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Advanced Fruit Fly Optimization Algorithm and Its Application to Irregular Subarray Phased Array Antenna Synthesis

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ABSTRACT In this paper, an advanced fruit fly algorithm (FOA) is proposed and applied in subarray phased array antenna synthesis. The proposed algorithm introduces orthogonal crossover, quantum selection and simulated annealing operations on the individuals, and then combines them by using an adaptive expansion-contraction factor. Accordingly, a linear generation mechanism of candidate solution based fruit fly algorithm (LGMS-FOA) is generated, in which individuals are selected in a highly balanced way, and the poor solutions are still accepted with a varying probability during the iteration. These mechanisms help the proposed algorithm enhance the population diversity and global searching capability but avoid falling into local optimum. Numerical classical unimodel benchmark functions are provided to test the proposed algorithm (OLFOA) in comparison with other advanced algorithms. In addition, to further validate its superiority, the proposed algorithm is applied to handle the subarray array synthesis of several tough planar and circular apertures with different array sizes and subarray shapes. Simulation results show that the proposed OLFOA can achieve better performance than other improved evolutionary algorithms.

INDEX TERMS Irregular subarray, fruit fly algorithm, orthogonal crossing, quantum behavior, simulated annealing, array synthesis.

I. INTRODUCTION

Recently, subarray technology has attracted considerable interests in radar and communication systems, because it can greatly reduce the cost and complexity of the system by reducing the number of antenna splitters and phase shifters [1]. Currently, the subarray partition and optimization problem remains to be a large barrier in the development of subarray technology. Various solutions have been explored to solve this problem. The subarray partitioning method based on genetic algorithm (GA) was proposed in [2]–[5]. These methods could solve the partitioning of irregular subarray, but got poor performance in solving the exact partition problem. Then, a method based on analytic schematadriven optimization, which achieves exact partition in low-/

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medium-sized rectangular subarrays, was introduced in [6]. The *X* algorithm-based subarray tiling method, which exhibits great efficiency and accuracy in irregular subarray partitioning, was proposed in [7]. Although subarray technology applied in array antenna design helps to alleviate the high grating lobe to certain extent, exploring high-performance intelligent optimization algorithms for array synthesis, especially for large array or huge elements, is urgently desired.

Evolutionary algorithms have long been considered as efficient candidates to solve antenna synthesis problems. Genetic algorithm (GA) and particle swarm optimization (PSO) are two well-known optimization algorithms for array antenna synthesis [8], [9]. Simulated annealing algorithm (SA), ant colony optimization algorithm (ACO), and differential evolution algorithm (DE) are also widely used in array antenna optimization [10]–[12]. In addition, several recently proposed algorithms, such as invasive weed optimization



algorithm (IWO) [13] and artificial bee colony algorithm technique (ABC) [14], have been successfully implemented in antenna design and optimization. These algorithms appear to be less and less effective in solving complex problems with high dimension and large computation overhead.

In 2012, motivated by the behavior of fruit fly in seeking food, a new fruit fly optimization algorithm (FOA) [15] was proposed. As a new global evolutionary algorithm, FOA is well-known for its simple principle, few adjustable parameters, strong global optimization capability, and fast convergence speed. Similar to other evolutionary algorithms, FOA also shows the disadvantages of easily falling into the local optimum and limited performance when calculating multi-dimensional problems. To address these shortcomings, a modified fruit fly algorithm integrated with the linear generation mechanism of candidate solution (LGMS) was proposed in [16], showing that the algorithm performance was greatly improved without changing any natural concept. However, the shortcomings of the fruit fly algorithm were still not addressed completely.

In this study, an advanced LGMS-FOA, namely, OLFOA, is proposed. By introducing orthogonal cross [17] and quantum selection [19] operations on the individuals, the proposed OLFOA combines them with an adaptive expansion-contraction factor to improve the convergence performance in solving high-dimensional complex problems. On this basis, the simulated annealing [20] strategy is introduced to further enhance the diversity of the population. The superior performance of the proposed algorithm has been validated via both numeral benchmark function tests and high-dimensional subarray phased array antenna synthesis problems with different array sizes and subarray shapes.

This paper is organized as follows: Section II introduces the concepts of FOA and LGMS-FOA. Section III presents a detailed architecture of the proposed OLFOA. Section IV makes comparisons between OLFOA and several recently proposed algorithms. Section V describes the application of OLFOA in solving high-dimensional subarray phased array antenna synthesis problems. Section VI draws the conclusion.

II. FOA AND LGMS-FOA

A. FOA

Fruit fly algorithm is a global optimization method based on the food-finding behavior of the fruit fly population. In the process of searching for food in the search space, other fruit flies are randomly searched for a certain range from the current location of fruit fly closest to the food. The search process is repeated starting from the fruit fly that is currently closest to the food until the food is found. Fig. 1 illustrates the food-finding iterative process of the fruit fly swarm. The x- and y-axis are the search spaces for the fruit fly population. The circles indicate the fruit fly swarms. The solid arrows indicate the food-finding direction of the fruit fly population, whereas the dashed arrows indicate the food-finding direction of fruit fly individuals. $x_{best}^{i}, y_{best}^{i}$ indicates the fruit fly that

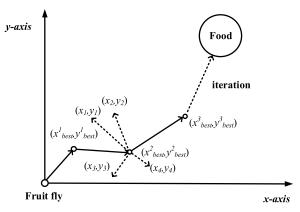


FIGURE 1. Food-finding iterative process of fruit fly swarm.

is closest to the food in the *i*th iteration. x_n, y_n indicates the location of nth fruit fly individual in the x- and y-axis, respectively.

The specific steps of the FOA algorithm are shown as

Step 1. The maximum number of iterations (genmax), population size (popsize), range of random fruit flies (LR), and random direction of fruit fly (FR) in the fruit fly algorithm are initialized. Then, the location of the fruit fly population is defined.

$$x \ axis = rand(LR) \tag{1}$$

$$v \ axis = rand(LR) \tag{2}$$

where the x_axis and y_axis represent the searching center of the fruit fly population in x- and y-axis, respectively.

Step 2. Each fruit fly is updated with a random search direction and distance by

$$x_i = x_axis + rand(FR) \tag{3}$$

$$y_i = y_axis + rand(FR)$$
 (4)

Step 3. The distance (Dist) between the location of the fruit fly and the origin and the taste decision value (S) of the fruit fly (S characterizes the distance from the food) are calculated as follows:

$$Dist_i = \sqrt{x_i^2 + y_i^2}$$

$$S_i = \frac{1}{Dist_i}$$
(5)

$$S_i = \frac{1}{Dist_i} \tag{6}$$

Step 4. The taste decision value is substituted into the fitness function to calculate the corresponding fitness value (Smell).

$$Smell_i = fitness function(S_i)$$
 (7)

Step 5. The optimal fitness value (bestsmell) and corresponding location (bestindex) of the fruit fly individual are obtained

$$[bestsmell, bestindex] = min(Smell)$$
 (8)

Step 6. The optimal fitness is set as the global optimal value (gsmell), and the corresponding location of fruit fly is used

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as the searching center coordinate of the next iteration.

$$gsmell = bestsmell$$
 (9)

$$x \ axis = x(bestindex)$$
 (10)

$$y_axis = y(bestindex)$$
 (11)

Step 7. Steps 2–6 are repeated until the terminal criterion is met or the maximum number of iterations is reached.

B. LGMS-FOA

From the description of the fruit fly algorithm, it is discovered that, given that the taste determination value (*S*) is always greater than zero, the fruit fly algorithm cannot express the negative number in the dimension level. Moreover, given that the taste judgment value cannot satisfy the uniform distribution, the searching of the fruit fly algorithm in the dimension is not uniform; thus, the fruit fly algorithm cannot effectively solve the complex optimization problem [16].

With this inspiration, the LGMS-FOA proposed by D. Shan in 2014 [16] expands the range of taste judgment values by introducing the LGMS mechanism. By doing so, the new taste judgment value satisfies the uniform distribution. The process of LGMS-FOA is shown as follows:

Step 1. The maximum number of iterations (*gen*max), population size (*popsize*), searching coefficient (n), initial weight (w_0), and weight coefficient (α) are initialized. Then, the location of the fruit fly population is defined.

$$x_axis = n \times rand(domain)$$
 (12)

where x_axis represents the searching center of the fruit fly population

Step 2. Each fruit fly is updated with a random search direction and distance by

$$x_i = x_axis + w \times rand(domian)$$
 (13)

$$w = w_0 \times \alpha^{gen} \tag{14}$$

where gen represents the current number of iterations.

Step 3. The taste decision value (*S*) of individual flies is calculated on the basis of LGMS.

$$S_i = x_i \tag{15}$$

Step 4. The taste decision value is substituted into the fitness function to calculate the corresponding fitness value (Smell).

$$Smell_i = fitness function(S_i)$$
 (16)

Step 5. The optimal fitness value (*bestsmell*) and corresponding location (*bestindex*) of the fruit fly individual are obtained by

$$[bestsmell, bestindex] = min(Smell)$$
 (17)

Step 6. The optimal fitness is set as the global optimal value (*gsmell*), and the corresponding location of the fruit fly is used as the searching center of the next iteration.

$$gsmell = bestsmell$$
 (18)

$$x_axis = x(bestindex)$$
 (19)

Step 7. Steps 2–6 are repeated until the terminal criterion is met or the maximum number of iterations is reached.

III. OLFOA

For the proposed OLFOA, on the basis of the LGMS, the orthogonal cross and quantum selection mechanism (OQSM) and simulated annealing strategies (SM) are employed to achieve good performance and highly stable convergence. The two mechanisms are presented below in details.

A. OQSM

1) QUANTUM BEHAVIOR MECHANISM

Quantum behavior mechanism [17] has been already used in quantum particle swarm optimization (QPSO) to improve the performance of the algorithm. In the original PSO, the velocity of the particles and the search space of each iteration are limited, which means that the searching area cannot cover the entire feasible searching space. Therefore, the PSO algorithm cannot guarantee the absolute convergence to the global optimal solution [18]. In the quantum space, particles with quantum motion characteristics can appear at any point in space with a certain probability and can reach the entire feasible solution space. As a result, the capability of the PSO algorithm to obtain the global optimum is greatly improved.

On the basis of the principle of quantum behavior, the locations of the particles are updated by

$$X_{r,j}(gen+1) = gbest_{r,j} \pm \frac{W(gen)}{2} \ln(\frac{1}{u(gen)})u \sim u(0,1)$$
(20)

where X means the location of particle, gbest means the best location of the particle in the last iteration, gen means the number of current iteration, r and j represent the number of individuals and the dimension of the locations, respectively. W means the probability that a particle will appear at a relative point and is expressed by the following formula:

$$W(gen) = 2\beta \cdot |mbest(gen) - X_{r,j}(gen)|$$
 (21)

where *mbest* means the mean value of the best position and is expressed by

$$mbest(gen) = \frac{1}{popsize} \sum_{r=1}^{popsize} gbest_r(gen)$$
 (22)

where *popsize* represents the population size. β in (21) means expansion-contraction factor and is expressed by

$$\beta = 0.5 \times (gen \max - gen)/gen \max + 0.5 \tag{23}$$

where *gen*max represents the maximum number of iterations.

The expansion-contraction factor is vital in the QPSO because it controls the convergence speed and search range of the particle. In QPSO, the expansion-contraction factor scales linearly and lacks flexibility. In this study, a weighting factor *wf* with values between 0 and 4 is introduced in

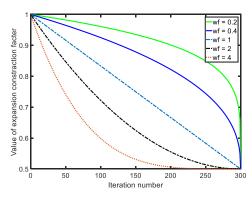


FIGURE 2. Expansion contraction factor versus iteration for different values of wf.

OLFOA. The adaptive expansion–contraction factor value is determined as follows, which replaces (23) in OLFOA.

$$\beta = 0.5 \times ((gen \max - gen)/gen \max)^{wf} + 0.5 \quad (24)$$

Fig. 2 shows the adaptive expansion-contraction factor versus iterations for different values of *wf*. The corresponding expansion-contraction factors have different convergence trends due to the different values of *wf*. A small *wf* value results in a slow convergence speed and a wide searching range. On the contrary, a large *wf* value leads to a fast convergence speed.

2) ORTHOGONAL DESIGN MECHANISM

As a multi-factor optimized experimental design method, the orthogonal design [19] introduces a series of orthogonal arrays for different numbers of factors and levels. The level represents the variable that affects the experimental results, whereas the factor represents the value of these variables. Different level and factor combinations will generate different samples and obtain different experimental results. The orthogonal crossover mechanism shows particular efficiency in handling the optimization problem, which doesn't require an exhaustive search over all the possible combinations to find the optimal solution.

By using orthogonal arrays, the levels and factors are rearranged in a certain order in accordance with the orthogonality, and only the most representative combinations are selected instead of calculating all possible combinations to find a suboptimal solution, thereby greatly reducing the computational burden. Specifically, the process of orthogonal crossover mechanism is established as follows:

I. Orthogonal array $L_M(Q^N)$ is selected for the orthogonal crossing, where L denotes a Latin square, Q and N denote the numbers of levels and factors, which are used for orthogonal crossing, respectively. M represents the number of combinations that is obtained by orthogonal crossing. Generally, a large number of M and Q will obtain good experiment results with an increase in the complexity. After numeral experiments, the $L_9(3^4)$ has been proven to be an efficient

TABLE 1. Orthogonal array $L_9(3^4)$.

Combination	Factor1	Factor2	Factor3	Factor4
1	1	1	1	1
2	1	2	2	2
3	1	3	3	3
4	2	1	2	3
5	2	2	3	1
6	2	3	1	2
7	3	1	3	2
8	3	2	1	3
9	3	3	2	1

orthogonal array by considering performance and calculation complexity [19]. Table 1 shows the orthogonal array $L_9(3^4)$.

In Table 1, each row represents a combination of different factors and levels. For example, the sixth combination consists of the Factor 1 of Level 2, Factor 2 of Level 3, Factor 3 of Level 1, and Factor 4 of Level 2. The combinations are the most representative candidates for all possible combinations.

The orthogonality of the orthogonal array is referred to the following: (1) for the factor in any column, each level occurs for the same number of times; (2) for the two factors in any two columns, each combination of two levels occurs for the same number of times; and (3) the selected combinations are uniformly distributed over the entire space of all possible combinations [19].

II. The three individuals belonging to the same experiment are divided into four factors:

$$E_1 = (e_{1,1}, e_{1,2}, e_{1,3}, e_{1,4})$$
 (25)

$$E_2 = (e_{2,1}, e_{2,2}, e_{2,3}, e_{2,4})$$
 (26)

$$E_3 = (e_{3,1}, e_{3,2}, e_{3,3}, e_{3,4})$$
 (27)

where E means the level of experiments and e means the factor of experiments.

III. Three individuals are taken into the orthogonal array $L_9(3^4)$ and nine combinations are obtained.

$$O_d = (e_{m_d,1}, e_{m_d,2}, e_{m_d,3}, e_{m_d,4}) \quad 1 \le d \le 9$$
 (28)

where O_d means the dth combination and m_d means the parameter determined by the orthogonal array.

B. SM

The simulated annealing algorithm [20] is originally designed to search the metal state with the lowest energy during metal temperature dropping, i.e., metal annealing process. To avoid the situation that the optimal state cannot be reached due to rapid cooling, the simulated annealing algorithm accepts the solution, which is worse than the current with a certain probability.

In the proposed OLFOA, the similar mechanism named simulated annealing mechanism (SM) is introduced. Specifically, if the current solution is better than the previous one, the SM does not work; otherwise, the current solution will be



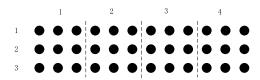


FIGURE 3. Diagram of division process.

still taken as the global optimum with a certain probability determined by SM.

C. OLFOA STEPS

With the improved mechanisms, the process of the OLFOA is described as follows:

Step 1. Initialization

The population size (popsize), searching coefficient (n), annealing temperature (T), final temperature (Tfin), maximum iteration number (gen max), and weighting factor (wf) are initialized. Then, the locations of the fruit fly swarm are initialized and updated as follows.

$$x = n \times rand(domain) \tag{29}$$

Step 2. Evaluation of the swarm

In this step, the *S* parameters of the fruit fly individual, which are calculated by LGMS, will be substituted into the objective function to obtain the smell values of the swarm. The optimal smell value is selected as the global optimal value (*gsmell*), and the corresponding fruit fly location is denoted as *gbest*.

$$S_i = x_i \tag{30}$$

$$Smell_i = fitness function(S_i)$$
 (31)

$$[gsmell, gbest] = min(Smell)$$
 (32)

Step 3. OQSM update of the swarm

The locations for each individual of the fruit fly population are calculated three times on the basis of (20), and the three locations are set as levels of orthogonal array. Each level is divided into four parts and set as four factors. To describe the division process visually, its diagram is presented as follows:

The *S* parameters of the individual flies are assumed to have 12 dimensions. Each black circle represents the S-parameter of each dimension of the fruit fly individuals. Each row represents a fruit fly individual, the vertical numbers represent the levels, and the horizontal numbers represent the factors respectively. As shown in Fig. 3, the taste decision value (*S*) of the three fruit fly individuals are divided into four equal parts (as equal as possible). Each of the divided parts is brought into Table 1 on the basis of its number of levels and factors, and nine new individuals are reconstituted after the crossover.

Then, the smell value of all nine combinations of fruit fly individuals can be obtained on the basis of the fitness function (31). The fruit fly individual corresponding to the best value of smell among the nine individuals will be selected

TABLE 2. Comparison algorithms.

Algorithm	Method	Authors and reference
FOA IFFO	Fruit fly optimization algorithm Improved fruit fly optimization	Pan et al. [15] Pan et al. [22]
IFFO	algorithm	ran et al. [22]
CMFOA	Chaotic fruit fly optimization algorithm	L. Wu et al. [23]
MSFOA	Multi-scale cooperative mutation fruit fly optimization algorithm	Y. Zhang et al. [24]
CEFOA	Co-evolution fruit fly optimization algorithm	X. Han et al. [25]
MFOA	Mixed modified fruit fly optimization algorithm	Pan et al. [26]
RMPSO	Repository and mutation-based particle swarm optimization	B. Jana et al.[27]
BLPSO	Biogeography-based learning particle swarm optimization algorithm	X. Chen et al. [28]
JADE	Adaptive differential evolution algorithm	J. Zhang et al. [29]
NGHS	Novel global harmony search algorithm	D. Zou et al. [30]

as the new fruit fly individual. Then, this process is repeated until the entire fruit fly swarm are updated.

Step 4. SM update of global optimum

Calculate the smell value of the updated fruit fly swarm. The best smell value (*bestsmell*) and corresponding location of the specific fruit fly (*bestindex*) is found:

$$[bestsmell, bestindex] = min(Smell)$$
 (33)

The SM triggering conditions are defined as follows:

$$\exp(-(bestsmell - gsmell)/T) > rand(0, 1)$$
 (34)

If the current *bestsmell* is better than the *gsmell*, or the *gsmell* and *bestsmell* meet the SM triggering conditions in (34), set *bestsmell* as the global optimal value (*gsmell*), and the corresponding location of specific fruit fly (*bestindex*) will be set as *gbest*.

Then, T is updated by

$$T = T - (T - Tfin)/(gen \max - gen)$$
 (35)

Step 5. Termination

Steps 3—4 is repeated until the maximum number of iterations is reached or the optimal value is found.

IV. EXPERIMENTS

In this section, OLFOA will be evaluated via the classical benchmark functions. The test results are compared with those of other improved algorithms to show the superior performance of the proposed OLFOA algorithm. Table 2 lists the improved algorithms in the experiments.

A. EXPERIMENTAL RESULTS

In this subsection, the capability of OLFOA is compared with the algorithms via 16 classic benchmark functions presented in Table 3. These algorithms are implemented by MATLAB 2016a and run on an i5 3.3 GHz CPU with 8 GB memory



TABLE 3. Benchmark functions.

ID	Function name	Equation	Global optimum	Domain
F1	Exponential problem	$f(x) = -\exp(-0.5\sum_{i=2}^{n} x_i^2)$	$x^* = 0$ and $f(x^*) = -1$	$-1 \le x_i \le 1$
F2	Quatic	$f(x) = \sum_{i=1}^{n} ix_i^4 + rand()$	$x^* = 0$ and $f(x^*) = 0$	$-5.12 \le x_i \le 5.12$
F3	Schwefels	$f(x) = \sum_{i=1}^{n} (\sum_{j=1}^{i} x_j)^2$	$x^* = 0$ and $f(x^*) = 0$	$-100 \le x_i \le 100$
F4	Schwefels 2.21	$f(x) = \max x_i , 1 \le i \le n$	$x^* = 0$ and $f(x^*) = 0$	$-100 \le x_i \le 100$
F5	Schwefels 2.22	$f(x) = \sum_{i=1}^{n} x_i + \prod_{i=1}^{n} x_i $	$x^* = 0$ and $f(x^*) = 0$	$-100 \le x_i \le 100$
F6	Sphere	$f(x) = \sum_{i=1}^{n} x_i^2$	$x^* = 0$ and $f(x^*) = 0$	$-100 \le x_i \le 100$
F7	Axis	$f(x) = \sum_{i=1}^{n} ix_i^2$	$x^* = 0$ and $f(x^*) = 0$	$-5.12 \le x_i \le 5.12$
F8	Shifted Sphere	$f(x) = \sum_{i=1}^{n} z_i^2 + f_bias$	$z = x - o, o =$ $(o_1, o_2,, o_n), x^* = 0$ $f(x^*) = f_bias$ $z = x - o, o =$	$-100 \le x_i \le 100$
F9	Shifted Schwefels 1.2	$f(x) = \sum_{i=1}^{n} (\sum_{j=1}^{i} z_j)^2 + f_{bias}$	$(o_1, o_2,, o_n), x^* = 0$ $f(x^*) = f_bias$	$-100 \le x_i \le 100$
F10	Ackley	$f(x) = -20 \exp(-0.2\sqrt{\frac{1}{n} \sum_{i=1}^{n} x_i^2})$ $-\exp(\frac{1}{n} \sum_{i=1}^{n} \cos(2\pi x_i)) + 20 + e$	$x^* = 0$ and $f(x^*) = 0$	$-32 \le x_i \le 32$
F11	Alpine	$f(x) = \sum_{i=1}^{n} x_i \sin x_i + 0.1x_i $	$x^* = 0$ and $f(x^*) = 0$	$-100 \le x_i \le 100$
F12	Griwank	$f(x) = \frac{1}{4000} \sum_{i=1}^{n} x_i^2 - \prod_{i=1}^{n} \cos(\frac{x_i}{\sqrt{t}}) + 1$	$x^* = 0$ and $f(x^*) = 0$	$-600 \le x_i \le 600$
F13	Cosine Wave	$f(x) = -\sum_{i=1}^{n-1} (\exp(-\frac{x_i^2 + x_{i+1}^2 + 0.5x_i x_{i+1}}{8}))$ $\times \cos(4\sqrt{x_i^2 + x_{i+1}^2 + 0.5x_i x_{i+1}})$	$x^* = 0$ and $f(x^*) = 1-n$	$-5 \le x_i \le 5$
F14	Neumaier 3 problem	$f(x) = \sum_{i=1}^{n} (x_i - 1)^2 - \sum_{i=2}^{n} x_i x_{i-1}$	$x^* = i(n+1-i)$ and $f(x^*) = -\frac{n(n+4)(n-1)}{6}$	$-n^2 \le x_i \le n^2$
F15	Rastrign	$f(x) = \sum_{i=1}^{n} (x_i^2 - 10\cos(2\pi x_i) + 10)$	$x^* = 0$ and $f(x^*) = 0$	$-5.12 \le x_i \le 5.12$
F16	Salomon	$f(x) = 1 - \cos(2\pi \sqrt{\sum_{i=1}^{n} x_i^2}) + 0.1 \sqrt{\sum_{i=1}^{n} x_i^2}$	$x^* = 0$ and $f(x^*) = 0$	$-100 \le x_i \le 100$

capacity. These algorithms are applied to minimize 16 benchmark functions with dimensions Dim = 30, 50. The population size is set as 80. In order to make a fair comparison, the maximum generation number is set to 300 for each function, which is consistent with the references. The experiment results are obtained by independently running 10 times for

fairness. The control parameters of all improved algorithms are set as the same as in [15] and [22]–[30]. In OLFOA, T is set as 900, T is set as 0.001×10^{-10} , and the weighting factor w is set as 0.4.

Table 4 shows the mean values and standard deviations of different fruit fly algorithms evaluated via numerical



TABLE 4. Results of algorithms on basic benchmark functions with dimension = 30, 50.

	Dim	F	71	I	72	F	3	I	7 4
		Mean	Std	Mean	Std	Mean	Std	Mean	Std
MFOA	30	-6.24E-2	2.34E-2	1.98E-3	1.05E-3	1.36E1	6.51	0.152	0.274
	50	-9.92E-1	1.86E-2	1.04E-2	1.16E-2	2.01E1	5.73	1.70	1.05
IFFO	30	-0.3674	0.5879	7.66E1	4.59E1	3.58E2	1.72E2	2.86E1	2.58E1
FOA	50 30	-5.68E-2 -9.54E-2	0.9113 2.16E-2	3.01E2 1.05E-7	2.29E2 1.77E-7	1.78E2 5.29E1	1.04E2 2.45	2.60E2 3.98E-2	1.79E2 4.46E-2
roa	50	-9.34E-2 -8.37E-2	2.86E-2	1.03E-7 1.21E-6	2.98E-6	5.07E1	2.44	2.10E-1	5.91E-1
MSFOA	30	-0.9999	9.14E-5	6.24E-8	6.55E-8	3.1462	4.5233	0.4139	0.4549
	50	-0.9999	9.03E-5	7.60E-7	7.96E-7	2.15E-8	2.20E-8	0.7171	4.17E-3
CMFOA	30	-0.9998	0.0001	3.35E-7	4.17E-7	0.0017	0.025	14.6682	15.3765
	50	-0.9906	0.036	6.53E-5	1.31E-5	0.0056	0.022	20.1622	11.2438
CEFOA	30	-1.00	0.00	1.2E-4	1.79E-4	7.92E-14	1.98E-14	1.98E-9	3.46E-8
	50	-1.00	0.00	9.52E-3	2.08E-4	1.02E-13	2.10E-12	4.99E-7	3.50E-7
OLFOA	30	-1.00	0.00	3.26E-3	3.68E-3	6.37E-1	5.13E-1	7.35E-10	2.84E-8
	50 D:	-1.00	0.00	7.78E-3	5.59E-3	5.35	7.56	3.26E-7	4.53E-6
	Dim	Mean F	Std	Mean	Std	Mean F	Std	Mean	Std
MEGA	20								
MFOA	30 50	4.74E-4 9.64E-4	2.56E-4 1.75E-3	1.97 2.07	1.09E-1 1.28E-1	2.82E1 2.01E1	5.07E1 5.27E1	-4.45E2 -4.45E2	5.45E1 5.45E1
IFFO	30	3.28E-1	1.58E-1	0.94	1.76E-1	2.01E1 2.25E1	5.63E1	-4.43E2 -4.43E2	3.38E-3
	50	0.5367	0.2219	2.56	1.16	1.50E2	3.12E2	-4.34E2	2.13E-1
FOA	30	1.03E2	4.26E2	1.05E-12	5.80E-1	8.64E1	1.45E1	-4.45E2	1.05E-1
	50	3.36E2	2.55E1	1.43E-11	4.26E-1	9.05E1	1.03E1	-4.41E2	4.33E-1
MSFOA	30	2.04E-5	2.39E-5	1.7160	1.7222	0.2159	0.2204	-448.26	1.8145
	50	2.46E-5	2.46E-5	2.1005	1.1212	0.787	0.588	-442.739	1.1184
CMFOA	30	0.0057	0.0078	0.0928	0.1	0.0269	0.0296	-449.916	0.0896
	50	0.0081	0.0114	0.1422	0.927	0.5809	0.5496	-442.976	0.1578
CEFOA	30	1.95E-28	2.08E-10	1.95E-12	2.08E-10	0.00	0.00	-450	0.00
OI FOA	50 30	1.02E-12	1.01E-6	1.95E-12	1.88E-10	0.00	0.00	-450	0.00
OLFOA	50	1.50E-7 3.25E-6	2.12E-7 8.19E-6	0.00	0.00	0.00	0.00	-450 -450	0.00
	50	3.23E 0	0.17E 0	0.00	0.00	0.00	0.00	450	0.00
	Dim	F	79	F	10	F.	11	F	12.
	Dim	Mean	Std	F Mean	10 Std	Mean	11 Std	F Mean	Std
MFOA	Dim 30								
MFOA		Mean	Std	Mean	Std	Mean	Std	Mean	Std
MFOA	30 50 30	Mean -4.44E2 -4.34E2 -4.35E2	3.67 2.58 4.57E-4	Mean 1.87E1 2.05E1 5.17E-1	Std 1.32E-1 3.45E-1 9.19E-1	Mean 2.65E-3 4.82E-2 1.1222	Std 4.22E-3 3.52E-2 2.56	Mean 1.89E2 3.63E2 1.52E-2	Std 4.31E1 5.31E1 2.75E-2
IFFO	30 50 30 50	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2	3.67 2.58 4.57E-4 4.70E-3	Mean 1.87E1 2.05E1 5.17E-1 3.2973	Std 1.32E-1 3.45E-1 9.19E-1 1.3559	Mean 2.65E-3 4.82E-2 1.1222 1.02E1	Std 4.22E-3 3.52E-2 2.56 2.76E1	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1	Std 4.31E1 5.31E1 2.75E-2 1.32E-2
	30 50 30 50 30	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.36E2	3.67 2.58 4.57E-4 4.70E-3 3.56	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1
IFFO	30 50 30 50 30 50	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.36E2 -4.35E2	3.67 2.58 4.57E-4 4.70E-3 3.56 1.16	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1	\$td 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1
IFFO	30 50 30 50 30 50 30	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.36E2 -4.35E2 -447.014	3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01
FOA	30 50 30 50 30 50 30 50 30	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.36E2 -4.35E2 -4.35E2 -447.014 -450	3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36
IFFO	30 50 30 50 30 50 30 50 30 50 30	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.36E2 -4.35E2 -4.47.014 -450 -449.18	3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759
FOA	30 50 30 50 30 50 30 50 30	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.36E2 -4.35E2 -4.35E2 -447.014 -450	3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36
IFFO FOA MSFOA CMFOA	30 50 30 50 30 50 30 50 30 50 30 50	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.36E2 -4.35E2 -447.014 -450 -449.18 -448.982	3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375
IFFO FOA MSFOA CMFOA	30 50 30 50 30 50 30 50 30 50 30 50 30	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.36E2 -4.35E2 -447.014 -450 -449.18 -448.982 -450 -450 -450 -450	3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 5.33E-4	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4
IFFO FOA MSFOA CMFOA CEFOA	30 50 30 50 30 50 30 50 30 50 30 50 30 50 30	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.35E2 -4.35E2 -447.014 -450 -449.18 -448.982 -450 -450 -450 -450	\$td 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 0.00	Mean 1.87E1 2.05E1 5.17E—1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E—10 1.32E-4 3.72E-2	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3
IFFO FOA MSFOA CMFOA CEFOA	30 50 30 50 30 50 30 50 30 50 30 50 30	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.36E2 -4.35E2 -447.014 -450 -449.18 -448.982 -450 -450 -450 -450 -450	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 0.00	Mean 1.87E1 2.05E1 5.17E—1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E—10 1.32E-4 3.72E-2	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3
IFFO	30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 50 50 30 50 50 50 50 50 50 50 50 50 50 50 50 50	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 13 Std	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2 14 Std	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std
IFFO FOA MSFOA CMFOA CEFOA	30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 50 30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 0.00 13 Std 6.11E-1	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 5.33E-4 7.28E-2 14 Std 2.41E5	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 Mean 1.60E-4	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 Std 2.27E-3	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2
IFFO	30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 30 50 50 30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 0.00 13 Std 6.11E-1 5.51E-1	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2 14 Std 2.41E5 1.41E5	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 Fi Mean 1.60E-4 6.11E-4	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2 2.74E-2
IFFO	30 50 50 30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 0.00 13 Std 6.11E-1 5.51E-1 1.15E-1	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5 3.15E3	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2 14 Std 2.41E5 1.41E5 6.29E2	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 Fi Mean 1.60E-4 6.11E-4 3.15E2	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3 2.98E2	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1 2.63	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2 2.74E-2 1.75
IFFO	30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 13 Std 6.11E-1 5.51E-1 1.15E-1 2.65E-1	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5 3.15E3 2.265E2	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2 14 Std 2.41E5 6.29E2 5.56E2	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 Fi Mean 1.60E-4 6.11E-4 3.15E2 4.18E3	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3 2.98E2 1.69E3	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1 2.63 2.44	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2 2.74E-2 1.75 2.71
IFFO	30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 13 Std 6.11E-1 5.51E-1 1.15E-1 2.65E-1 0.71	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5 3.15E3 2.265E2 1.24E6	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 5.33E-4 7.28E-2 14 Std 2.41E5 1.41E5 6.29E2 5.56E2 6.60E5	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 Mean 1.60E-4 6.11E-4 3.15E2 4.18E3 2.76E1	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3 2.98E2 1.69E3 3.20E1	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1 2.63 2.44 4.06E-1	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2 1.75 2.71 7.73E-3
IFFO	30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 13 Std 6.11E-1 5.51E-1 1.15E-1 2.65E-1	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5 3.15E3 2.265E2	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2 14 Std 2.41E5 6.29E2 5.56E2	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 Fi Mean 1.60E-4 6.11E-4 3.15E2 4.18E3	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3 2.98E2 1.69E3	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1 2.63 2.44	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2 2.74E-2 1.75 2.71
IFFO	30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 0.00 13 Std 6.11E-1 5.51E-1 1.15E-1 2.65E-1 0.71 0.98	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5 3.15E3 2.265E2 1.24E6 1.68E6	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2 14 Std 2.41E5 1.41E5 6.29E2 5.56E2 6.60E5 3.98E5	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 Mean 1.60E-4 6.11E-4 3.15E2 4.18E3 2.76E1 4.12E2	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3 2.98E2 1.69E3 3.20E1 2.89E1	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1 2.63 2.44 4.06E-1 4.76E-1	\$td 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 \$td 2.24E-2 2.74E-2 1.75 2.71 7.73E-3 7.60E-3
IFFO	30 50 50 30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 13 Std 6.11E-1 5.51E-1 1.15E-1 2.65E-1 0.71 0.98 7.15E-2	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5 3.15E3 2.265E2 1.24E6 1.68E6 15.9872	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 5.33E-4 7.28E-2 14 Std 2.41E5 1.41E5 6.29E2 5.56E2 6.60E5 3.98E5 4.95E3	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 Mean 1.60E-4 6.11E-4 3.15E2 4.18E3 2.76E1 4.12E2 0.882	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3 2.98E2 1.69E3 3.20E1 2.89E1 9.00E-01	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1 2.63 2.44 4.06E-1 4.76E-1 0.1965	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2 1.75 2.71 7.73E-3 7.60E-3 1.97E-01 1.97E-01
IFFO	30 50 50 30 50 50 50 50 50 50 50 50 50 5	Mean -4.44E2 -4.34E2 -4.35E2 -4.15E2 -4.36E2 -4.36E2 -4.47.014 -450 -449.18 -448.982 -450 -450 -450 -450 -5.57 -6.02 -17.25 -13.99 -6.09 -6.57 -28.9297 -48.864 -23.0247 -38.6263	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 0.00 13 Std 6.11E-1 5.51E-1 1.15E-1 2.65E-1 0.71 0.98 7.15E-2 1.37E-1	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5 3.15E3 2.265E2 1.24E6 15.9872 15.9872	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 5.33E-4 7.28E-2 14 Std 2.41E5 1.41E5 6.29E2 5.56E2 6.60E5 3.98E5 4.95E3 4.95E3	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 Final Mean 1.60E-4 6.11E-4 3.15E2 4.18E3 2.76E1 4.12E2 0.882 1.635	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3 2.98E2 1.69E3 3.20E1 2.89E1 9.00E-01 4.37E-01 0.3368 1.1627	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1 2.63 2.44 4.06E-1 4.76E-1 0.1965 0.3122	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2 1.75 2.71 7.73E-3 7.60E-3 1.97E-01 1.16E-01
IFFO	30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 13 Std 6.11E-1 2.65E-1 0.71 0.98 7.15E-2 1.37E-1 6.1269 10.5073 1.05 1.05	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5 3.15E3 2.265E2 1.24E6 1.68E6 15.9872 15.9872 827.128 931.128 -1.89E4 1.89E4 1.89E4	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2 14 Std 2.41E5 6.29E2 6.60E5 3.98E5 4.95E3 4.95E	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 F1 Mean 1.60E-4 6.11E-4 3.15E2 4.18E3 2.76E1 4.12E2 0.882 1.635 0.3156 2.2025 9.46E-8	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3 2.98E2 1.69E3 3.20E1 2.89E1 9.00E-01 4.37E-01 0.3368 1.1627 4.42E-8	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1 2.63 2.44 4.06E-1 4.76E-1 0.1965 0.3122 1.4198 1.0772 0.00	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2 1.75 2.71 7.73E-3 7.60E-3 1.97E-01 1.16E-01 1.4512 1.7336 0.00
IFFO FOA MSFOA CEFOA OLFOA IFFO FOA MSFOA CMFOA CEFOA	30 50 50 30 50 50 30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 13 Std 6.11E-1 5.51E-1 1.15E-1 2.65E-1 0.71 0.98 7.15E-2 1.37E-1 6.1269 10.5073 1.05 1.52	Mean 1.87E1 2.05E1 5.17E—1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E—10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5 3.15E3 2.265E2 1.24E6 1.68E6 15.9872 15.9872 827.128 931.128 -1.89E4 -1.69E4	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2 14 Std 2.41E5 1.41E5 6.29E2 5.56E2 6.60E5 3.98E5 4.95E3 4103.259 3357.637 3.60E3 2.64E3	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 Mean 1.60E-4 6.11E-4 3.15E2 4.18E3 2.76E1 4.12E2 0.882 1.635 0.3156 2.2025 9.46E-8 1.06E-8	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3 2.98E2 1.69E3 3.20E1 2.89E1 9.00E-01 4.37E-01 0.3368 1.1627 4.42E-8 2.27E-8	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1 2.63 2.44 4.06E-1 4.76E-1 0.1965 0.3122 1.4198 1.0772 0.00 0.00	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2 2.74E-2 1.75 2.71 7.73E-3 7.60E-3 1.97E-01 1.16E-01 1.4512 1.7336 0.00 0.00
IFFO	30 50 50 50 50 50 50 50 50 50 5	Mean	Std 3.67 2.58 4.57E-4 4.70E-3 3.56 1.16 3.1573 1.24E-08 0.0335 0.04273 0.00 0.00 0.00 13 Std 6.11E-1 2.65E-1 0.71 0.98 7.15E-2 1.37E-1 6.1269 10.5073 1.05 1.05	Mean 1.87E1 2.05E1 5.17E-1 3.2973 1.26E1 3.02E1 0.5921 0.6491 0.1205 0.4475 1.60E-10 1.32E-4 3.72E-2 F Mean 7.30E5 2.46E5 3.15E3 2.265E2 1.24E6 1.68E6 15.9872 15.9872 827.128 931.128 -1.89E4 1.89E4 1.89E4	Std 1.32E-1 3.45E-1 9.19E-1 1.3559 5.01E-1 1.05E-1 5.98E-01 7.11E-01 0.1235 0.4387 4.01E-10 2.13E-10 5.33E-4 7.28E-2 14 Std 2.41E5 6.29E2 6.60E5 3.98E5 4.95E3 4.95E	Mean 2.65E-3 4.82E-2 1.1222 1.02E1 4.15E1 3.99E1 0.0536 0.1741 0.1313 0.4520 9.15E-14 1.05E-13 2.87E-20 2.21E-16 F1 Mean 1.60E-4 6.11E-4 3.15E2 4.18E3 2.76E1 4.12E2 0.882 1.635 0.3156 2.2025 9.46E-8	Std 4.22E-3 3.52E-2 2.56 2.76E1 1.58 1.38 5.42E-02 1.56E-01 0.1536 0.5165 1.55E-12 1.95E-13 5.91E-18 4.39E-15 15 Std 2.27E-3 1.50E-3 2.98E2 1.69E3 3.20E1 2.89E1 9.00E-01 4.37E-01 0.3368 1.1627 4.42E-8	Mean 1.89E2 3.63E2 1.52E-2 5.11E-1 5.07E1 6.89E1 0.9661 1.6335 0.2594 33.1151 8.89E-16 1.09E-15 6.44E-4 7.17E-3 F Mean 2.98E-1 4.00E-1 2.63 2.44 4.06E-1 4.76E-1 0.1965 0.3122 1.4198 1.0772 0.00	Std 4.31E1 5.31E1 2.75E-2 1.32E-2 1.70E1 1.11E1 9.67E-01 1.36 0.2759 40.7375 4.70E-15 8.70E-14 2.82E-4 8.33E-3 16 Std 2.24E-2 1.75 2.71 7.73E-3 7.60E-3 1.97E-01 1.16E-01 1.4512 1.7336 0.00

benchmark functions with dimensions of 30 and 50. OLFOA exhibits computational benefit and superior performance compared with FOA, MFOA, IFFO, and CMFOA. OLFOA performed better than MSFOA and CEFOA with a faster

convergence speed for most of the benchmark functions (F1, F4, F6, F7, F8, F9, F11, and F15), whereas it does not show outstanding performance compared to MSFOA in F2 and F13. Compared with CEFOA, the OLFOA does not



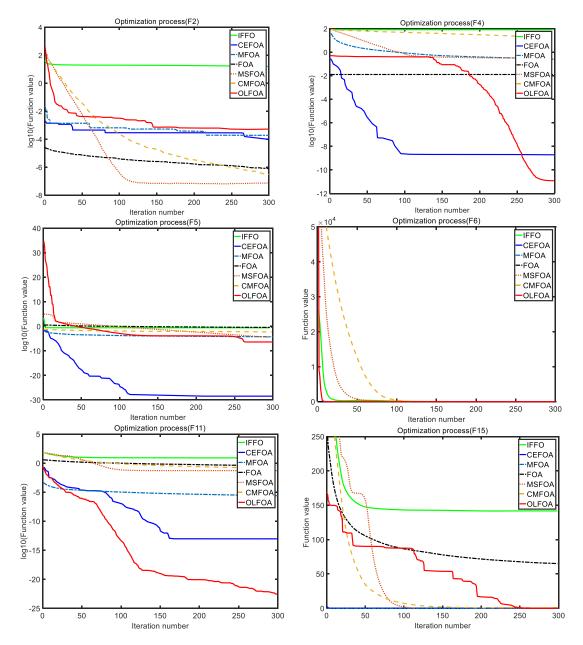


FIGURE 4. Convergence curve of multimodal functions for different algorithms with dimension = 30.

work well in F3, F5, F10, F12, F14 and F16. Thus, conclusion can be drawn that the proposed OLFOA prevails over other algorithms for most of the benchmark functions. In the case with a dimension of 50, similar results have been acquired except both the mean value and standard deviation of all algorithms have certain deterioration.

B. CONVERGENCE ANALYSIS

To describe the convergence performance of the algorithms visually, Figs. 4 and 5 provide the average convergence results of randomly selected test functions (F2, F4, F5, F6, F11, and F15) after 300 iterations with dimensions of 30 and 50, respectively. The dB fitness value is used and displayed

in the *y-axis* of the figures in the optimization of F2, F4, F5, and F11. Only for benchmark functions F2 and F5, OLFOA does not show outstanding performance compared to other algorithms in terms of the convergence and optima. However, for the other unimodel benchmark functions, OLFOA shows its obvious advantage in stability and efficiency in acquiring the global optimum, especially for benchmark functions F11 and F15. For benchmark functions F4 and F6, OLFOA obtained the best fitness value and showed a fast convergence speed. These results indicate that the proposed OLFOA algorithm outperforms numerous improved FOA methods (IFFO, CEFOA, CMFOA, MFOA, and MSFOA) and the original FOA in global optimum and convergence capability.



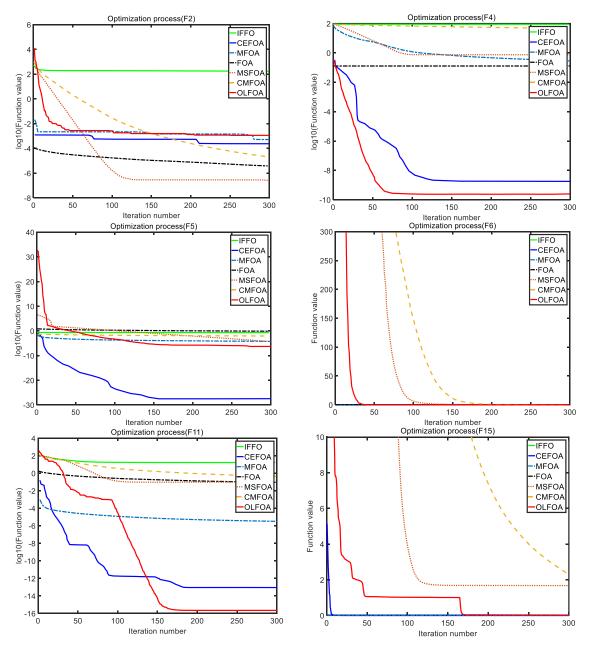


FIGURE 5. Convergence curve for multimodal functions with dimension = 50.

C. EXTRA EXPERIMENTAL RESULTS

Considering the array synthesis application of the proposed algorithm has a specific range of [0, 1], it is necessary to carry out tests on benchmark functions in the specific range for further performance verification. In this subsection, OLFOA is compared with CEFOA, and the recently proposed improved FOAs in Table 5. The search space of fruit fly individuals are set as [0,1].

Table 6 shows the mean value and the standard deviation of those FOAs for different benchmark functions in the range of [0, 1] with a dimension of 30. Conclusion can be drawn that the performance of CEFOA deteriorates severely when applied in such test functions, whereas the proposed OLFOA

TABLE 5. Comparison algorithms in extra tests.

Algorithm	Method	Authors and reference		
AE-LGMS- FOA	Averager engine linear generation mechanism of candidate solution of FOA	A. Darvish et al. [21]		
IFOA	Improved fruit fly algorithm	Xu et al. [31]		

obtains better and more stable results when compared with other improved FOA algorithms.

D. COMPARISON WITH OTHER ALGORITHMS

In this subsection, OLFOA is compared with other different types of improved algorithms (RMPSO, BLPSO, JADE, and



CEFOA

	Dim	F	1	F	2	F	3	F	4
		Mean	Std	Mean	Std	Mean	Std	Mean	Std
AE-LGMS- FOA	30	-1.04E-1	3.57E-2	3.31E-2	7.76E-2	4.49	3.36	7.95E-4	1.54E-4
IFOA	30	-2.19E-1	4.10E-2	3.54E-2	1.82E-2	3.18	2.68	6.68E-6	2.97E-6
CEFOA	30	-0.51	3.27E-1	232.5	6.77E-1	7.54E5	8.82E-5	0.7	5.99E-4
OLFOA	30	-1	0.00	2.9E-3	1.78E-3	9.37E-1	3.34E-1	5.27E-9	3.75E-8
	Dim	F	5	F	6	F	7	F	8
		Mean	Std	Mean	Std	Mean	Std	Mean	Std
AE-LGMS- FOA	30	5.96E-7	8.58E-6	5.46E-23	4.14E-23	3.33E-25	4.90E-25	-4.49E2	9.12E-14
IFOA	30	6.68E-6	2.85E-6	8.82E-26	2.65E-26	6.47E-27	3.43E-26	-4.49E2	2.05E-17
CEFOA	30	20	2.79E-2	15	1.02E-15	4.2E3	5.87E-3	-4.35E2	6.65E-24
OLFOA	30	1.87E-15	2.5E-14	0.00	0.00	0.00	0.00	-450	0.00
	Dim	F	79	F10		F11		F12	
		Mean	Std	Mean	Std	Mean	Std	Mean	Std
AE-LGMS- FOA	30	-4.49E2	7.14E-9	3.98E-7	9.66E-6	5.68E-11	4.89E-10	2.69E-23	6.77E-23
IFOA	30	-4.48E2	5.31E-12	7.29E-9	4.47E-7	2.74E-12	2.78E-10	7.32E-21	5.02E-21
CEFOA	30	-4.35E2	8.83E-30	3.57	5.14E-1	4.04E-4	1.91E-4	5.45E-1	1.46E-2
OLFOA	30	-450	0.00	3.64E-14	1.12E-14	5.74E-20	1.32E-18	0.00	0.00
	Dim	F	13	F	15	F16			
		Mean	Std	Mean	Std	Mean	Std		
AE-LGMS- FOA	30	-28.57	2.12E-3	4.98E-4	5.79E-3	4,63E-1	4.24E-1		

4.06E2

8.00E1

TABLE 6. Results of extra basic benchmark functions with dimension = 30.

NGHS) to justify its performance. The parameter settings are the same as those in Part A of Section IV.

-23.84

7.87E-9

30

Table 7 shows the mean value and standard deviation of those algorithms for different benchmark functions with dimensions of 30 and 50. Obviously, OLFOA exhibits its superior advantage in global optimum and convergence stability when compared with RMPSO, BLPSO, and JADE. When compared with NGHS, OLFOA performs better for most of the benchmark functions (F1, F2, F4, F5, F6, F7, F8, F9, F10, F11, F12, F13, F15, and F16) with fast and stable convergence speed, whereas OLFOA does not show competitive performance advantage compared to NGHS for F3 and F14.

From all these results and analysis above, conclusions can be drawn below:

- 1) OLFOA obtains much more superior values among all the algorithms in most cases. OLFOA can achieve excellent results with high stability in different dimensional and population problems.
- 2) OLFOA shows a strong local search capability and stable convergence rate among most of the algorithms.
- 3) OLFOA can demonstrate its competitive advantage in the benchmark tests in the range of [0, 1], which exactly corresponds to the application considered later in this paper.

V. OLFOA APPLICATION

In this section, OLFOA is applied into several different subarray phased array synthesis problems to prove its performance. In the simulation, the excitation of each subarray element is set as one dimension of the individual fruit fly, and the

excitation of the entire subarray antenna element constitutes the location of individual fruit fly, the number of the swarm is set as 80, T is set as 900, T in is set as 0.001 \times 10⁻¹⁰, the weighting factor w is set as 0.4, and the maximum iteration number is set as 100.

3.05E-1

A. ANTENNA ARRAY NOTATION

6.28E-1

Considering a planar array antenna with N rows and M columns of elements arranged in a rectangular grid in the x-and y-axis, then the radiation pattern of planar array can be expressed as:

$$FF(\theta, \varphi) = \sum_{n=1}^{N} \sum_{m=1}^{M} I_{mn} f_{mn}(\theta, \varphi) \times e^{-j(kd_{xmn} \sin \theta \cos \varphi + kd_{ymn} \sin \theta \sin \varphi + \phi_{mn})}$$
(36)

where I_{mn} is the element excitation current amplitude, ϕ_{mn} is the element excitation current phase, $f_{mn}(\theta, \varphi)$ is the array element pattern, d_{xmn} and d_{ymn} are the distance from array element to axis origin in x-and y-axis respectively.

Put this array antenna into the subarray tiling and each subarray consists of C elements. Then the maximum number of subarrays (L) that can be used to tile the entire aperture is $L = N \cdot M/C[2]$. If the shape of the subarray is the same, after rotating and folding, eight different shapes exist on the array aperture. Furthermore, if the subarray is symmetrical, the subarray shapes are reduced to four or even two [3].

In this study, the subarray tiling method based on X algorithm [7] is adopted to achieve the exact partition of subarrays on the array aperture. After the exact partition, the radiation



TABLE 7. Results of five algorithms on basic benchmark functions with dimension = 30, 50.

	Dim	F1		I	72	F	73	I	74
		Mean	Std	Mean	Std	Mean	Std	Mean	Std
RMPSO	30	-1.04E-3	2.15E-2	2.18	1.59	5.93	1.46	1.709E-1	4.51E-1
	50	-7.15E-2	3.733E-2	1.87E1	2.13E1	8.19E1	4.51E1	1.93	4.74
BLPSO	30	-6.47E-2	1.04E-2	3.54E-2	2.80E-2	2.10E-1	3.08E-2	8.13E-1	2.65E-1
	50	-5.72E-2	3.54E-2	2.99E-2	1.96E-2	2.04E-1	2.87E-2	5.24E-1	2.85E-1
JADE	30	-3.57E-1	3.12E-1	4.27E-2	5.19E-2	8.54E-1	2.97E-2	6.07E-4	2.48E-4
	50	-3.14E-1	2.92E-1	3.86E-2	4.24E-2	7.11E-1	2.49E-2	5.67E-4	1.98E-4
NGHS	30	-1.03E-4	4.47E-5	7.48E-3	2.04E-3	2.80E-6	3.16E-6	1.44E-4	1.29E-3
	50	-1.01E-4	2.15E-5	5.22E-3	1.09E-3	3.02E-6	2.92E-6	1.04E-4	7.20E-4
OLFOA _	30	-1.00	0.00	3.26E-3	3.68E-3	6.37E-1	5.13E-1	7.35E-10	2.84E-8
	50	-1.00	0.00	7.78E-3	5.59E-3	5.35	7.56	3.26E-7	4.53E-6
	Dim		`5		76		7		78
		Mean	Std	Mean	Std	Mean	Std	Mean	Std
RMPSO	30	3.71E-1	5.48E-1	6.67E-1	1.44	5.78E-1	2.26E-1	-4.41E2	3.72E-4
	50	6.35	4.42	1.92	1.77	3.56	1.85	-4.23E2	1.36E-4
BLPSO	30	1.12E-1	5.29E-2	1.78E-4	4.22E-4	2.88E-4	5.60E-3	-4.40E2	1.41E-3
	50	1.08E-1	6.19E-2	1.25E-4	3.59E-4	1.93E-4	5.11E-3	-4.40E2	1.05E-3
JADE	30	1.12E-1	5.29E-2	1.78E-4	4.22E-4	2.88E-4	5.60E-3	-4.43E2	3.89E-1
	50	1.17E-5	3.51E-5	1.19E-5	3.08E-6	5.70E-5	2.03E-5	-4.33E2	2.94E-1
NGHS	30	4.55E-7	3.24E-6	6.99E-8	3.18E-8	1.50E-6	8.62E-8	-4.42E2	1.06E-1
OT FO	50	2.44E-7	2.28E-6	6.14E-8	1.27E-8	9.12E-7	7.29E-8	-4.40E2	1.01E-1
OLFOA _	30	1.50E-7	2.12E-7	0.00	0.00	0.00	0.00	-450	0.00
	50	3.25E-6	8.19E-6	0.00	0.00	0.00	0.00	-450	0.00
	Dim	Mean F	Std	Mean	10 Std		11 Std		12 Std
						Mean		Mean	
RMPSO	30	-4.32E2	3.13E-1	4.47E-2	6.69E-2	8.23E-1	8.46E-1	9.82	6.77
DI DOO	50	-4.25E2	2.35E-1	5.89	4.61	6.03E-1	2.73E-1	1.35E1	1.22E1
BLPSO	30	-4.41E2	1.35E-2	9.27E-3	2.27E-3	4.06E-2	1.41E-1	7.32E-2	5.02E-2
LADE	50	-4.40E2	1.24E-08	7.19E-3	5.98E-01	3.41E-2	5.42E-02	5.32E-2	9.67E-01
JADE	30 50	-4.33E2 -4.36E2	5.70E-1 5.10E-1	8.06E-1 7.43E-1	5.14E-1 4.58E-1	3.78E-2 3.20E-2	1.79E-2 1.51E-2	5.45E-1 3.75E-1	1.46E-2 1.11E-2
NGHS	30	-4.36E2 -4.45E2	1.00E-2	2.56E-3	4.58E-1 3.80E-3	3.20E-2 7.01E-4	4.11E-4	3.75E-1 3.22E-2	1.11E-2 1.12E-2
110115	50	-4.44E2	1.04E-2	2.77E-3	2.63E-3	8.54E-4	2.71E-4	3.02E-2	1.02E-2
OLFOA	30	-450	0.00	1.32E-4	5.33E-4	2.87E-20	5.91E-18	6.44E-4	2.82E-4
	50	-450	0.00	3.72E-2	7.28E-2	2.21E-16	4.39E-15	7.17E-3	8.33E-3
	Dim		13		14		15		16
	Dini	Mean	Std	Mean	Std	Mean	Std	Mean	Std
RMPSO	30	-2.33	4.66	2.54E5	1.151E4	4.77E1	7.82E1	3.54E-1	2.44E-1
	50	-1.51	6.57	2.76E5	2.51E4	5.12E2	4.43E2	8.98E-1	4.89E-1
BLPSO	30	-1.24	2.45	8.75E4	3.67E4	3.27	3.07E-01	2.71E-2	1.89E-2
	50	-1.15	1.59	7.05E4	3.13E4	2.18	1.53E-1	2.0E-2	1.80E-2
JADE	30	-5.05	1.23	4.22E3	7.23E3	4.06E2	8.00E1	6.28E-1	3.05E-1
_	50	-4.84	1.2	3.11E3	5.03E3	3.54E2	4.12E1	3.14E-1	3.51E-1
NGHS	30	-6.00	1.07E-1	1.05E3	3.91E3	4.80E-2	1.46E-2	2.48E-2	9.22E-3
	50	-6.22	8.25E-2	8.12E2	4.58E3	4.87E-2	7.23E-3	2.08E-2	1.29E-2
	30	-27.7434	1.56E-3	1.08E5	2.26E5	6.60E-8	8.85E-7	5.13E-3	4.45E-3
OLFOA	30	-41.1737	1.5015-5	1.000				J.1JL J	

pattern of the subarray antenna can be expressed as

$$FF(\theta,\varphi) = \sum_{l=0}^{L} I_{l}^{sub} e^{-j\phi_{l}} \sum_{\{m,n|l_{mn}=l\}} I_{mn}^{ele} f_{mn}(\theta,\varphi) e^{-j\phi_{mn}}$$

$$\times e^{-j(kd_{xmn}\sin\theta\cos\varphi + kd_{ymn}\sin\theta\sin\varphi)}$$
(37)

where I_l^{sub} is the normalized subarray excitation current amplitude, I_{mn}^{ele} is the normalized element excitation current amplitude, ϕ_l is the subarray excitation current phase, $\{m, n | l_{mn} = l\}$ is the set of antenna elements longing to the lth subarray, ϕ_l is the element excitation current phase.

For engineering practicality, the optimization object of subarray antenna array synthesis problems is set as the subarray excitation current amplitude (I_l^{sub}), which ranges from 0 to 1. The optimization target is the maximum sidelobe level of the antenna pattern. The fitness function can be expressed

as:

$$Fitness = \underset{(\theta, \varphi) \in FF_S}{abs} \left(\frac{FF}{\max(FF)} \right)$$
 (38)

where FF_S represents the area of sidelobe.

B. RESULTS OF ARRAY SYNTHESIS

The first synthesis case is a 40-element array (5 \times 8) with half-wavelength spacing, and a rectangular subarray consisting of two connected elements is desired [6], as shown in Fig. 6. Fig. 7 presents the far-field radiation pattern of the arrays optimized after 100 iterations, and the corresponding PSL is -23.46 dB, which is 4.57 dB lower than that in [6].

Arrays of 128 (8 \times 16) and 432 (18 \times 24), with inter-element spacing of half-wavelength, are considered in the second and the third synthesis cases, respectively.



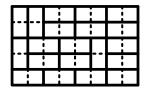


FIGURE 6. Structures of 5×8 array tiling optimized with X algorithm.

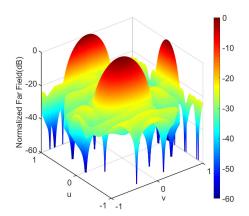


FIGURE 7. Radiation pattern for the arrays optimized with OLFOA.

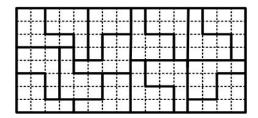


FIGURE 8. Structures of 8 \times 16 array tiling optimized with $\it X$ algorithm.

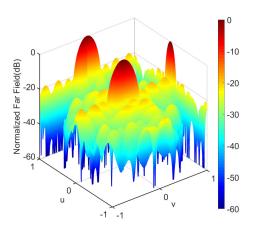


FIGURE 9. Radiation pattern for the arrays optimized with OLFOA.

A subarray with an L-octomino shape consisting eight connected elements is desired. Fig. 8 and 10 show the acceptable exact partition of the aperture by using the X algorithm. Fig. 9 and 11 present the far-field radiation patterns of the arrays optimized by OLFOA after 100 iterations. The corresponding PSL for these two arrays are -19.98 and -30.64 dB, respectively.

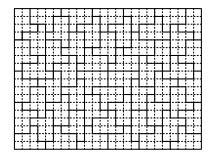


FIGURE 10. Structures of 18×24 array tiling optimized with X algorithm.

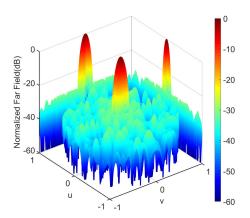


FIGURE 11. Radiation pattern for the arrays optimized with OLFOA.

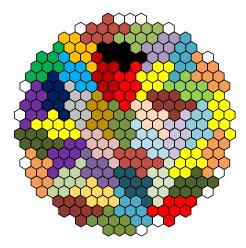


FIGURE 12. Structures of circular aperture array tiling optimized with the X algorithm.

The fourth case is a 349-element circular aperture array with half-wavelength spacing. The subarray consists of eight connected polyhex-shaped elements. As shown in Fig. 12, the array is divided into 55 subarrays by the *X* algorithm (including 42 eight-element polyhex-shaped subarrays and 13 independent elements) [7]. The subarray partition and the beam pointing of the array are set to be the same as in [7]. Fig. 13 displays the far-field radiation pattern of the arrays optimized after 100 iterations, and the corresponding *PSL* is -30.76dB. This optimization result is 3.56dB lower than the maximum sidelobe achieved in [7], which indicates the



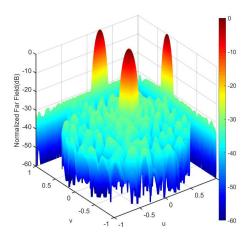


FIGURE 13. Radiation pattern for the arrays optimized with OLFOA.

TABLE 8. Performance comparison of different subarray antennas synthesized by different methods of three algorithms.

Synthesis	PSL (dB)						
case	Case 1	Case 2	Case 3	Case 4			
Uniform excitation	-12.05	-13.17	-13.29	-17.34			
LGMS- FOA [16]	-21.97	-17.19	-26.45	-25.47			
AE- LGMS- FOA [21]	-22.63	-18.68	-28.28	-27.89			
GA	-19.26	-15.74	-24.5	-24.14			
DE	-18.13	-16.61	-25.1	-23.43			
QPSO [17]	-18.64	-16.79	-24.4	-23.85			
OLFOA	-23.46	-19.98	-30.64	-30.76			

superiority of the proposed algorithm when applied in the design of irregular subarray antennas.

Table 8 presents the comparison results in terms of *PSL* optimized by those different algorithms under four irregular subarray cases. For fair comparison, the parameters of the other algorithms are set the same as those of the proposed algorithm. From Table 8, conclusion can be drawn that the proposed OLFOA shows the superior *PSL* performance when compared with the other algorithms for all these cases.

VI. CONCLUSION

In this paper, an advanced fruit fly optimization algorithm, namely, OLFOA has been proposed. Individuals are selected in a highly balanced way by adding the OQSM and SM mechanisms. The population diversity, global searching capability, and ability to escape from the local optimum of the algorithm are significantly improved. The OLFOA has been tested via numerous classical benchmark functions in comparison with other improved FOAs and advanced algorithms to demonstrate its capability. Then, OLFOA is applied to synthesize four different cases of subarray antenna array of planar and circular aperture. Simulation results show that the proposed algorithm presents a superior performance both in benchmark function test and the subarray antenna array synthesis problems.

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