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# Technology Computer Aided Design Study of GaN MISFET With Double P-Buried Layers

YING WANG<sup>1</sup>, (Senior Member, IEEE), MENG-TIAN BAO<sup>1</sup>,  
FEI CAO<sup>1</sup>, JIAN-XIANG TANG<sup>1</sup>, AND XIN LUO<sup>2</sup>

<sup>1</sup>Key Laboratory of RF Circuits and Systems, Ministry of Education, Hangzhou Dianzi University, Hangzhou 310018, China

<sup>2</sup>National Institute of LED on Silicon Substrate, Nanchang University, Nanchang 330047, China

Corresponding author: Fei Cao (caofei@hdu.edu.cn)

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**ABSTRACT** In this paper, a performance-improved AlGaIn/GaN-Based metal-insulator-semiconductor field effect transistor (MISFET) with double P-buried layers MISFET (DP-MISFET) is proposed. The proposed structure is simulated, and its characteristics are analyzed by the Sentaurus TCAD tool; the results show that with a gate-drain spacing of  $6 \mu\text{m}$ , the optimized DP-MISFET can achieve high Baliga's figure of merit of  $3.23 \text{ GW} \cdot \text{cm}^{-2}$  due to the modulation of the electric field distribution. Compared with the conventional MISFET (C-MISFET) with the breakdown voltage (BV) of 503.9 V and specific on-resistance ( $R_{\text{on,sp}}$ ) of  $0.63 \text{ m}\Omega \cdot \text{cm}^2$ , the proposed structure can achieve a better trade-off between the breakdown voltage and specific on-resistance achieving  $R_{\text{on,sp}}$  and BV of  $0.63 \text{ m}\Omega \cdot \text{cm}^2$  and 1427 V, respectively.

**INDEX TERMS** P-buried layers, GaN, MISFET, Sentaurus TCAD, figure of merit.

## I. INTRODUCTION

Over the past decades, the AlGaIn/GaN-Based metal-insulator-semiconductor field effect transistors (MISFETs) have been attracting much attention [1]–[8] due to their excellent features, such as great properties of gallium nitride materials [9] and high electron density of a two-dimensional electron gas (2DEG) from the polarization effect [10]. Moreover, GaN HEMTs have been recognized as excellent devices for the fabrication of high efficiency power converters, since they can have very low ON-resistance, high switching speed, and high breakdown voltage [11]. However, achieving a high breakdown voltage (BV) at a low on-resistance ( $R_{\text{on}}$ ) is still challenging. Over the years, many scholars and researchers have done a lot of researches to improve the characteristics of the MISFETs. For example, the field plate (FP) devices such as uniform field plates [12], multiple field plates [13], source-drain field plates [14], and floating field plates [15] were proposed to reduce the electric field peak at the gate edge and achieve the multiple electric field peaks between the gate and drain. Karmalkar *et al.* [16] and Duan and Yang [17] adopted the reduced surface field (RESURF) concept [18] to achieve a high breakdown voltage. The Fe-doped [19]–[21]

and C-doped [22]–[24] technologies were also proposed to reduce the buffer leakage current.

Luo *et al.* used the P-buried layer technology to improve the breakdown voltage [25]. In the proposed SC-PBL FPs MISFET structure, the P-buried layer could fully deplete the 2DEG in channel and improve the breakdown voltage significantly. However, the P-buried layer also increased the specific on-resistance ( $R_{\text{on,sp}}$ ) and reduced the maximum saturation current due to the decrease in 2DEG density of the channel, which degraded the forward characteristic of the device.

Hence, this paper introduces an AlGaIn/GaN based MISFET with the double P-buried layers (DP-MISFET). The source-connected bottom P-buried layer (BP) can deplete the 2DEG and improve the breakdown voltage without affecting the forward characteristic due to the large distance between the BP and channel layer. The floating top P-buried (TP) layer can further improve the breakdown voltage by absorbing the lateral electric field from the drain and blocking current flowing from the source to the drain as a current blocking layer (CBL) [26] while the forward characteristic of the device is almost unchanged because the 2DEG density is not affected by the P-buried layers; meanwhile, the TP is formed by Magnesium (Mg) ion implantation in this paper.

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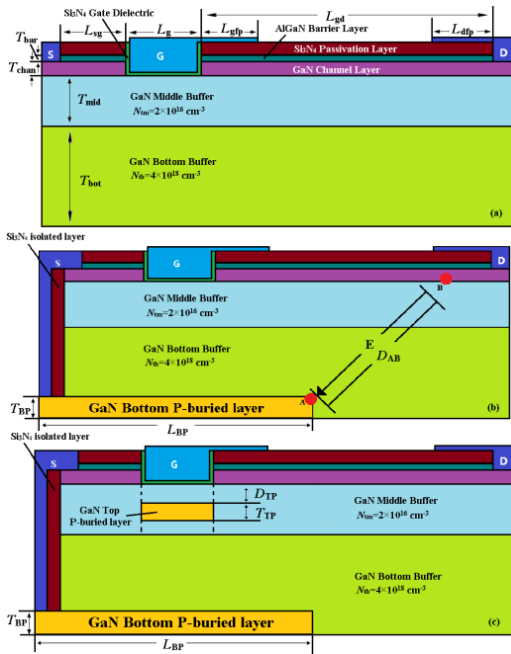


FIGURE 1. The cross-section of: (a) C-MISFET (b) BP-MISFET, and (c) DP-MISFET.

## II. STRUCTURES AND SIMULATION

The cross-section of a MISFET with the double P-buried layers (DP-MISFET) is illustrated in Fig. 1(c). To show the difference in structure between the MISFET we proposed and the conventional MISFET (C-MISFET) and the MISFET with only one bottom P-buried layer (BP-MISFET), the cross-sections of the C-MISFET and BP-MISFET are also proposed in Fig 1(a) and (b).

All these structures include an unintentionally doped  $Al_{0.15}Ga_{0.75}N$  barrier layer, an unintentionally doped GaN channel layer, a  $0.4\text{-}\mu\text{m}$ -thick GaN middle buffer layer and a  $1.6\text{-}\mu\text{m}$ -thick GaN bottom buffer layer that form the buffer layer of the MISFET, and the donor concentration is set to  $1 \times 10^{16} \text{ cm}^{-3}$  in the buffer layers as background carriers induced by fabrication process. Besides, in middle buffer layer and bottom buffer layer, we sets an acceptor type traps at concentrations of  $2e16 \text{ cm}^{-3}$  and  $4e18 \text{ cm}^{-3}$ , respectively, and its trap level is  $1.0 \text{ eV}$  from intrinsic fermi level. On the  $Si_3N_4/AlGaIn$  interface, we also sets a donor type traps at concentrations of  $5e13 \text{ cm}^{-2}$ , and its trap level is  $0.4 \text{ eV}$  from intrinsic fermi level. Moreover, the silicon nitride ( $Si_3N_4$ ) material is used as a gate dielectric and the passivation layers with the thicknesses of  $20 \text{ nm}$  and  $100 \text{ nm}$ , and which are also used as an isolated layer with the length of  $0.1 \mu\text{m}$ . Furthermore, the lengths of the gate field plate and drain field plate are  $0.5 \mu\text{m}$  and  $0.8 \mu\text{m}$  at first, respectively [25].

The values of the key parameters of the proposed structure are summarized in Table 1. As shown in Fig. 1(b),  $L_{BP}$  and  $T_{BP}$  are the length and thickness of the bottom P-buried layer (BP), respectively, and  $N_{aBP}$  is the hole concentration of the BP. In Fig. 1(c),  $D_{TP}$  is the spacing between the top P-buried layer (TP) and the channel layer, and  $N_{aTP}$  is the

TABLE 1. Simulation parameters used for device simulation.

PARAMETERS	ALIASES	VALUES
Gate-source spacing	$L_{sg}$	$0.5 \mu\text{m}$
Gate Length	$L_g$	$0.5 \mu\text{m}$
Gate-drain spacing	$L_{gd}$	$6 \mu\text{m}$
Gate field plate length	$L_{gfp}$	$0.5 \mu\text{m}$
Drain field plate length	$L_{dfp}$	$0.8 \mu\text{m}$
Thickness of TP	$T_{TP}$	$0.1 \mu\text{m}$
TP and channel layer spacing	$D_{TP}$	$0.2 \mu\text{m}$
Thickness of BP	$T_{BP}$	$0.4 \mu\text{m}$
Length of BP	$L_{BP}$	$4 \mu\text{m}$
TP hole concentration	$N_{aTP}$	$5 \times 10^{17} \text{ cm}^{-3}$
BP hole concentration	$N_{aBP}$	$2 \times 10^{17} \text{ cm}^{-3}$
Barrier layer thickness	$T_{bar}$	$25 \text{ nm}$
Channel layer thickness	$T_{chan}$	$50 \text{ nm}$
Middle buffer layer thickness	$T_{mid}$	$0.4 \mu\text{m}$
Bottom buffer layer thickness	$T_{bot}$	$1.6 \mu\text{m}$

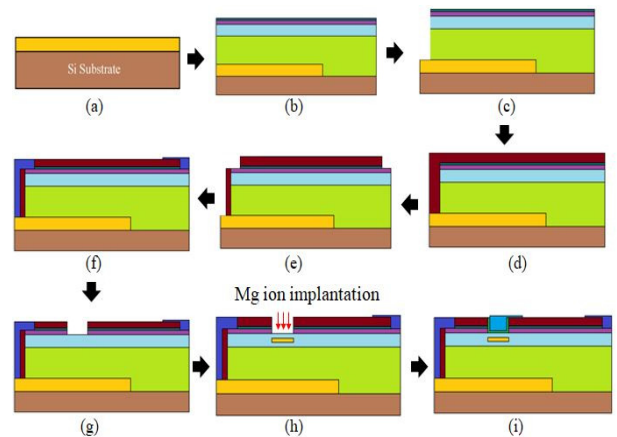
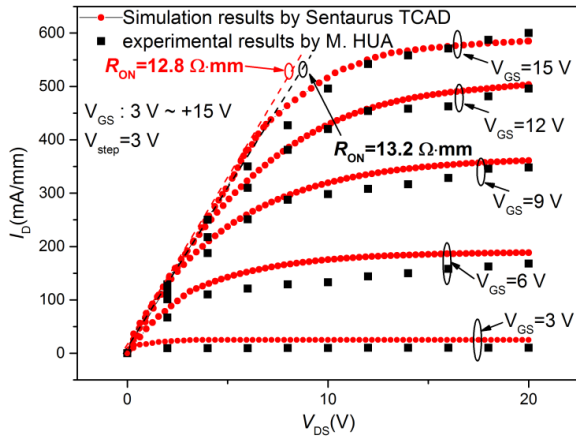


FIGURE 2. Schematic of fabrication process steps for proposed structure.

hole concentration of the TP. The whole concentration of both P-buried layers is set in the range from  $1 \times 10^{17} \text{ cm}^{-3}$  to  $5 \times 10^{17} \text{ cm}^{-3}$  [25], [27]. The thickness of the TP ( $T_{TP}$ ) is set to  $0.1 \mu\text{m}$  [28]. The work function of the gate metal is set to  $5.15\text{eV}$  [29].

The schematic of the fabrication process of the proposed structure is presented in Fig. 2.

- (a) Growing an epitaxial p-type layer on a Si substrate, this can be realized by the metal-organic chemical vapor deposition (MOCVD) using Mg as a P-type impurity [30]–[32].
- (b) Etching the right part of p-type layer through the inductively coupled plasma (ICP) process [30], [33] and then growing the bottom buffer layer, middle buffer layer, channel layer and barrier layer.
- (c) Etching the left part of the device.
- (d)  $Si_3N_4$  is used to fill the trench and form the passivation layer.
- (e) Etching the source and drain contact.
- (f) Forming the ohmic contact of the source and drain electrode.
- (g) Etching the gate contact.



**FIGURE 3.** The  $I_D$ - $V_{DS}$  characteristics from simulation and experiment validate the effectiveness of models in simulation.

- (h) Forming the p-type region by using Mg ion implantation, which can simplify the fabrication procedures by accomplishing the gate at the same time, and the depth or hole concentration are decided by the energy and dose of ion implantation [34]–[36].
- (i) Growing epitaxial  $\text{Si}_3\text{N}_4$  as a gate dielectric and forming the gate electrode.

The TCAD Sentaurus software from the Synopsys Inc was used to simulate and optimize three different MISFETs based on the Baliga’s figure of merit ( $BFOM$ ), defined as  $BFOM = V_{BK}^2/R_{on,sp}$  [37]. To get more accurate results, the physical models such as the SRH, Auger, DopingDep, high field saturation and polarization model including the Gate Dependent strain were used in the simulation. Besides, the substrate is removed for the suppression of the vertical leakage current [38]–[41]. In Fig 3, the effectiveness of these models has been proved by Luo *et al.* [29] with the experimental results [42], in which the gate-drain spacing took the value of 15  $\mu\text{m}$ . It can be seen that the simulation results as 12.8 $\Omega\bullet\text{mm}$  of  $R_{ON}$  is fit well with the experimental results as 13.2 $\Omega\bullet\text{mm}$  of  $R_{ON}$ .

When the breakdown performance was simulated, the Avalanche model with a dependent electric field was adopted in the simulation. The impact ionization rate was defined by [25]:

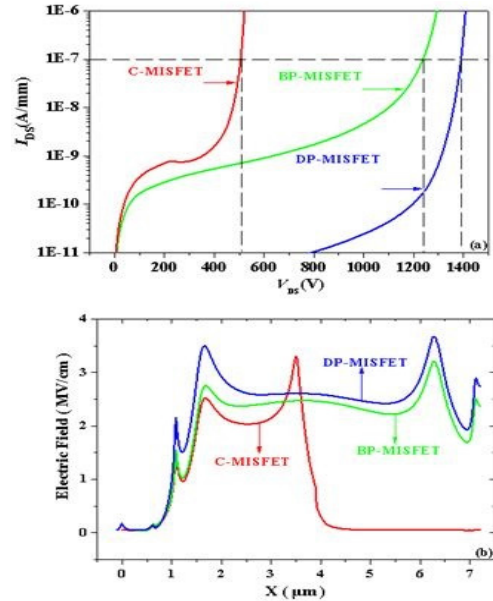
$$G = \alpha_n n v_n + \alpha_p p v_p \quad (1)$$

where  $n$  and  $p$  refer to the concentration of electrons and holes, respectively,  $v_n$  and  $v_p$  refer to the saturation velocity of the electrons and the holes, respectively, and  $\alpha_n$  and  $\alpha_p$  are the values of the impact-ionization coefficient which relates to the electric field, and they are defined by Equation (2). The temperature dependence of the phonon gas against which carriers are accelerated is expressed by parameters  $\gamma_n$  and  $\gamma_p$ . In (2), coefficients  $a_n$ ,  $a_p$ ,  $b_n$ , and  $b_p$  are fitting parameters, and their values are listed in Table 2 [25], [43].

$$\alpha_{n,p} = \gamma_{n,p} a_{n,p} \exp(-b_{n,p} \gamma_{n,p} / E) \quad (2)$$

**TABLE 2.** Fitting parameters used in equation (2).

PARAMETERS	VALUES
$a_n$	$2.9 \times 10^8 \text{ cm}^{-1}$
$a_p$	$3.4 \times 10^7 \text{ V/cm}$
$b_n$	$1.34 \times 10^8 \text{ cm}^{-1}$
$b_p$	$2.03 \times 10^7 \text{ V/cm}$



**FIGURE 4.** (a) Breakdown characteristics of C-MISFET, BP-MISFET and DP-MISFET. (b) the corresponding horizontal electric field distribution in channel 1nm below heterojunction.

### III. RESULTS AND DISCUSSION

#### A. BASIC CHARACTERISTICS

The comparison of the breakdown characteristics and the electric field distribution of the C-MISFET, BP-MISFET, and DP-MISFET is presented in Fig. 4. The  $BV$  values of the C-MISFET, BP-MISFET, and DP-MISFET extracted at  $I_D = 0.1 \mu\text{A/mm}$  and  $V_{GS} = 0 \text{ V}$  are 503.9 V, 1237 V, and 1389 V, respectively. In the C-MISFET, the 2DEG is not completely depleted, so the electric field peak appears between the gate and drain, which limited the breakdown voltage of the device. In contrast to the C-MISFET, the bottom P-buried layer could deplete the 2DEG completely and improve  $BV$  of the BP-MISFET, which could flat the electric field distribution and extend the electric field distribution to the drain. In the DP-MISFET, a floating top P-buried layer was added to further improve  $BV$  at the cost of slight forward characteristics degradation.

As presented in Figs. 5(a)-(b), the on-resistance ( $R_{ON}$ ) increased only from 8.72  $\Omega\bullet\text{mm}$  in the C-MISFET to 8.77 $\Omega\bullet\text{mm}$  in the optimized DP-MISFET, which was lower than 9.18  $\Omega\bullet\text{mm}$  presented in [25], and  $V_{TH}$  increased only from 2.21 V to 2.98 V. The shift of  $V_{TH}$  was due to the higher-band energy level under the gate induced by the floating top P-buried layer [29], which also increased  $R_{ON}$  because the

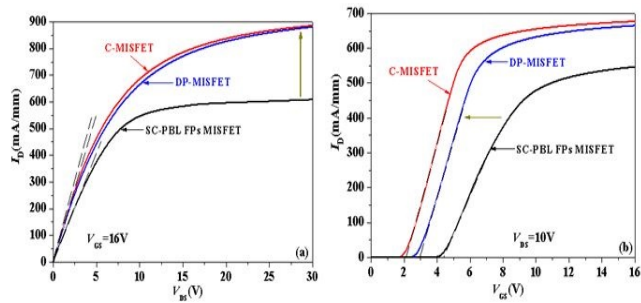


FIGURE 5. (a).  $I_D$ - $V_{DS}$  characteristics at  $V_{GS} = 16$  V and (b)  $I_D$ - $V_{GS}$  characteristics at  $V_{DS} = 10$  V.

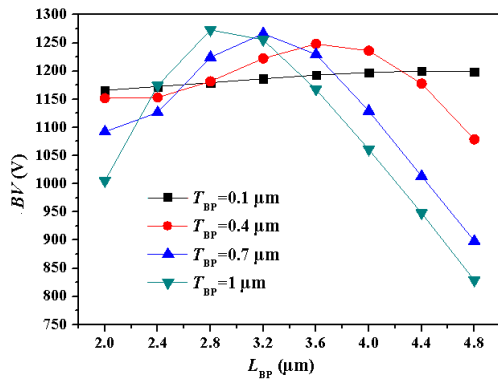


FIGURE 6. The relationship between  $BV$ ,  $L_{BP}$  and  $T_{BP}$  while  $N_{aBP} = 3 \times 10^{17} \text{ cm}^{-3}$ .

eDensity under the gate was decreased from  $2.79 \times 10^{13} \text{ cm}^{-2}$  to  $2.71 \times 10^{13} \text{ cm}^{-2}$  at  $V_{GS} = 16$  V. Besides, the eDensity of the 2DEG was almost unaffected because the gate and the top P-buried layer were aligned, thus, the maximum saturation current of the device is increased from 609mA/mm presented in [25] to 881mA/mm in the optimized DP-MISFET, increased by 45%, which can ensure that the device has a strong current drive capability.

### B. EFFECT OF BOTTOM P-BURIED LAYER (BP)

As shown in Fig. 1(b), the P-buried layer was added to the bottom buffer. The influence on the breakdown characteristic of three key parameters, i.e.,  $N_{aBP}$ ,  $L_{BP}$ , and  $T_{BP}$ , were analyzed through the simulations. Initially,  $N_{aBP}$  was set to  $3 \times 10^{17} \text{ cm}^{-3}$ .

The relationship between  $BV$ ,  $L_{BP}$ , and  $T_{BP}$  is presented in Fig. 6, and these relationships also can be summarized as the relationship between  $BV$  and the distance of point A and point B ( $D_{AB}$ ) in Fig. 1(b). At  $T_{BP} = 0.4 \mu\text{m}$ , when  $L_{BP}$  increased,  $BV$  also increased until the  $BV$  peak occurred at  $L_{BP} = 3.6 \mu\text{m}$ . Due to the absorbing of the electric field by the BP, the electric field line from the drain to the point A was directed, which enhanced the electric field in the body of MISFET, decreased the concentration of the electric field under the gate and modulated the electric field distribution between the gate and drain.

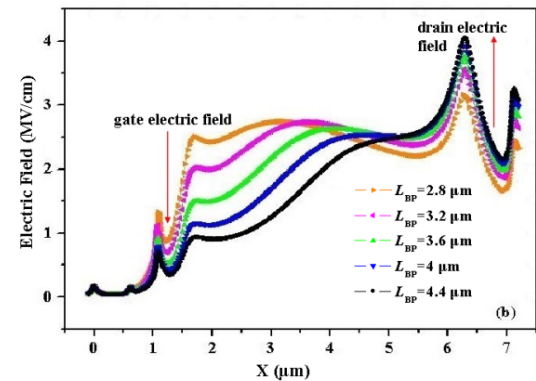
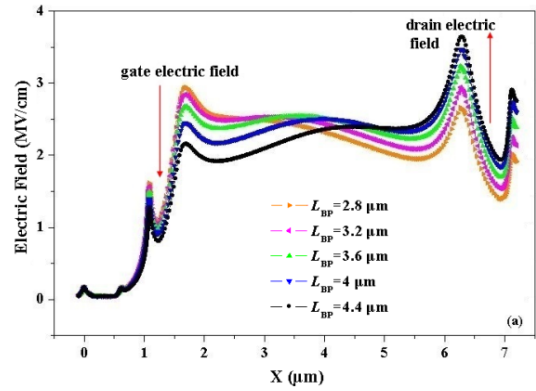


FIGURE 7. The relationship between Electric Field and  $L_{BP}$  while  $N_{aBP} = 3 \times 10^{17} \text{ cm}^{-3}$  with (a)  $T_{BP} = 0.4 \mu\text{m}$  (b)  $T_{BP} = 1 \mu\text{m}$ .

The results presented in Fig. 7(a) also prove that with the increase in  $L_{BP}$ , i.e. decrease in  $D_{AB}$ , the value of the drain electric field peak was getting higher and higher; at the same time, the value of the gate electric field peak was getting lower and lower, and the high drain electric field peak would cause avalanche breakdown to occur in advance, so the  $BV$  decrease when  $L_{BP}$  was larger than  $3.6 \mu\text{m}$  (Fig.7). On the other hand, Fig. 6 also shows that with the increase in the thickness of BP ( $T_{BP}$ ), the  $BV$  peak shifted to the left and the value of maximum  $BV$  increased only a little; however, the  $BV$  curves declined rapidly after the peak point. This phenomenon is related to the change of  $D_{AB}$ . When  $T_{BP}$  was small, about  $0.1 \mu\text{m}$ , with the increase in  $L_{BP}$ , the change of  $D_{AB}$  was not obvious. On the other hand, when  $T_{BP}$  was larger than  $0.4 \mu\text{m}$ , the changes of  $D_{AB}$  were particularly significant as  $L_{BP}$  increased. Both situations are presented in Fig.6, where one curve is almost flat, and the other curves have a distinct rise and fall.

The results presented in Fig. 7(b) also show that the peak of the gate electric field dropped more rapidly at  $T_{BP}$  of  $1 \mu\text{m}$  than at  $T_{BP}$  of  $0.4 \mu\text{m}$ , which is displayed in Fig. 7(a), causing a rapid drop in the breakdown voltage. Also, if the BP layer is too thick, it would be more difficult to control the length of the BP in semiconductor fabrication procedure. In this work, the  $T_{BP}$  was set to  $0.4 \mu\text{m}$ . Besides, the reason for the changes of the drain electric field and gate electric field was not only related to  $D_{AB}$  but also to  $N_{aBP}$ . With the aim to

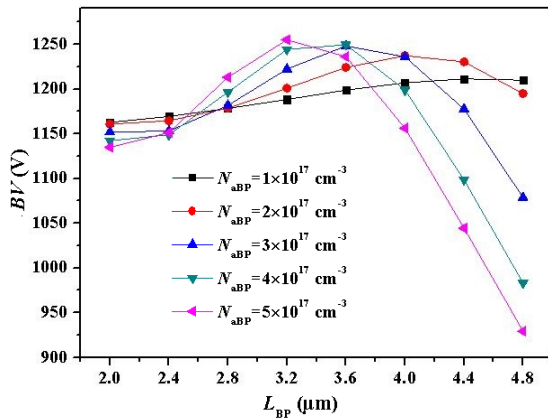


FIGURE 8. The relationship between  $BV$ ,  $L_{BP}$  and  $N_{aBP}$  while  $T_{BP} = 0.4 \mu\text{m}$ .

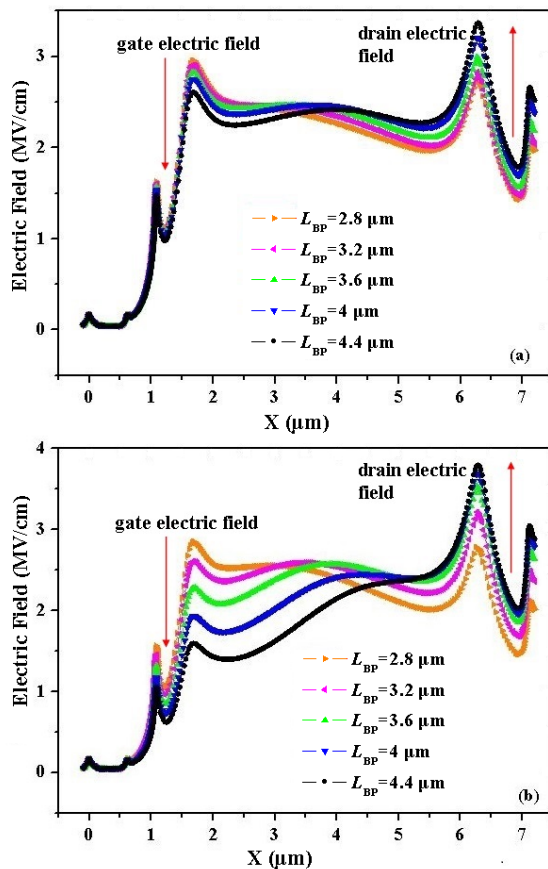


FIGURE 9. The relationship between electric field and  $L_{BP}$  while  $T_{BP} = 0.4 \mu\text{m}$  with (a)  $N_{aBP} = 2 \times 10^{17} \text{cm}^{-3}$  (b)  $N_{aBP} = 5 \times 10^{17} \text{cm}^{-3}$ .

study the influence of  $N_{aBP}$  and  $L_{BP}$  on  $BV$ , more simulations were performed to provide the results necessary for further discussion; while the relationship between  $BV$  and  $L_{BP}$  was investigated in the previous work at  $N_{aBP} = 3 \times 10^{17} \text{cm}^{-3}$ .

In Fig. 8, it is shown that the maximum  $BV$  was almost unchanged, but the curves declined more rapidly when  $N_{aBP}$  was large than  $2 \times 10^{17} \text{cm}^{-3}$ . As  $N_{aBP}$  increased, the ability

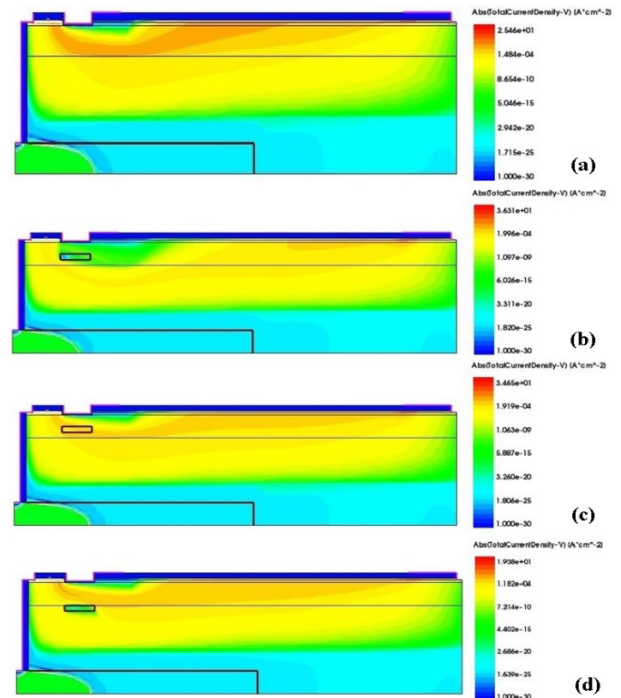


FIGURE 10. The path of the leakage current of: (a) BP-MISFET (b) DP-MISFET with  $N_{aTP} = 5 \times 10^{17} \text{cm}^{-3}$  and  $D_{TP} = 0.2 \mu\text{m}$  (c) DP-MISFET with  $N_{aTP} = 1 \times 10^{17} \text{cm}^{-3}$  and  $D_{TP} = 0.2 \mu\text{m}$  (d) DP-MISFET with  $N_{aTP} = 5 \times 10^{17} \text{cm}^{-3}$  and  $D_{TP} = 0.4 \mu\text{m}$ .

of BP to absorb the electric field was also getting stronger, which decreased the concentration of the electric field under the gate and caused a rapid drop in the breakdown voltage. The results presented in Fig. 9(b) prove that the peak of the gate electric field dropped more rapidly at  $N_{aBP}$  of  $5 \times 10^{17} \text{cm}^{-3}$  than at  $N_{aBP}$  of  $2 \times 10^{17} \text{cm}^{-3}$  in Fig. 9(a). Considering that  $BV$  dropped rapidly after the peak point at a higher  $N_{aBP}$ , which made it difficult to control  $L_{BP}$  in semiconductor fabrication procedure,  $N_{aBP}$  and  $L_{BP}$  were set to  $2 \times 10^{17} \text{cm}^{-3}$  and  $4 \mu\text{m}$ , respectively.

### C. EFFECT OF FLOATING TOP P-BURIED LAYER (TP)

The BP is discussed in the previous section, where it is stated that breakdown voltage can fully deplete 2DEG and enhance the electric field in the body of the MISFET; however, the electric field lines points not only to the BP but also to the source, which causes the current leakage as shown in Fig 10(a), and limiting the breakdown voltage.

Therefore, a floating top P-buried layer was added to further improve the breakdown voltage without increasing  $R_{on,sp}$  or complicating the fabrication process presented in Fig. 1(c).

It can be seen that the TP not only could absorb more lateral electric field but also could block the current flowing through the middle buffer layer, acting as a current blocking layer (CBL) as shown in Fig. 10(b) unlike the BP-MISFET shown in Fig. 10(a). So the leakage current could only pass through the bottom buffer layer which could suppress the

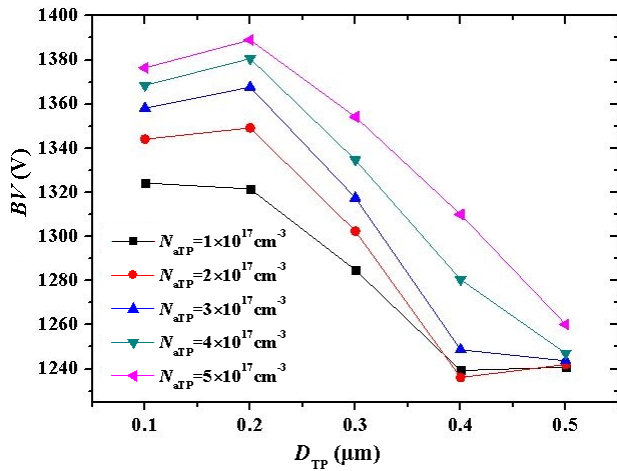


FIGURE 11. The relationship between  $BV$ ,  $R_{on,sp}$  and  $D_{TP}$ .

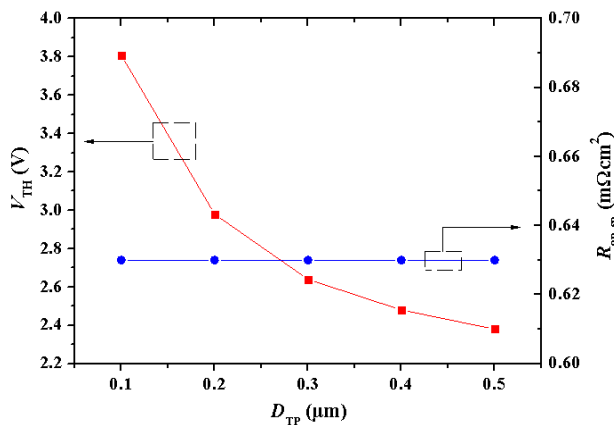


FIGURE 12. The relationship between  $V_{TH}$ ,  $R_{on,sp}$  and  $D_{TP}$  while  $N_{aTP} = 5 \times 10^{17} \text{ cm}^{-3}$ .

leakage current by a higher acceptor trap. Consequently, as shown in Fig. 4, the electric field distribution and breakdown voltage were improved.

The results presented in Fig. 11 show that  $BV$  increased with the increase in  $N_{aTP}$ . Also, as it can be seen in Fig 10(c), the TP at lower  $N_{aTP}$  could not act as a current blocking layer, so the leakage current still could pass through the middle buffer layer; meanwhile, when the TP was far away from the channel layer, i.e., it was getting closer to the BP, the ability to block the leakage current in the middle buffer layer decreased as displayed in Fig 10(d); then, the device breakdown occurs in advance. Furthermore, the results in Fig. 11 also indicate that the highest value of  $BV$  was 1389 V while  $D_{TP}$  was 0.2  $\mu\text{m}$  and  $N_{aTP}$  was  $5 \times 10^{17} \text{ cm}^{-3}$ , which was higher than 1312 V in [25].

As shown in Fig. 12, the change of  $D_{TP}$  almost did not affect  $R_{on,sp}$ , which could guarantee good conduction characteristics, but in the other hand,  $V_{TH}$  increased when the TP got close to the gate.

Finally, we discuss and corrects the length of the drain plate, which can be seen in Fig 13(a). It shows that when  $L_{dfp}$  is equal to 0.6  $\mu\text{m}$ , the breakdown voltage and

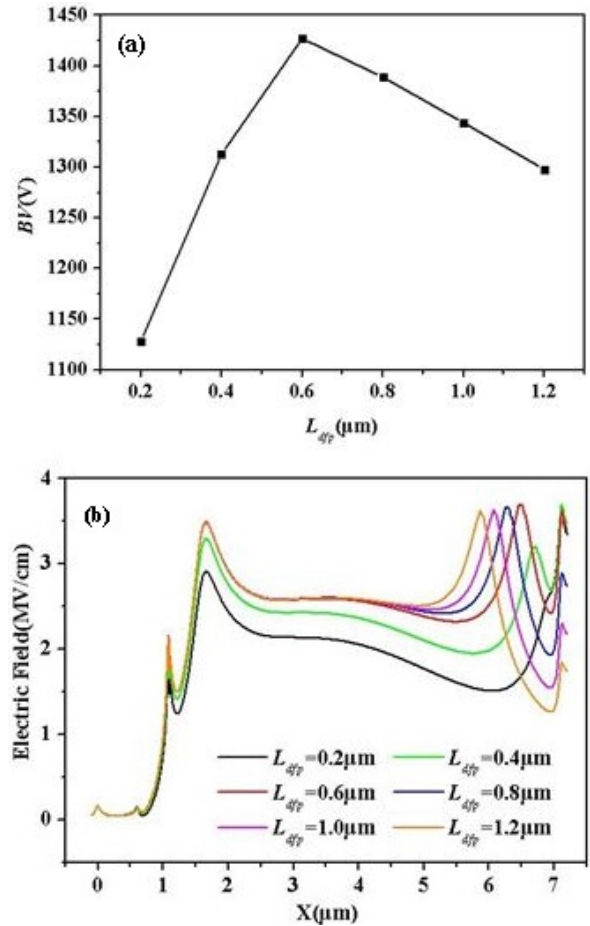


FIGURE 13. (a) The relationship between  $L_{dfp}$  and  $BV$  (b) The relationship between  $L_{dfp}$  and the surface electric field distribution.

$BFOM$  of the device can reach the maximum of 1427V and 3.23  $\text{GW}\cdot\text{cm}^{-2}$ . And Fig 13(b) shows the relationship between the length of the drain field plate and the surface electric field distribution.

#### IV. CONCLUSION

In this paper, we presented a high  $BFOM$  normally-off AlGaIn/GaN MISFET with the double P-buried layers. To show the improvement in the MISFET characteristics, we compared three different MISFETs, i.e., the C-MISFET, the BP-MISFET and the DP-MISFET, and simulated the properties of these devices using the common physical models. Moreover, we analyzed the influence of the BP and the TP by discussing and optimizing their values. The optimized MISFET exhibited a strong current drive capability, a high-power  $BFOM$  of 3.23  $\text{GW}\cdot\text{cm}^{-2}$ ,  $BV$  of 1427 V, and  $R_{on,sp}$  of 0.63  $\text{m}\Omega\cdot\text{cm}^2$ , thus, the proposed structure showed good performance.

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**YING WANG** (SM'17) received the B.S. degree in microelectronics and the M.S. degree in microelectronics and solid state electronics from Liaoning University, China, in 1999 and 2002, respectively, and the Ph.D. degree in electronic science and technology from Xi'an Jiaotong University, China, in 2005.

From 2005 to 2016, he was with the Harbin Engineering University, Chinas. He became a Professor, in 2009. He is currently with the Key Laboratory of RF Circuits and Systems Ministry of Education, Hangzhou Dianzi University, Hangzhou, China. He has rich experience in the research of microelectronic devices and integration technology, power semiconductor devices, and micro-sensor design. He has over 70 publications and is the holder of 22 patents. His current research and development interests include the advanced SiC/GaN power semiconductor devices design and simulation, the space radiation effects, and enhanced method analysis.



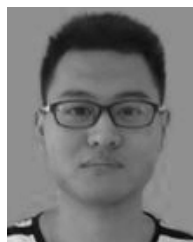
**MENG-TIAN BAO** received the B.S. degree in microelectronics, the M.S. degree in electronic and communication engineering, and the Ph.D. degree in information and communication engineering from Harbin Engineering University, China, in 2008, 2012, and 2019, respectively.

For many years, she has been involved in the research of semiconductor device structure design and metallization technology. She is currently a Lecturer with the Hangzhou Dianzi University. Her current research interests include SiC power devices design and the irradiation effect analysis.



**FEI CAO** received the B.S. degree in electronic science and technology and the M.S. degree in microelectronics and solid state electronics from Liaoning University, China, in 2004 and 2009, respectively, and the Ph.D. degree in material science from the Harbin Institute of Technology, China, in 2016.

For many years, she has been involved in the research of semiconductor device structure design and metallization technology. She is currently a Lecturer with the Hangzhou Dianzi University. She has experience in semiconductor device fabrication and related performance characterization and analysis, and has accumulated a certain theoretical and experimental basis in semiconductor device metallization and interconnection technology.



**JIAN-XIANG TANG** received the B.S. degree in electronic information engineering from Tongji Zhejiang College, China, in 2016, and the M.S. degree from Hangzhou Dianzi University, China, in 2019. His research interests include new structure and key technologies of power transistor with the third generation wide-gap semiconductor materials, and optimizing device structure and performance by theoretical analysis and simulation.



**XIN LUO** received the B.S. degree in microelectronics and the Ph.D. degree in information and communication engineering from Harbin Engineering University, China, in 2008 and 2019, respectively.

He is currently with the National Institute of LED on Silicon Substrate, Nanchang University, Nanchang, China, where he is researching on the advanced GaN photoelectric devices.

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