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# Aging Process Evaluation Method of Silicone Rubber in Composite Insulators in Natural Environmental Experiment Station

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**ABSTRACT** In this paper, silicone rubber on composite insulators from three different manufacturers with an operating duration between 1 and 10 years were sampled. In order to investigate the law of diminishing performance of these samples in aging process, widely adopted aging process evaluation test methods such as Hydrophobicity test, Water absorption test were performed. Based on test results, parameters significantly correlated with operating time were obtained by means of correlation calculation. Finally, considering the differences of parameter values among three manufacturers, the relative decrease value (denoted as *w*) of parameters was proposed as a unified standard and the equivalent equations between *w* and operating time were established for predicting lifespan of composite insulators in high altitude area. Test results indicate that parameters including saturated water absorption ratio  $\delta_s$ , the relative content of Si and O elements ( $X_{Si}$  and *XO*) are significantly correlated with operating time, and these three parameters can be used to characterize aging degree of composite insulators. Besides, for the relative error  $\sigma_1$  between theoretical operating time calculated by the equivalent relationship obtained in this paper and actual operating time is less than 20%, within the allowable error range of engineering practice, this equation can be applied to predict the operating time of composite insulators from three manufacturers in future research.

**INDEX TERMS** Composite insulators, aging properties, equivalent relationship, aging characterization.

#### **I. INTRODUCTION**

Since the 1960s, composite insulators were widely used in power transmission line systems [1]–[4]. As operating time went by, most composite insulators lost their hydrophobicity and allowed cracks and voids appearing in the superficial material of silicone rubber, resulting in pollution flashover and ice flashover accidents [5]–[8].

Over the past few years, scholars carried out plenty of researches to evaluate aging process properties of composite insulators. In literature [9]–[11], researchers evaluated the aging properties of composite insulators in aging process through measuring hydrophobicity in the superficial material of silicone rubber. In literature [11]–[12], images captured by

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Scanning Electron Microscope (SEM) were used to analyse the aging degree of composite insulators in aging process.

On this basis, some researchers proposed one or several parameters concluded from research results to characterize aging degree of composite insulators. In literature [12]–[14], Static Contact Angle (CA) method and FTIR method were employed to evaluate aging properties of composite insulators with different aging time, and parameters static contact angle and absorption peak altitude of main functional groups were proposed to characterize aging degree of composite insulators of the same manufacturer. In literature [15], aging properties of 391 composite insulators were evaluated through testing contamination, hydrophobicity, porosity analysis and so on of samples, and parameters such as the equivalent salt deposit density (ESDD), static contact angle (CA), porosity were proposed to establish the lifespan prediction model of silicone rubber in composite insulators.



**FIGURE 1.** Aging environments of composite insulators in a high altitude area experimental station.

**TABLE 1.** Samples of composite insulators with different aging years.

		Manufacturer	
Operating time/year	А	B	C
1	A <sub>1</sub>	$B_1$	$C_1$
3.5	A <sub>2</sub>	B <sub>2</sub>	C <sub>2</sub>
6	$A_3$	$B_3$	$C_3$
8	$A_4$	$B_4$	C <sub>4</sub>
10	A <sub>5</sub>	$B_5$	$C_5$

According to the current research of studying aging characterization of composite insulators, parameters such as static contact angle, hardness, images captured by SEM were commonly accepted [16]–[17]. However, due to the ignorance of the great influence of different compositions on aging process properties of composite insulators in aging process, the accuracy of the equivalent relationship obtained in most research is doubtful.

This work described in this paper was focused on establishing the equivalent equation where operating time of composite insulators from different manufacturers in high altitude area can be predicted widely. The main contents in this paper were divided into three parts. Sample, experimental setups and procedure of test methods such as CA method and Water absorption test method for different composite insulators are shown in Section 2. Results and analysis of aging process properties including physical, chemical and electrical properties of composite insulators are shown in Section 3. In Section 4, the correlation calculation of parameters of aging process properties for different composite insulators are shown in Part *A*, while the aging process evaluation method and verification are shown in Part *B*.

# **II. SAMPLE, EXPERIMENTAL SETUPS AND TEST PROCEDURE FOR DIFFERENT AGING COMPOSTIE INSULATORS**

## A. SAMPLE

In this research, composite insulators from three different manufacturers (denoted as A, B, C) exposed in natural environmental experiment station located in XueFeng mountain of Hunan province (as shown in Figure 1) for  $1 - 10$  years, were sampled, as shown in Table 1.



**FIGURE 2.** Silicone rubber rings from composite insulators. (a) Samples from Factory A. (b) Samples from Factory B. (c) Samples from Factory C.

In order to evaluate the aging process properties of silicone rubber in composite insulators, silicone rubber rings were cut off from composite insulators, as shown in Figure 2.

## B. EXPERIMENTAL SETUPS AND TEST PROCEDURE

Based on previous research [18], several widely accepted methods which can be used to evaluate aging process properties were employed for composite insulators from different manufacturers aged for different years.

#### 1) PHYSICAL PROPERTIES

## *a: CA (STATIC CONTACT ANGLE) METHOD*

Static contact angle in the superficial material of silicone rubber was measured through DropMeter A-100P. CA test criterion is based on IEC/TS 62073 - 2003 [19], where CA test results are divided into two parts. In this standard, if static contact angle of samples is more than 90 ◦ , silicone rubber is regarded as hydrophobic material; on the contrary, silicone rubber is regarded as hydrophilic material. Three samples from the same insulator were selected, and each sample was tested for six times. The average of test results, denoted as  $\theta_{av}$ , was obtained for comparing the hydrophobicity between composite insulators aged for different years.

## *b: WATER ABSORPTION TEST METHOD*

Water absorption test of samples was performed in a bucket, as shown in Figure 3. In Figure 3, TH is a hygrothermograph placed on the wall of the bucket to ensure the temperature constant in  $20 \pm 3^{\circ}$  and the humidity constant in 100%. Samples were placed on a glass plate which is 10 cm above the deionized water surface. In preparation, all samples should be dried until the quality of samples (denoted as  $m_0$ ) no longer decreased in air dry oven, where temperature was constant in 40 $^{\circ}$ .

When testing, the measuring process was divided into three stages. The first stage is  $0 - 8$  hours of experiment, in which the sample quality was tested every 1 hour. Sample quality of composite insulators was tested every 8 hours within 8 - 40 hours of the second stage. And during the last 168 hours, sample quality was tested every 24 hours. The ratio of water absorption, denoted as  $\sigma_t$ , could be obtained, as shown in Eq.  $(1)$ .

$$
\sigma_t = \frac{m_t - m_0}{m_0} \times 100\%
$$
 (1)



**FIGURE 3.** Water absorption testing device.



**FIGURE 4.** Schematic diagram of the AC test circuit.

where,  $m_t$  is sample quality in *t*th hour, g;  $m_0$  is the original sample quality, g.

# 2) CHEMICAL PROPERTIES *a: FTIR (FOURIER TRANSFORM INFRARED SPECTROSCOPY) METHOD*

The ALPHA Fourier infrared spectrometer produced by Bruker Company was used in infrared spectral measurement of samples. Absorption peak altitude of main functional groups ranged from 500  $cm^{-1}$  to 4000  $cm^{-1}$  were obtained for comparing chemical properties of composite insulators aged for different years in ATR mode.

#### *b: XPS (X-RAY PHOTOELECTRON SPECTROSCOPY) METHOD*

In order to further study chemical properties of composite insulators, X-ray photoelectron spectroscopy(XPS) was carried out in this research by ESCALAB 250Xi energy dispersive system, and relative content of main elements was obtained.

#### 3) ELECTRICAL PROPERTIES

#### *a: Salt-fog flashover test method*

In this paper, salt-fog flashover test was carried out in testing hall of Chongqing University. The power is supplied by the YDJ-5/50 AC testing transformer, of which the frequency is 50 Hz. The test circuit is shown in Figure 4, where B is the voltage regulator,  $T$  is the test transformer,  $R_0$  is the protective resistance, L is artificial fog chamber, P is ultrasonic water mist generator, DAS is voltage measuring system, Sample is the silicone rubber with the size of  $6 \text{ cm} \times 4 \text{ cm}$ . Electrodes were installed on both sides of the sample to meet the test requirement DLT 859 - 2004 [20], as shown in Figure 5.

Before the test, all samples were cleaned with anhydrous ethanol and water so that all traces of dirt were removed. Then



**FIGURE 5.** Diagram of the samples.

samples were left to dry indoors for 24 hours to avoid dust and other pollution.

According to DLT 859 - 2004 [20], the concentration of salt-fog in this study is 1000  $\mu$ S/cm, and samples should be wetted in salt-fog environment for 15 minutes to meet the test requirements. When testing, the uniform boosting method was adopted, in which applied voltage increases uniformly until flashover occurred. To enhance the accuracy of test results, three pieces of the sample from the same manufacturer with the same operating time were selected and each for three repeated tests, and the average value of flashover voltage was obtained to compare electrical properties between composite insulators aged for different years. The average flashover voltage  $U_f$ , the voltage gradient  $E_L$  and the relative standard deviation error  $\sigma$ % are calculated as follow:

*N*

$$
U_f = \frac{\sum\limits_{i=1}^{N} U_i}{N} \tag{2}
$$

$$
E_L = \frac{U_f}{d} \tag{3}
$$

$$
\sigma\% = \sqrt{\frac{\sum_{i=1}^{N} (U_i - U_f)^2}{N - 1}} \cdot \frac{100\%}{U_f}
$$
(4)

where, *U<sup>i</sup>* is an applied flashover voltage, kV; *N* is total number of tests;  $U_f$  is the average flashover voltage, kV;  $E_L$  is the voltage gradient, kV/cm; d is the arc development path of samples,  $d = 6$  cm in this paper;  $\sigma$ % is the relative standard deviation error.

# **III. TEST RESULTS AND ANALYSIS OF AGING PROCESS PROPERTIES OF COMPOSITE INSULATORS**

## A. PHYSICAL PROPERTIES

1) HYDROPHOBICITY

Due to excellent hydrophobicity of silicone rubber, composite insulators with silicone rubber as shed has good anti-pollution performance. With an increase of operating time, anti-pollution performance of samples becomes worse, which leads to an increase of possibility of pollution flashover. To study this phenomenon, CA test method was adopted, and test results were shown in Table 2.

Table 2 presents the following:

(i) In initial, loss and recovery phase, change regularities of static contact angle are similar. With the increase of operating time, static contact angle of composite insulators in three phases gradually decreases in aging process.

Phases	<b>Initial Phase</b>				Loss Phase			<b>Recovery Phase</b>		
Aging time/year										
	10.9	10.	10.6	84.3	82.1	81.2	105.8	106.3	111.6	
3.0	108.8	106.7	104.8	83.4	79.3	79.9	102.1	103.3	105.7	
	102.7	102.6	99.7	82.9	77.4	76.1	100.6	102.	94.1	
	94.8	93.3	92.2	81.1	70.1	72.9	92.2	95.3	91.8	
10	87.6	84.6	80.8	78.1	70.6	68.7	85.5	86.4	83.	

**TABLE 2.** Hydrophobicity test results on samples in aging process.

(ii) The hydrophobicity of samples in initial, loss and recovery phase is different. In Table 2, static contact angles of composite insulators from three manufacturers are all above 90 ° within 8 years, which indicates that these composite insulators are still in good condition and can be regarded as hydrophobic material according to IEC/TS 62073 - 2003 [19]. Compared with the static contact angles in initial phase, static contact angles in loss phase decrease by 10.8% - 26.5%, which leads to a decrease of hydrophobicity of samples and these composite are all regarded as hydrophilic material according to IEC/TS 62073 - 2003 [19]. After drying indoors for 24 hours, static contact angle of samples in recovery phase is similar to that in initial phase and it indicates that the hydrophobicity of samples recovers to the state of the initial stage.

#### 2) WATER ABSORPTION TEST

With the increase of operating time, more cracks appear in the superficial material of composite insulators, which leads to the increase of water absorption performance of samples. After absorbing water, the physical, chemical and electrical properties of silicone rubber will change. Besides, water is the key factor which affects the performance of silicone rubber. In this paper, the water absorption test was performed to analyze the relationship between the water absorption of composite insulators and operating time. The relationship between the ratio of water absorption  $\sigma_t$  and water absorption time was shown in Figure 6.

Figure 6 presents the following:

(i) The change regularities of the water absorption ratio  $\sigma_t$  of composite insulators from three manufacturers with testing time are similar, which are mainly divided into three parts including 0 - 8 hours, 8 - 40 hours and 40 - 240 hours. In 0 - 8 hours, due to the dry state of silicone rubber, water absorption speed of samples is the fastest; In 8 - 40 hours, with the increase of water content, the water absorption speed slows down; In 40 - 208 hours, the water content in silicone rubber reaches saturation, and water absorption speed is the slowest at this stage.

(ii) In the same humidity environment, there are some differences of the water absorption speed among composite insulators aging for different years. With the increase of operating time, the water absorption speed of composite insulators gradually increases. For example, the water absorption ratio of samples aged for 1, 6 and 10 years from Factory A at



 $(C)$ 

**FIGURE 6.** Water absorption regularity of samples of composite insulators in aging process. (a) Samples from Factory A. (b) Samples from Factory B. (c) Samples from Factory C.

8 hour is 0.088%, 0.173% and 0.329% respectively; Besides, the water absorption ratio at 40 hour is 0.134%, 0.235% and 0.517% respectively; Finally, the water absorption ratio at 208 hour is 0.172%, 0.401% and 0.791% respectively.

The differences of compositions in composite insulators from different manufacturers will result in the differences in the water absorption speed of samples. Thus, the method, comparing the water absorption ratio of different samples at a certain time cannot reflect the differences in the water



**FIGURE 7.** Saturated water absorption ratio of samples in aging process.

**TABLE 3.** Key absorption peaks of silicone rubber in FTIR analysis.

Functional groups	Wavenumber/cm <sup>-1</sup>
$O-H$	3700-3200
$CH_3(C-H)$	2960
C-H	1440-1410
$Si$ $CH2(C2H)$	1270-1255
$Si-O-Si(Si-O)$	1100-1000
$O-Si(CH_3)_2-O(Si-O)$	840-790
SiCH <sub>3</sub>	800-700

absorption performance of composite insulators accurately. In this paper, the saturated water absorption ratio  $\delta_s$  was proposed in this paper as the parameter to characterize the water absorption performance of composite insulators, and results of  $\delta_s$  of samples from three manufacturers are shown in Figure 7.

In Figure 7, the increase of operating time leads to an gradually accelerating increase of the saturated water absorption ratio of composite insulators. Through comparing δ*<sup>s</sup>* of samples, it can be found that the saturated water absorption ratio of samples from Factory A aged for 3.5, 6, 8, 10 years is 0.59, 1.35, 2.95, 3.63 times that of samples aged for 1 year. The increase trend of the saturated water absorption ratio of samples from Factory A gradually accelerates with an increase of operating time. And the saturated water absorption ratio of samples from other two manufacturers all follows this change regularity.

## B. CHEMICAL PROPERTIES

#### 1) FTIR TEST

Fourier transform infrared spectroscopy (FTIR) has been widely adopted in material analysis to obtain an infrared spectrum of absorption of samples. Key absorption peaks corresponded to functional groups in silicone rubber material are listed in Table 3 and test results of main functional groups of samples from Factory A, B and C are shown in Figure 8–10 respectively.

Figure 8–10 present the following:

(i) The main functional groups of samples from three manufacturers are consistent, and there are no new key functional groups appearing in the superficial material of samples in the aging process.



**FIGURE 8.** FTIR analysis results of samples from Factory A in aging process. (a) Wavenumber between 500 ∼ 2000 cm−**1**. (b) Wavenumber between 2000 ∼ 4000 cm−**1**.



**FIGURE 9.** FTIR analysis results of samples from Factory B in aging process. (a) Wavenumber between 500 ∼ 2000 cm−**1**. (b) Wavenumber between 2000 ∼ 4000 cm−**1**.

(ii) With the increase of operating time, it leads to a decrease of the absorption peak altitude of Si-O-Si at wavenumber  $1100 \sim 1000 \text{ cm}^{-1}$  and Si-(CH<sub>3</sub>)<sub>2</sub> at wavenumber 840  $\sim$  790 cm<sup>-1</sup> as well as an increase of the absorption peak altitude of –OH at wavenumber 3700  $\sim$  2800 cm<sup>-1</sup>.



**FIGURE 10.** FTIR analysis results of samples from Factory C in aging process. (a) Wavenumber between 500 ∼ 2000 cm−**1**. (b) Wavenumber between 2000 ∼ 4000 cm−**1**.

**TABLE 4.** Results of H of composite insulators in aging process.

Operating time/year		H	
	Factory A	Factory B	Factory C
	0.9681	0.9302	0.9664
3.5	0.9569	0.9304	0.9400
6	0.9588	0.9259	0.9381
8	0.9529	0.9232	0.9260
$\overline{0}$	0.9429	0.9097	0.9276

However, due to the different compositions of composite insulators from three manufacturers, analyzing differences of absorption peaks altitude between typical functional groups cannot reflect changes of chemical properties of composite insulators. In previous research, researchers indicate that the ratio of the absorption peak altitude of Si-O-Si to C-H can reflect the relative content of its side bond, which is the key reason for the changes of chemical properties in aging process [21]. In this paper, the ratio (denoted as  $H$ ) of Si-(CH<sub>3</sub>)<sub>2</sub> absorption peak altitude to Si-O-Si absorption peak altitude is used to characterize aging degree of composite insulators, and test results of *H* of samples from three manufacturers are shown in Table 4.

#### 2) XPS TEST

In order to further study the chemical properties of composite insulators in aging process, XPS test method was employed in this paper to analyze the relative content of main elements of composite insulators. Test results of Si, C, O, Al, Fe and Pt elements of samples from three manufacturers are shown in Table 5–7.

**TABLE 5.** The relative content of main elements of samples from factory A in aging process.

Samples	$Si\frac{9}{6}$	C(%)	O(%)	$Al(\%)$	$Fe\frac{9}{6}$	$Pt(\%)$
Aı	21.88	47.17	28.17	2.49	0.18	0.11
A2	21.3	47.01	28.99	2.4	0.18	0.12
A3	20.49	46.18	30.8	2.18	0.23	0.12
A4	19.33	44.56	32.94	2.82	0.22	0.13
A٤	18.11	44.09	34.79	2.65	0.23	0.13

**TABLE 6.** The relative content of main elements of samples from factory B in aging process.

Samples	$Si(\%)$	C(%)	O(%)	Al(%)	$Fe\frac{9}{6}$	$Pt(\%)$
в,	22.71	45.74	29.3		0.12	0.13
B <sub>2</sub>	21.86	44.86	30.8	2.14	0.14	0.2
$B_3$	21.21	43.11	33.1	2.27	0.14	0.17
B4	20.09	41.71	35.93	1.94	0.17	0.16
В,	19.18	40.83	37.74		0.12	0.13

**TABLE 7.** The relative content of main elements of samples from factory C in aging process.



#### Table 5–7 presents the following:

(i) With the increase of operating time, the relative content of Si and C elements in the superficial material of samples from three manufacturers gradually decrease, which results in the decrease of Si-O-Si and  $Si$ - $CH_3$ )<sub>2</sub> absorption peak altitude in aging process.

(ii) With the increase of operating time, the relative content of O element in the superficial material of samples from three manufacturers gradually increases, which leads to an increase of –OH absorption peak altitude in aging process.

(iii) With the increase of operating time, there are few changes in the relative content of Al, Fe and Pt elements, which indicates that the factor aging in high altitude area will not cause the relative content of elements such as Al, Fe and Pt to change in aging process.

## C. ELECTRICAL PROPERTIES

#### 1) SALT-FOG FLASHOVER TEST

In this paper, the salt-fog flashover test was carried out to analyze the change regularity of salt-fog flashover voltages with the increase of operating time, and test results are shown in Table 8.

Table 8 presents the following:

(i) With the increase of operating time, salt-fog flashover voltage of samples from three manufacturers gradually decreases. For samples from Factory A, salt-fog voltage of samples at 3.5, 6, 8 and 10 year is 13.71, 13.23, 12.40 and 11.42 kV respectively, which decrease by 3.86%,

Operating	Factory A				Factory B			Factory		
time(year)	U/(kV)	$\sigma$ <sup>(%)</sup>	$E_I(kV/cm)$	UAKV	$\sigma$ <sup>(%)</sup>	$E_l$ (kV/cm)	UdkV	$\sigma$ <sup>(%</sup> )	$E_l(kV/cm)$	
	l 4.3	-4.0	2.4	1 J.I	າ າ <u>.</u>	ن ، ک	13.9	$\sim$ $\sim$ ن. ب	$\sim$ $\sim$ $\sim$ .J	
3.5	13.7	$-4.1$	2.3	14.6	4.5	2.4	13.3	4.9	$\Omega$ $\overline{\phantom{m}}\cdot\overline{\phantom{m}}$	
	13.2	. . ں ر	2.2	14.2	4.1	2.4	12.8	$\sim$ $\sim$ ر. ے	$\sim$ .	
	2.4	$\sim$ <u>، ، ،</u>	2.1	12.1	3.8	2.0	11.2	$\sim$ . 1		
10	1.4	ັ∙		10.6		0.،	10.0	4.č		

**TABLE 8.** Test results of salt-fog flashover voltage of samples in 1000µS/cm environment in aging process.

**TABLE 9.** Aging parameters of samples from three manufacturers.

No.	Aging parameters	Test methods
	$\theta_{av}$	Static contact angle of the surface of samples in initial phase
$\overline{2}$	$\delta_{\rm S}$	Saturated water absorption ratio of samples
3	H	The ratio of $Si$ - $(CH_3)$ <sub>2</sub> absorption peak altitude to $Si$ -O-Si absorption peak altitude
4	$X_{\rm Si}$	Relative content of Si element of samples
5	$X_{\rm C}$	Relative content of C element of samples
6	$X_{\rm O}$	Relative content of O element of samples
	$U_{y1}$	Salt-fog flashover voltage of samples in 1000us/cm

7.22%, 13.04%, 19.9% compared with samples at 1 year in 1000  $\mu$ s/cm salt-fog environment.

(ii) With the increase of operating time, *E<sup>L</sup>* of samples gradually decreases, but they are all within the range where composite insulators can maintain excellent electrical performance. For samples aged for 10 years from three manufacturers, salt-fog voltages of  $A_5$ ,  $B_5$  and  $C_5$  are 1.90, 1.76 and 1.67 kV/cm respectively.

## **IV. AGING PROCESS EVALUATION METHOD OF COMPOSITE INSULATORS**

## A. CORRELATION PARAMETERS ANALYSIS OF AGING PROCESS PROPERTIES FOR COMPOSITE INSULATORS

In Section 3, aging properties of samples from three manufacturers are measured through CA test method, Water absorption test method, FTIR method, XPS method and Salt-fog flashover test. Through analyzing test results of aging effects, some parameters which can be used to characterize aging degree are concluded and listed on Table 9.

In this section, Person correlation analysis calculation was employed and the correlation coefficient *r* was proposed to analyze the correlation between these parameters and operating time.

$$
r = \frac{\sum_{i=1}^{n} (x_i - \bar{x})(t_i - \bar{t})}{\sqrt{\sum_{i=1}^{n} (x_i - \bar{x})^2} \sqrt{\sum_{i=1}^{n} (t_i - \bar{t})^2}}
$$
(5)

where,  $x_i$  is the aging characterization parameters of *i*th sample;  $t_i$  is aging year of *i*th sample;  $\bar{x}$  is the mean value of aging characterization parameters of samples aged for different years;  $\bar{t}$  is the mean value of operating time of samples aged for different years.

Besides, *T* -test was employed to verify the significance of the correlation coefficient  $r$  of samples from three manufacturers and the results of  $T$ -test were denoted as  $\alpha$ .

$$
T = \frac{r\sqrt{n-2}}{\sqrt{1-r^2}} \sim t(n-2)
$$
 (6)

where, if  $\alpha > 0.05$ , it indicates that two variables are irrelative with each other; if  $0.01 < \alpha \leq 0.05$ , it indicates that two variables are correlated; if  $\alpha \leq 0.01$ , it indicates that two variables are significantly correlated.

The correlation calculation results of aging characterization parameters are shown in Table 10.

Based on test results of correlation analysis, the conclusion that parameters including static contact angle  $\theta$ , saturated water absorption ratio of samples  $\delta_S$ , the relative content of Si, C and O element are significantly correlated with operating time. Besides, parameter  $U_{v1}$ (salt-fog flashover voltage of samples in 1000  $\mu$ s/cm) is correlated with operating time.

Meanwhile, the partial correlation method was employed to test the independence of these significantly correlated parameters, and operating time is taken as control variable. The analysis method is similar to that of correlation calculation between different parameters. If the significance of the independent hypothesis  $\alpha > 0.05$ , the hypothesis is true and two variables are non-independent variables; Otherwise, these two parameters are independent with each other. The calculation results are listed on Table 11–13.





#### **TABLE 11.** The calculation results of the independence of significantly correlated parameters of factory A.

Parameters	$\alpha(\theta)$	$\alpha(\delta_{\rm S})$	$\alpha(X_{Si})$	$\alpha(X_O)$
$\alpha(\theta)$	0	0.192	0.033	0.003
$\alpha(\delta_S)$	0.192	0	0.103	0.234
$\alpha(X_{\rm Si})$	0.033	0.103	0	0.052
$\alpha(X_O)$	0.003	0.234	0.052	0

**TABLE 12.** The calculation results of the independence of significantly correlated parameters of factory B.

Parameters	$\alpha(\theta)$	$\alpha(\delta_{\rm S})$	$\alpha(X_{Si})$	$\alpha(X_O)$
$\alpha(\theta)$	0	0.024	0.037	0.184
$\alpha(\delta_{\rm S})$	0.024	$^{()}$	0.117	0.222
$\alpha(X_{Si})$	0.037	0.117	0	0.221
$\alpha(X_O)$	0.184	0.222	0.221	0

**TABLE 13.** The calculation results of the independence of significantly correlated parameters of factory C.



Based on calculation results in Table 11–13, parameters except static contact angle  $\theta$  and relative content of C element are all independent with each other, and these parameters including saturated water absorption ratio  $\delta_S$ , the relative content of Si and O elements  $(X_{Si}$  and  $X_O$ ) can be used in characterizing aging degree of composite insulators in aging process.

# B. AGING PROCESS EVALUATION METHOD AND VERIFICAITION

In previous research, some scholars proposed some parameters to analyze aging degree of composite insulators from one single manufacturer. Due to the influence of different compositions of composite insulators from three manufacturers

#### **TABLE 14.** The change regularity of the saturated water absorption ratio  $\delta_{{\bm S}}.$

Operating	Factory A			Factory B	Factory C	
time/year	$\partial_S$	$w\frac{6}{6}$	$\partial_S$	$w\%$	$\partial s$	wO6
	0.188		0.175		0.214	0
3.5	0.272	45.1	0.241	37.7	0.29	35.5
6	0.401	113.9	0.338	93.1	0.412	92.5
8	0.522	178.4	0.469	168	0.54	152.3
10	0.791	321.9	0.625	257.1	0.764	257

**TABLE 15.** The change regularity of the relative content of Si element  $X_{\text{S}i}$ .



to the initial value of parameters, it is difficult to conclude the methods where aging degree of composite insulators from different manufacturers can be characterized quantitatively.

In this paper, although the initial values of each characterization parameter are different among samples from different manufacturers, the change regularity of parameters is similar with the increase of time and the aging degree of composite insulators can be characterized by the relative decrease value compared with the initial value of parameters. The relative decrease value (denoted as *w*) compared with the initial value was proposed as a unified standard to characterize the aging degree of composite insulators from different manufacturers.

$$
w = \frac{x_t - x_1}{x_1} \times 100\%
$$
 (7)

where,  $x_t$  is the value of parameters at *t*th year;  $x_1$  is the initial value of parameters at 1 year.

The results of *w* of parameters including  $\delta_S$ ,  $X_{Si}$  and  $X_O$  are shown in Table 14–16.

**TABLE 16.** The change regularity of the relative content of Si Element  $X_0$ .

Operating	Factory A			Factory B	Factory C	
time/year	$X_O$	$w\frac{6}{90}$	$X_{\Omega}$	$w\frac{6}{20}$	$X_{\Omega}$	wG6
	27.67		29.30		30.77	0
3.5	27.99	4.30	30.80	5.12	33.72	6.34
6	28.8	11.31	33.11	12.99	35.36	14.92
8	32.44	19.05	35.93	22.63	38.48	25.06
10	34.79	25.73	37.74	28.81	40.22	30.72

**TABLE 17.** Aging parameters significantly correlated with operating time of composite insulators in aging process.





**FIGURE 11.** The estimated regression calculation of parameters with operating time. (a) δ**<sup>S</sup>** (b) **XSi**. (c) **XO**.

In order to establish the equivalent relationship between *w* of parameters significantly correlated with operating time and operating time, the median (denoted as  $w_1$ ), which can reflect the centralization trend of parameter in mathematical statistics, was proposed to represent the decreasing trend of parameters from different manufacturers at the same aging year. The results of  $w_1$  of relative decrease values are listed on Table 17.

In this paper, SPSS, a data processing software, is used to perform the estimation regression calculation of *w* of parameters including  $\delta_S$ ,  $X_{Si}$  and  $X_O$  with operating time, and calculation results are shown in Figure 11.

Figure 11 presents that the cube of *w* of parameters fits well with operating time, which can be used to obtain the equivalent relationship between these parameters and operating time

#### **TABLE 18.** The error of operating time based on  $\delta_S$  between theoretical value and actual value in aging process.

Operating	$\sigma_1(\%)$		
time/year	Factory A	Factory B	Factory C
	0.05	0.05	0.05
3.5	11.40	0.14	3.71
6	9.90	0.79	1.13
8	0.11	2.43	6.20
10	13.13	5.88	5.90

**TABLE 19.** The error of operating time based on  $X<sub>O</sub>$  between theoretical value and actual value in aging process.

Operating time/year	$\sigma_1(\%)$		
	Factory A	Factory B	Factory C
	6.04	6.04	6.04
3.5	8.77	13.56	6.25
6	5.96	3.39	2.08
8	2.22	0.70	7.73
10	2.28	3.75	2.39

**TABLE 20.** The error of operating time based on  $X_{S_i}$  between theoretical value and actual value in aging process.



as follow:

$$
\begin{cases}\ny = 0.0000005x_1^3 - 0.0003x_1^2 + 0.0768x_1 + 0.9995 \\
y = -0.0007x_2^3 - 0.0349x_2^2 - 0.9322x_2 + 0.9396 \\
y = 0.0005x_3^3 - 0.0238x_3^2 + 0.6131x_3 + 0.9786\n\end{cases}
$$
\n(8)

where,  $x_1$  is the *w* of saturated water absorption ratio  $\delta_s$ ;  $x_2$ is the *w* of the relative content of Si element  $X_{Si}$ ;  $x_3$  is the relative content of O element  $X_O$ ;  $y$  is the operating time.

In this paper,  $\sigma_1$  is defined as the relative error between the actual operating time *y* and theoretical operating time  $y_1$ . Results of  $\sigma_1$  of different parameters are shown in Table 18–20.

$$
\sigma_1 = \frac{|y - y_1|}{y} \times 100\% \tag{9}
$$

Table 18–20 presents that the relative error  $\sigma_1$  of parameters including saturated water absorption ratio  $\delta_S$ , the relative content of Si element *XSi* and the relative content of O element  $X_O$  is less than 20%, which is within the allowable error range of engineering practice. In future research, when initial and current values of parameters including  $\delta_S$ ,  $X_{Si}$  and  $X_O$  have been obtained, operating time of composite insulators from these three manufacturers can be predicted by the Eq.(8).

### **V. CONCLUSION**

This paper studies the aging properties of composite insulators aging in natural environmental experiment station

through physical, chemical and electrical tests in aging process and explores aging characterization parameters based on test results. Considering the differences resulting from different components of three manufacturers, the relative decrease value (denoted as *w*) compared with the initial value was proposed as a unified standard, and the equivalent relationship significantly correlated parameters and operating time can be obtained based on the parameter *w*. The main conclusions are as follows:

(1) With the increase of operating time, the change regularity of aging properties of composite insulators from three manufacturers is similar in aging process: when the operating time increases, it will lead to an increase of the hydrophobicity, the relative content of O element and salt-fog flashover voltage of samples, and a decrease of the relative content of Si and C elements.

(2) Through calculating the correlating relationship between operating time and aging characterization parameters concluded from results of aging affects tests, it indicates that parameters including saturated water absorption ratio δ*<sup>s</sup>* , the relative content of Si and O elements  $(X_{Si}$  and  $X_O$ ) are significantly correlated with operating time. And these three parameters can be used to characterize aging degree of composite insulators from three manufacturers.

(3) The relative decrease value (denoted as *w*) of aging characterization parameters compared with the initial value was proposed as a unified standard to establish the equivalent relationship between aging parameters and operating time, and it turns out that the cube of *w* of parameters fits well with operating time by means of the estimation regression calculation.

(4) In this paper, the equivalent relationship between *w* of parameters and operating time was established. Through the verification, it turns out that the relative error  $\sigma_1$  between theoretical operating time based on *w* of parameters including saturated water absorption ratio  $\delta_S$ , the relative content of Si element  $X_{Si}$  and the relative content of O element  $X_O$ and actual operating time is less than 20%, which is within the allowable error range of engineering practice. Therefore, operating time of composite insulators from these three manufacturers aging in high altitude area can be predicted by the equivalent relationship obtained in this paper in the future research.

(5) The results and conclusions of this study are based on the samples exposed in high altitude area. In this case, whether the aging process evaluation method is applicable to other areas needs further verification and research.

#### **REFERENCES**

- [1] G. G. Karady, M. Shah, and R. L. Brown, "Flashover mechanism of silicone rubber insulators used for outdoor insulation-I,'' *IEEE Trans. Power Del.*, vol. 10, no. 4, pp. 1965–1971, Oct. 1995.
- [2] A. de la O, R. S. Gorur, and J. T. Burnham, "Electrical performance of nonceramic insulators in artificial contamination tests. Role of resting time,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 3, no. 6, pp. 827–835, Dec. 1996.
- [3] L. Xidong, ''Development of composite insulators in China,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 6, no. 5, pp. 586–594, Oct. 1999.
- [4] X. Jiang, J. Yuan, Z. Zhang, J. Hu, and L. Shu, ''Study on pollution flashover performance of short samples of composite insulators intended for ±800 kV UHV DC,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 14, no. 5, pp. 1192–1200, Oct. 2007.
- [5] X. Jiang, Z. Xiang, Z. Zhang, J. Hu, Q. Hu, and L. Shu, ''Predictive model for equivalent ice thickness load on overhead transmission lines based on measured insulator string deviations,'' *IEEE Trans. Power Del.*, vol. 29, no. 4, pp. 1659–1665, Aug. 2014.
- [6] Q. Hu, S. Wang, L. Shu, X. Jiang, J. Liang, and G. Qiu, ''Comparison of AC icing flashover performances of 220 kV composite insulators with different shed configurations,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 23, no. 2, pp. 995–1004, Apr. 2016.
- [7] Q. Hu, W. Yuan, L. Shu, X. Jiang, and S. Wang, ''Effects of electric field distribution on icing and flashover performance of 220 kV composite insulators,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 21, no. 5, pp. 2181–2189, Oct. 2014.
- [8] X. Jiang, J. Yuan, L. Shu, Z. Zhang, J. Hu, and F. Mao, ''Comparison of DC pollution flashover performances of various types of porcelain, glass, and composite insulators,'' *IEEE Trans. Power Del.*, vol. 23, no. 2, pp. 1183–1190, Apr. 2008.
- [9] S. M. Gubanski and A. E. Vlastos, ''Wettability of naturally aged silicon and EPDM composite insulators,'' *IEEE Trans. Power Del.*, vol. 5, no. 3, pp. 1527–1535, Jul. 1990.
- [10] W. Song, W.-W. Shen, G.-J. Zhang, B.-P. Song, Y. Lang, G.-Q. Su, H.-B. Mu, and J.-B. Deng, ''Aging characterization of high temperature vulcanized silicone rubber housing material used for outdoor insulation,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 22, no. 2, pp. 961–969, Apr. 2015.
- [11] N. C. Mavrikakis, P. N. Mikropoulos, and K. Siderakis, ''Evaluation of field-ageing effects on insulating materials of composite suspension insulators,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 24, no. 1, pp. 490–498, Feb. 2017.
- [12] G. Haddad, K. L. Wong, and P. Petersen, "Evaluation of the aging process of composite insulator based on surface charaterisation techniques and electrical method,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 23, no. 1, pp. 311–318, Feb. 2016.
- [13] S. M. Rowland, Y. Xiong, J. Robertson, and S. Hoffmann, "Aging of silicone rubber composite insulators on 400 kV transmission lines,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 14, no. 1, pp. 130–136, Feb. 2007.
- [14] C. Xie, Y. Zhang, J. Wang, Y. Hao, M. Gao, and Y. Liu, ''Research on evaluation method of composite insulators aging,'' presented at the IEEE 9th Int. Conf. Properties Appl. Dielectr. Mater., Jul. 2009, doi: [10.1109/ICPADM.2009.5252420.](http://dx.doi.org/10.1109/ICPADM.2009.5252420)
- [15] L. Cheng, L. Wang, Z. Guan, and F. Zhang, "Aging characterization and lifespan prediction of silicone rubber material utilized for composite insulators in areas of atypical warmth and humidity,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 23, no. 6, pp. 3547–3555, Dec. 2016.
- [16] A. R. Chughtai, D. M. Smith, L. S. Kumosa, and M. Kumosa, "FTIR analysis of non-ceramic composite insulators,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 11, no. 4, pp. 585–596, Aug. 2004.
- [17] R. Chakraborty and B. S. Reddy, ''Studies on high temperature vulcanized silicone rubber insulators under arid climatic aging,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 24, no. 3, pp. 1751–1760, Jun. 2017.
- [18] *Guide for the Assessment of Composite Insulators in the Laboratory After Their Removal From Service*, CIGRE Brochure 481, Working Group B2.21, CIGRE, Pairs, France, 2011.
- [19] *Guidance on the Measurement of Wettability of Insulator Surfaces*, Standard IEC TS 62073:2003, 2003.
- [20] *Artificial Contamination Test of Composite Insulators for High Voltage AC System*, Standard DL/T 859-2004, Beijing, China, 2004.
- [21] L. Cheng, H. Mei, L. Wang, Z. Guan, and F. Zhang, ''Research on aging evaluation and remaining lifespan prediction of composite insulators in high temperature and humidity regions,'' *IEEE Trans. Dielectr. Electr. Insul.*, vol. 23, no. 5, pp. 2850–2857, Oct. 2016.



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