.13           05         18.13           05         98.22           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           04         98.22           05         2.9           05         2.9           07         0.05           07         0.05           07         0.05           08         10.9           08         10.9           08         10.9           08         10.9           08         10.9           08         13.94           08         13.94           08         24.6           08         24.6           08         0.07  | 03         0.07           08         10.3           06         18.13           05         18.13           05         98.25           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           04         13.94           05         2.9           07         0.05           03         0.05           04         13.94           05         2.9           06         98.23           07         0.05           08         10.9           08         10.9           08         13.94           08         10.9           08         13.94           08         13.94           08         10.1           08         13.94           08         13.94           08         13.94           08         13.94           08         10.1           08         10.7 <td< td=""><td>03         0.07           08         10.3           06         18.13           05         18.13           03         0.02           52         1799           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           04         98.22           05         315.9           05         315.9           05         315.9           06         891.9           07         0.05           08         13.94           07         0.05           08         10.9           08         13.94           08         13.94           08         19.9           08         19.9           08         13.94           08         13.94           08         13.94           08         13.94           08         13.94           08         13.94           08         10.7           08         10.7           08         10.7</td></td<>   | 03         0.07           08         10.3           06         18.13           05         18.13           03         0.02           52         1799           03         0.07           03         0.07           03         0.07           03         0.07           03         0.07           04         98.22           05         315.9           05         315.9           05         315.9           06         891.9           07         0.05           08         13.94           07         0.05           08         10.9           08         13.94           08         13.94           08         19.9           08         19.9           08         13.94           08         13.94           08         13.94           08         13.94           08         13.94           08         13.94           08         10.7           08         10.7           08         10.7   |
| 0.03   | ).27         0.08           0.58         0.06           0.46         0.03   
   
   | ).27         0.08           ).58         0.06           0.46         0.03           1.25         0.52           0.22         0.03   | ).27         0.08           .58         0.06           .146         0.03           1.25         0.52           0.22         0.03           1         0.06           0.37         0.08   | ).27     0.08       ).58     0.06       ).46     0.03       1.25     0.52       3.22     0.03       1     0.06       0.37     0.08       1.29     0.55       0.37     0.08       0.5     0.55  | ).27         0.08           ).58         0.06           ).46         0.03           1.25         0.52           0.22         0.03           1         0.06           0.37         0.08           0.57         0.03           0.57         0.03           0.57         0.03           0.57         0.03           0.57         0.03           0.57         0.03           0.57         0.03           0.57         0.03           0.55         0.03           0.58         0.05  | ).27     0.08       ).58     0.06       ).46     0.03       1.25     0.52       ).22     0.03       1     0.06       0.37     0.08       0.57     0.03       0.58     0.05       0.58     0.05       0.58     0.05       0.58     0.05       0.59     0.05       0.11     0.02       0.52     0.05   
  | ).27         0.08           ).58         0.06           ).46         0.03           1.25         0.52           1.27         0.03           1.29         0.06           0.37         0.08           0.57         0.03           1         0.06           1         0.06           0.37         0.08           0.55         0.03           0.58         0.05           0.11         0.02           0.11         0.02           0.56         0.05           0.26         0.05  
  | ).27         0.08           ).58         0.06           ).46         0.03           1.25         0.52           1         0.06           ).37         0.08           1         0.06           0.37         0.03           1         0.06           0.37         0.08           0.57         0.05           0.58         0.05           0.11         0.02           0.53         0.08           0.11         0.02           0.26         0.05           0.26         0.06           0.26         0.05           0.26         0.05           0.26         0.05           0.26         0.05           0.26         0.05  | ).27         0.08           ).58         0.06           ).46         0.03           1.25         0.52           ).22         0.03           1         0.06           0.37         0.08           0.37         0.08           0.37         0.03           0.55         0.05           0.55         0.03           0.58         0.05           0.11         0.02           0.11         0.02           0.11         0.02           0.126         0.05           0.11         0.02           0.05         0.05           0.13         0.08           0.26   
     0.05           0.06         0.01           0.06         0.01           0.075         0.08   | ).27         0.08           ).58         0.06           ).46         0.03           1.25         0.52           ).22         0.03           1.29         0.05           0.5         0.03           1.1         0.06           0.55         0.03           0.57         0.08           0.57         0.08           0.57         0.08           0.58         0.05           0.56         0.05           0.11         0.02           0.153         0.08           0.153         0.08           0.153         0.08           0.153         0.08           0.153         0.08           0.153         0.08           0.337         0.08           0.337         0.08           0.337         0.08           0.34         0.08  
                            | ).27         0.08           ).58         0.06           ).46         0.03           1.25         0.52           1.25         0.06           ).37         0.08           1.1         0.06           0.37         0.03           1.29         0.05           0.55         0.55           0.55         0.03           0.55         0.03           0.11         0.02           0.11         0.02           0.11         0.05           0.15         0.06           0.11         0.02           0.157         0.08           0.26         0.05           0.276         0.06           0.24         0.08           0.24         0.03           0.24         0.03   | ).27         0.08           ).58         0.06           ).46         0.03           1.25         0.52           ).22         0.03           129         0.05           0.57         0.03           0.57         0.03           1         0.06           0.57         0.03           0.57         0.03           0.57         0.03           0.58         0.03           0.59         0.03           0.11         0.02           0.11         0.02           0.11         0.02           0.126         0.01           0.11         0.02           0.11         0.03           0.24         0.03           0.24         0.03           0.19         0.05           0.19         0.05           0.19         0.05           0.19         0.05   | ).27         0.08           ).58         0.06           ).46         0.03           1.25         0.52           ).22         0.03           1.2         0.08           ).37         0.08           ).37         0.08           ).37         0.08           ).37         0.08           ).37         0.08           0.55         0.03           0.56         0.05           0.11         0.02           0.26         0.05           0.37         0.08           0.37         0.08           0.37         0.08           0.15         0.06           0.15         0.08           0.26         0.01           0.37         0.08           0.37         0.08           0.37         0.08           0.19         0.05           0.19         0.05           0.19         0.05           0.19         0.03           0.19         0.03  |
| 0.14 0.  | 0.0 0.0<br>2.93 0.<br>0.09 0.   
   
   | 0.6         0.           2.93         0.           2.93         0.           0.09         0.           2.82         1.           0.18         0.  | 0.0         0.0         0.           2.93         0.         0.           0.09         0.         0.           2.82         1.         0.           0.18         0.         0.           0.81         0.         0.   | 0.0         0.0           2.93         0.           2.93         0.           0.09         0.           0.18         0.           0.18         0.           0.18         0.           0.81         0.           0.93         0.           0.18         0.           0.18         0.           0.91         0.           0.12         0.  | 0.0         0.0         0.           2.93         0.         0.           0.09         0.         0.           0.18         0.         0.           0.18         0.         0.           0.18         0.         0.           0.18         0.         0.           0.12         0.         1.           0.312         0.         0.           0.912         0.         0.           0.12         0.         0.           0.12         0.         0.           0.12         0.         0.  | 0.0         0.0         0.0           2.93         0.         0.0           0.09         0.         0.           0.18         0.         0.           0.18         0.         0.           0.18         0.         0.           0.127         0.         0.           0.99         1.         0.           0.12         0.         1.           0.12         0         0.           0.12         0         2.04           0.12         0         2.14           0.12         0.         1.   
  | 0.0         0.0         0.           2.93         0.         0.           0.09         0.         0.           0.18         0.         0.           0.18         0.         1.           0.18         0.         1.           0.19         1.         0.           0.931         0.         1.           0.12         0.         1.           0.12         0.         1.           0.12         0.         1.           0.12         0.         1.           3.11         1.         1.           0.557         0.         0.  
  | $\begin{array}{cccccc} 0.0 & 0. \\ 0.0 & 0. \\ 2.93 & 0. \\ 0.08 & 0. \\ 0.18 & 0. \\ 0.18 & 0. \\ 0.18 & 0. \\ 0.11 & 0. \\ 0.9 & 11. \\ 0.12 & 0 & 0 \\ 0.12 & 0 & 0 \\ 2.04 & 0. \\ 5.7 & 0. \\ 5.7 & 0. \\ 0.55 & 0. \\ 1.1 & 1. \\ 1. \\ 0. \\ 0.55 & 0. \\ 1.1 & 0. \\ 0.55 & 0. \\ 0. \\ 1.1 & 0. \\ 0. \\ 1.1 & 0. \\ 0. \\ 0.55 & 0. \\ 0. \\ 0. \\ 0.55 & 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0.$   | $\begin{array}{c ccccc} 0.0 & 0. \\ 0.0 & 0. \\ 2.93 & 0. \\ 0.09 & 0. \\ 0.18 & 0. \\ 0.18 & 0. \\ 0.217 & 0. \\ 0.81 & 0. \\ 0.12 & 0 \\ 0.12 & 0 \\ 0.12 & 0 \\ 0.12 & 0 \\ 0.12 & 0 \\ 0.11 & 1. \\ 0. \\ 0.55 & 0. \\ 0. \\ 0.81 & 0. \\ 0. \\ 0.81 & 0 \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. \\ 0. $   
   | $\begin{array}{cccccc} 0.0 & 0.0 & 0.\\ 2.93 & 0.\\ 0.09 & 0.\\ 2.82 & 1.\\ 0.18 & 0.\\ 0.18 & 0.\\ 0.81 & 0.\\ 0.12 & 0 & 0\\ 0.12 & 0 & 1.\\ 0.12 & 0 & 1.\\ 0.12 & 0 & 0\\ 1.1 & 1.\\ 0.\\ 0.55 &
0.\\ 0.55 & 0.\\ 0.55 & 0.\\$ | $\begin{array}{ccccc} 0.0 & 0.0 & 0.\\ 2.93 & 0.\\ 0.09 & 0.\\ 2.82 & 1.\\ 2.82 & 1.\\ 0.18 & 0.\\ 0.81 & 0.\\ 0.9 & 1.\\ 0.9 & 1.\\ 0.91 & 0.\\ 3.11 & 1.\\ 1.\\ 1.71 & 0.\\ 0.55$  | $\begin{array}{cccccc} 0.0 & 0. & 0. \\ 2.93 & 0. \\ 0.09 & 0. \\ 2.82 & 1. \\ 2.82 & 1. \\ 2.27 & 0. \\ 0.81 & 0. \\ 0.12 & 0 & 1. \\ 0.12 & 0 & 1. \\ 0.12 & 0 & 1. \\ 0.12 & 0 & 0 \\ 2.04 & 0 & 1. \\ 0.12 & 0 & 0 \\ 0.55 & 0 & 0 \\ 0.55 & 0 & 0 \\ 0.03 & $ | $\begin{array}{cccccc} 0.0 & 0. & 0. \\ 2.93 & 0. \\ 0.09 & 0. \\ 2.82 & 1. \\ 0.18 & 0. \\ 0.81 & 0. \\ 0.9 & 1. \\ 0.9 & 1. \\ 0.12 & 0 & 1. \\ 0.12 & 0 & 1. \\ 0.12 & 0 & 0 \\ 1.71 & 0 & 0. \\ 3.11 & 1. \\ 1.71 & 0 & 0. \\ 0.55 & 0 & 0. \\ 0.55 & 0 & 0. \\ 0.55 & 0 & 0. \\ 0.78 & 0 & 0. \\ 0.06 & 0 & 0. \\ 0.00 & 0.0 & 0. \\ 0$ |
| 0.2 (  | 14.9<br>41.33<br>0.2<br>(12)  
   
   | 14.9         14.9           41.33         2           0.2         0           85.95         2           1.1         0   | 14.9         14.9           41.33         2           0.2         0.2           0.2         0.2           1.1         0           1.1         0           153.6         2           13.41         0   | 14.9         14.9           41.33         2           0.2         0.2           85.95         2           1.1         0           1.1         0           1.1         0           1.1         0           1.1         0           1.1         0           1.1         0           1.1         0           1.1         0           1.1         0           1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0  | 14.9           41.33         2           41.33         2           0.2         0.2           85.95         2           1.1         0           1.1         0           13.41         0           13.41         0           0.2         0.2           13.41         0           0.2         0.2           0.2         0.2  | 14.9         14.9           41.33         2           0.2         0.2           85.95         2           1.1         0           1.1         0           1.1         0           1.1         0           1.1         0           1.1         0           1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.3.5         2           1.1.4         0           1.1.5         0.2           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1         0           1.1.1  
  | 14.9         14.9           41.33         2           0.2         0.2           10.2         1.1           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.1         0           11.3.7         0           11.3.7         0           11.3.5         1           11.3.6         1           11.3.6         1           11.3.6         1           11.3.6         1           11.3.6         1           11.3.6         1           11.3.6         1           11.3.6         1  
  | 14.9           14.9           0.2           0.2           0.2           0.2           0.2           0.2           0.2           0.2           0.2           0.2           0.2           0.2           0.2           0.2           0.2           1.1   | 14.9         14.9           -0.2         0.2         0.2           0.2         0.2         0.2           1.1         1         1         1           1.1         1         1         1         1           1.1         1         1         1         1         1           1.1         1       
 1           | 14.9         14.9           0.2         0.2         0.2           0.2         0.2         0.2         0.2           1.1.1         0         1.1         0           1.1.1         0         1.1         0           1.1.1         0         1.1         0           1.1.1         0         1.1         0           1.1.1         0         1.1         0           1.1.1         0         1.1         0           1.1.3.7         0.2         0         0.2           0.2         0.2         0         0.2         0           1.1.3.7         1.1.1         0         1.1.1         0           1.1.3.4         0.2         0.2         0         1.1.1           1.1.3.5         1.1.1         1.1.1         1.1.1         1.1.1           1.1.1         0.2         0.2         0.2         0.2         1.1.1           1.1.3.4         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1         1.1.1   
                            | 14.9         14.9           -0.2         0.2         0           -0.2         0.2         0           -0.2         1.1         0         1.1           -0.1         1.1         0         1.1         0           -0.2         1.1         0         1.1         0         1.1           -0.2         1.1         1         1.1         0         1.1         1.1         0           -0.2         1.1         1.1         1.1         0         1.1   | 14.9         14.9           0.2         0.2         0.2           0.2         0.2         0.2         0.2           11.1         1         1         1         1           13.41         0         13.41         0         13.41           13.77         13.41         0         1.3         1           13.47         0.2         0.2         0         1           13.56         1         13.54         0         1           15.36         1         15.36         1         1           15.36         1         15.36         1         1           15.36         1         15.36         1         1           15.36         1         15.36         1         1           15.35         15.33         0         0         4         0   | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   |
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# TABLE 11. (Continued.) The raw data set used in ANFIS-FFA model development.

(s)

# TABLE 11. (Continued.) The raw data set used in ANFIS-FFA model development.

Kx(m2/s)	25.9	33.9	41.81	0.1	79.6	260.1	12.73	43.14	20.13	36.89	11.5	0.07	0.08	71.7	6.5	471.7	0.02	14.8	9.29	0.06	0.05	0.5	4.65	38	0.08	22.46	3.1	0.15	50.78	0.03
U*(m/s)	0.08	0.04	0.11	0.04	0.04	0.13	0.02	0.04	0.03	0.04	0.05	0.04	0.04	0.04	0.06	0.06	0.02	0.07	0.05	0.03	0.03	0.05	0.04	0.05	0.03	0.06	0.02	0.04	0.03	0.06
U(m/s)	0.41	0.91	88.0	98.0	99.0	0.77	0.31	0.56	0.32	0.54	0.56	98.0	0.75	0.18	0.31	1.49	0.47	0.21	0.43	6.65	5.0	0.36	0.21	90.0	0.24	0.13	0.27	96.0	0.42	0.48
H(m)	0.45	L	96.0	60.0	0.65	3.84	0.73	17.51	0.24	0.58	2.61	0.09	0.07	4.6	1.58	16.76	0.09	1.2	0.3	0.06	0.12	1.08	0.32	0.44	0.14	0.21	1.43	0.05	2.13	0.08
W(m)	24.99	120	67.1	0.2	51.2	71.63	29.26	701	14.02	28.65	48.34	0.2	0.2	202	21.77	867	0.2	48.5	32.6	0.4	0.2	29.61	35.1	15.13	1.1	9.14	19.2	0.4	100.3	0.4
row	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450
Kx(m2/s)	234.7	13.5	10.3	24.4	0.19	6.77	464.6	13.94	20.7	139.7	9.85	155.9	1.7	29.3	0.27	55.74	10.94	260.1	1.08	88.9	25.55	23.54	271.1	10.3	22	668.9	1.4	92.9	0.52	6.12
U*(m/s)	0.07	0.3	0.01	0.16	0.01	0.02	0.15	0.14	0.12	0.06	0.12	0.09	0.01	0.08	0.01	0.11	0.04	0.13	0.12	0.14	0.08	0.06	0.03	0.09	0.09	0.08	0.01	0.07	0.02	0.16
U(m/s)	0.41	0.55	0.44	0.47	0.05	0.24	1.74	1.01	0.15	1.34	0.14	1.08	0.13	0.15	0.05	0.67	0.29	0.76	0.53	0.74	0.52	0.23	1	0.07	0.32	0.64	0.11	0.39	0.2	0.77
H(m)	0.77	0.63	1.1	0.2	1.89	0.52	2.4	0.58	0.4	16.76	0.39	3.5	2.5	0.41	2.26	2.13	0.41	3.8	0.13	2	0.71	0.69	0.3	1.04	1	4.75	2.5	1.35	0.67	0.13
W(m)	37.06	10	27	167	37.8	20.42	85.3	24.99	18.3	867	18.6	230	34	49.68	45.11	59.44	10.8	71.6	0.6	75.6	24.38	42.21	300	41.45	63	127.4	35	202.7	16.31	9.0
row	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420
Kx(m2/s)	0.21	217.9	46.45	20.9	27	243	0.02	0.05	8.85	88.13	11	29.6	0.02	39.48	177.7	166.9	36.93	0.04	9.5	3.36	21	9.1	0.05	0.06	0.03	0.11	21.4	290.4	15	13.94
U*(m/s)	0.02	0.06	0.11	0.05	0.08	0.09	0	0.04	0.04	0.08	0.09	0.04	0.04	0.07	0.04	0.11	0.1	0.07	0.06	0.06	0.1	0.1	0.03	0.05	0.05	0.05	0.1	0.03	0.08	0.05
U(m/s)	0.07	1.04	0.46	0.46	0.73	0.27	0.02	0.63	0.22	0.38	0.84	0.62	0.32	0.4	0.47	0.3	0.69	0.6	0.15	0.35	0.6	0.19	0.67	0.91	0.45	0.83	0.52	1.42	0.24	0.37
H(m)	2.19	2.3	2.1	0.52	1.21	0.41	2.87	0.12	0.41	0.67	1.84	0.65	0.09	0.92	1.74	2.5	2.26	0.1	0.85	0.29	0.85	0.38	0.08	0.12	0.08	0.11	0.84	1.2	0.49	0.43
W(m)	34.45	158.2	53.34	50.9	25	9.14	21.49	0.2	18.29	46.18	54.89	51.21	0.4	36.58	160.3	79.97	55.78	0.4	34	10.53	18	14.02	0.4	0.2	0.4	0.2	18.3	78	13.34	15.85
row	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390



# TABLE 11. (Continued.) The raw data set used in ANFIS-FFA model development.

Kx(m2/s)	0.07	20	0.07	69	40.8	0.16	0.05	54.7	0.11	20.9	0.05	25.55	0.02	12.45	30.19	29.16	60.0	
U*(m/s)	0.03	0.08	0.08	0.04	0.06	0.01	0.03	0.03	0.04	0.05	0.04	0.08	0.07	0.03	0.07	0.07	0.01	
U(m/s)	0.58	0.27	0.64	0.36	0.23	80.0	0.52	0.2	69.0	0.46	0.63	0.52	0.61	0.23	0.42	0.44	80.0	
H(m)	0.09	0.49	0.12	0.2	0.69	2.01	0.14	1.4	0.12	0.42	0.12	0.71	0.13	2.47	0.8	0.87	2.16	
W(m)	0.2	16	0.4	15.7	42.21	37.62	0.2	33.4	0.2	50.9	0.2	24.4	0.4	61.72	42.4	47.5	38.3	
row	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	
Kx(m2/s)	0.09	32.51	44	1487	15.4	184.6	1.9	0.05	20.5	129.1	44	111.5	15.5	0.03	6.5	19.7	0.03	0.09
U*(m/s)	0.04	0.07	0.05	0.08	0.08	0.14	0.09	0.05	0.09	0.05	0.02	0.1	0.09	0.07	0.04	0.05	0.06	0.04
U(m/s)	0.75	0.34	0.36	1.62	0.24	66.0	0.22	0.83	0.77	0.56	0.34	0.43	0.78	0.58	0.23	0.21	0.54	0.67
H(m)	0.07	0.94	0.76	3.3	0.45	1.4	0.4	0.11	1.38	2.05	0.4	2.4	1.4	0.16	0.4	0.58	0.12	0.07
W(m)	0.2	25.91	31.7	180.6	12.4	44.2	11.58	0.2	25	103.6	161.5	70.1	25	0.4	40.5	35.8	0.4	0.4
row	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486
Kx(m2/s)	464.5	16.26	1040	0.14	16.26	0.03	12.8	99.0	176.3	11	0.07	0.27	33.52	153.3	55.74	0.04	0.07	5.1
U*(m/s)	0.07	0.07	0.09	0.01	0.07	0.07	0.04	0.01	0.06	0.05	0.04	0.05	0.09	0.51	0.11	0.03	0.04	0.1
U(m/s)	0.93	0.43	0.04	0.08	0.43	0.52	0.08	0.11	0.36	0.56	0.86	0.53	0.45	1.2	0.67	0.51	0.63	0.52
H(m)	2.23	0.52	0.36	1.46	0.52	0.11	0.61	1.46	0.53	2.71	0.09	0.13	1.3	2.94	2.13	0.06	0.12	0.92
W(m)	182.9	19.81	24.25	21.95	19.8	0.4	21.64	21.95	33.87	47.43	0.2	0.6	19.5	86	59.44	0.2	0.2	6.6
row	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468

- 7- Calculate the weighted output of consequences by Eq.13. The result of this step is given in column 8 in Table 10.
- 8- Calculate the final Kx value by using Eq.14: this is the final result of predicted Kx for given input values and is calculated and provide at the end of Table 10 (Kx=54.68).

these steps are used in an excel workbook and for all of the data are repeated to calculate the final values of model outputs and the procedure can be used in all of other cases as an explicit calculation procedure of ANFIS instead of previous black box approaches that limited the applicability of ANFIS models.

The newly developed equation (Eq.22) and its constants and parameters in Tables 9-10 is another novel contribution of ANFIS-FFA models in  $K_x$  estimations by providing explicit ANFIS based equation. Consequently, the newly developed equation can put its results into practical and numerical applications of pollutant transport over a wide range of hydraulic and hydrologic riverflows in the simulation of pollutant transport.

According to the statistical evaluations and one-by-one comparisons of ANFIS-FFA, ANFIS and existing equations, it is concluded that the ANFIS-FFA model shows a superior accuracy versus the others. The evaluation of the statistical indices of ANFIS-FFA and ANFIS demonstrates that hybrid training of the ANFIS with FFA is valuable because it provides a valuable improvement in the accuracy, generality and robustness of ANFIS to estimate the longitudinal dispersion in lack of the concentration profile measures.

### **IV. CONCLUSION**

In this paper, the ANFIS model trained with FFA is implemented to estimate the K<sub>x</sub> for pollutant transport. A global and general database of Kx contains 503 data records, is collected and assessed by the SSMD technique for subset selection. The sensitivity results attained in ANFIS-FFA with different input combinations of dominant variables showed that using the U, U<sup>\*</sup>, B and H variables led to the best results. Evaluation of ANFIS-FFA and existing equations suggests that the developed hybridization scheme outperforms the existing approaches in dimensional and Non-dimensional format of the results. The newly developed methodology estimated about 96% of  $K_x$  values with <5% error as presented by ellipse bounds. In conclusion, the ANFIS-FFA proved to be a consistent tool for pollutant dispersion estimations under a wide range of flow conditions, especially from small to large rivers. When the complexity of pollutant dispersion increases and generality of existing equations are wasted, due to a lack of their calibration data and inherent weaknesses of them, the newly developed model has valuable practical strength. The new developed explicit matrix formula (Eq.22) is a novel mathematical derivation of ANFIS-FFA model results. It can be used in hybridizing with numerical models of pollutant transport and this is one of the main contributions of the present paper in extending the applicability of black-box models of ANFIS-FFA in an explicit formulae. The proposed approach for the derivation of explicit equations based on ANFIS-FFA can be used in further studies of future ANFIS models.

### APPENDIX

See Table 11.

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