

## RESEARCH ARTICLE

# On the Robustness of a Modified Super-Twisting Algorithm With Prescribed-Time Convergence

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**ABSTRACT** This paper addresses the robustness of a novel two-stage super-twisting algorithm designed to converge within a prescribed time interval despite disturbances and model uncertainties. Initially, we introduce a method for tuning parameters that guarantees the algorithm's analytic solution will reach the origin precisely at a prescribed instant, assuming an unperturbed scenario. We then enhance this method to maintain prescribed-time convergence, even when faced with unknown bounded disturbances. The algorithm's performance is demonstrated through a numerical simulation of a state estimation problem for a perturbed damped pendulum. The results show that the estimation errors converge robustly to the origin at the prescribed time and remain there afterward.

**INDEX TERMS** Prescribed-time convergence, robust estimation, super-twisting algorithm.

## I. INTRODUCTION

The super-twisting algorithm (STA) [1], [2] has been widely applied to the design of finite-time robust controllers and estimators over the last three decades [3], [4], [5], [6], [7]. Although effective, it is essential to note that we cannot determine a global finite upper bound for the settling time (UBST) when employing the conventional STA. This is because the actual settling time tends towards infinity when the system's initial condition increases without bounds [8]. Recent extensions to this algorithm offer fixed-time stability [9], enabling us to estimate a finite UBST that does not depend on initial conditions [10], [11]. However, this estimate tends to be overly conservative compared to the actual settling time seen in experiments and relates to the system's parameters in a complex way. Moreover, a bounded settling time is insufficient for applications requiring precise timing, such as tactical missile guidance. Hence, this paper explores STA modifications that permit arbitrarily choosing the settling instant.

The pioneering work of Song et al. [12] has demonstrated that it is possible to drive the states of a nonlinear system

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in the normal form to a desired trajectory at a prescribed instant  $t_c \in \mathbb{R}_{>t_0}$  by employing time-varying gains that continuously approach infinity as time approaches  $t_c$ . This idea was initially proposed to design regulators and later expanded to state estimation by Holloway and Krstic [13]. However, to avoid encountering a singularity at  $t_c$ , the investigated prescribed-time initial value problem is only defined in the finite domain  $[t_0, t_c)$  in the aforementioned papers. Furthermore, these approaches are highly sensitive to measurement noise and numerical errors, primarily due to the unbounded growth of their time-varying gains as  $t$  approaches  $t_c$ . To address this latter limitation, recent papers [14], [15], [16] have investigated using the user-defined instant as a prescribed UBST instead of the convergence instant itself. In doing so, these recent studies ensure that the time-varying gains introduced in [12] and [13] remain finite but render the exact convergence instant unknown, although bounded.

The present paper is a continuation of [17] and proposes a modification of the STA that presents state convergence precisely at a prescribed instant  $t_c$ , which is set *a priori* as a system parameter. During the time interval  $[t_0, t_c)$ , the proposed algorithm uses both time-varying [12], [13] and switching [1], [2] gains to provide robustness and the

prescribed-time convergence property. At  $t_c$ , the algorithm assumes the dynamics of the conventional STA to ensure stability in the infinite time horizon. In contrast to works [1], [2], [10], [11], in which only a conservative bound of the settling time can be estimated, the proposed solution allows the arbitrary prescription of the settling instant. Unlike Song et al. [12] and Holloway and Krstic [13], our approach ensures robust stability in the infinite time domain  $[t_0, \infty)$  while also using a time-varying gain only in its first component state equation, which mitigates the sensitivity to measurement noise. Furthermore, our approach differs from [14], [15], and [16] by employing the prescribed instant as the exact settling instant, not as its upper bound. Convergence and robustness proofs for the modified super-twisting algorithm introduced in [17] are also provided. Additionally, for illustration, the proposed method is employed in designing a state estimator for a disturbed damped pendulum. In summary, the main contribution of this paper is the proposal of a novel two-stage STA-like algorithm capable of presenting robust convergence of its states to the origin at a user-defined instant in the presence of bounded disturbances or model uncertainties, along with analytical proofs of the aforementioned properties.

In the remaining text, Section II presents the mathematical preliminaries required to introduce the proposed results and states the paper's primary objective. Section III presents the proposed proofs that indicate the existence of system parameters that guarantee the prescribed-time robust convergence. Section IV presents simulation results and comparisons with a similarly prescribed-time convergent method. Finally, Section V concludes this paper.

### A. DEFINITIONS

Consider the system

$$\dot{x} = f(t, x), \quad x(t_0) \triangleq x_0 \in \mathbb{R}^n, \quad t \in \mathbb{R}_{\geq t_0}, \quad (1)$$

where  $x \in \mathbb{R}^n$  is the system state vector,  $t$  is the time variable,  $t_0 \in \mathbb{R}_{\geq 0}$  is the initial instant, and  $f : \mathbb{R}_{\geq t_0} \times \mathbb{R}^n \rightarrow \mathbb{R}^n$  is a nonlinear function such that  $f(\cdot, \cdot)$  is jointly continuous in  $t$  and  $x$ , and  $f(t, 0) = 0, \forall t \in [t_0, \infty)$ . A solution  $x(t; t_0, x_0)$  of (1) is viewed in the generalized Filippov sense [18], and is understood as a first-order differentiable function satisfying (1) and the initial condition, *i.e.*,  $x(t_0; t_0, x_0) = x_0$ .

We present the definition of the stability and convergence concepts required in this paper.

**Definition 1** [19]: The equilibrium point  $x = 0$  of (1) is said to be *finite-time stable* if it is asymptotically stable, and any solution  $x(t; t_0, x_0)$  converges the origin in a finite time interval  $t \in [t_0, t_0 + T(t_0, x_0)]$ , where

$$T(t_0, x_0) = \inf \{T \geq t_0 : x(t; t_0, x_0) = 0, \forall t \geq t_0 + T\} \quad (2)$$

is the settling-time function.

**Definition 2:** A solution of (1) is said to present *prescribed-time convergence* to its equilibrium point if the system is finite-time stable and its states reach the equilibrium

point in a finite time interval upper bounded by  $t_0 + t_c$ , where  $t_c$  can be arbitrarily specified.

### II. PROBLEM STATEMENT

The super-twisting algorithm (STA) is given by [1]

$$\dot{\varepsilon}_1 = -\kappa_1 [\varepsilon_1]^{1/2} + \varepsilon_2, \quad (3)$$

$$\dot{\varepsilon}_2 = -\kappa_2 \text{sign}(\varepsilon_1) + \delta, \quad (4)$$

where  $\varepsilon \triangleq (\varepsilon_1, \varepsilon_2) \in \mathbb{R}^2$  is its state vector,  $\kappa_1, \kappa_2 \in \mathbb{R}_{>0}$  are scalar parameters,  $[\varepsilon_1]^{1/2} \triangleq |\varepsilon_1|^{1/2} \text{sign}(\varepsilon_1)$ , and  $\delta \in \mathbb{R}$  is the disturbance term. Consider that  $\delta$  is bounded by a known constant  $L$ , *i.e.*,  $|\delta| \leq L$ . Despite of  $\delta$ , the origin  $\varepsilon = 0$  is finite-time stable if the gain condition [20]

$$L < \min \left\{ \frac{\kappa_1}{2}, \frac{\kappa_1 \kappa_2}{1 + \kappa_1} \right\} \quad (5)$$

is satisfied.

As the STA (3)–(4) is a finite-time stable system, only a conservative bound of its settling time can be estimated, and the respective estimate is dependent on the system's initial conditions, as expressed in Definition 1. The goal of the present paper is to introduce and analyze a new second-order system analogous to (3)–(4), but endowed with the ability to converge to the origin within a prescribed time interval, despite the presence of the unknown disturbance  $\delta$ .

### III. MAIN RESULTS

To achieve the aforementioned goal, we propose a novel algorithm obtained from a modification of the STA (3)–(4), given by

$$\dot{\varepsilon}_1 = -\sigma(t, \varepsilon_1) + \varepsilon_2, \quad (6)$$

$$\dot{\varepsilon}_2 = -\kappa_2 \text{sign}(\varepsilon_1) + \delta, \quad (7)$$

where

$$\sigma(t, \varepsilon_1) \triangleq \begin{cases} \frac{\eta}{t_c - t} \varepsilon_1, & t \in [t_0, t_c), \\ \kappa_1 [\varepsilon_1]^{1/2}, & t \in [t_c, \infty), \end{cases} \quad (8)$$

with  $t_c$  representing the prescribed convergence instant, and  $\eta \in \mathbb{Z}_{\geq 1}$  being a scalar parameter. The algorithm above presents a hybrid structure containing two stages. The first stage comprises the time interval  $t \in [t_0, t_c)$ , in which the system (6)–(7) combines both a time-varying and a switching gains. In the second stage  $t \in [t_c, \infty)$ , the proposed algorithm coincides with the conventional STA (3)–(4). Considering the unperturbed case, *i.e.*,  $\delta \equiv 0$ , and the first stage, the following proposition provides an analytical solution to the initial value problem (IVP) consisting of (6)–(7) and the given initial conditions.

**Proposition 1:** Consider the IVP consisting of (6)–(7) with  $\delta \equiv 0$  and an initial condition  $\varepsilon(t_0) = (\varepsilon_1(t_0), \varepsilon_2(t_0)) \in \mathbb{R}^2$ , denote its solution in  $[t_0, \infty)$  by  $\varepsilon(t) := (\varepsilon_1(t), \varepsilon_2(t)) \in \mathbb{R}^2$ , and recursively define the zero-crossing instants of  $\varepsilon_1(t)$  as

$$t_j \triangleq \inf \mathcal{T}_j, \quad j = 1, 2, \dots, n_r, \quad (9)$$

where  $n_r$  is the number of times  $\varepsilon_1(t)$  has reset to zero and

$$\mathcal{T}_j \triangleq \left\{ \zeta \in \mathbb{R}_{\geq t_0} : \zeta > t_{j-1} \text{ and } \lim_{t \rightarrow \zeta^-} \varepsilon_1(t) = 0 \right\}. \quad (10)$$

On each time interval  $t \in [t_{j-1}, t_j)$ , the solution to the IVP is recursively given by

$$\varepsilon_1(t) = \frac{t_c - t}{(\eta - 2)(\eta - 1)} \alpha(t) + \beta(t_{j-1}) \left( \frac{t_c - t}{t_c - t_{j-1}} \right)^\eta, \quad (11)$$

$$\varepsilon_2(t) = \varepsilon_2(t_{j-1}) - \kappa_2 s_{1,j-1} (t - t_{j-1}), \quad (12)$$

where  $s_{i,j-1} \triangleq \text{sign}(\varepsilon_i(t_{j-1}))$ , and

$$\alpha(t) \triangleq s_{1,j-1} (\kappa_2(t_c - t - (\eta - 2)(t - t_{j-1})) + (\eta - 2)\varepsilon_2(t_{j-1})), \quad (13)$$

$$\beta(\tau) \triangleq \varepsilon_1(\tau) - \frac{t_c - \tau}{\eta - 1} \varepsilon_2(\tau) - \frac{(t_c - \tau)^2}{(\eta - 2)(\eta - 1)} \kappa_2 s_{1,j-1}. \quad (14)$$

*Proof:* By the definition (9),  $t_j, j = 1, \dots, n_r$ , are the instants that  $\varepsilon_1(t)$  resets to zero and, consequently,  $\text{sign}(\varepsilon_1(t))$  switches its sign. Therefore,  $\text{sign}(\varepsilon_1(t)) = s_{1,j-1} \forall t \in [t_{j-1}, t_j)$ . Hence, the analytic solution of (7) in the interval  $t \in [t_{j-1}, t_j)$  is given by

$$\varepsilon_2(t) = \varepsilon_2(t_{j-1}) - \kappa_2 s_{1,j-1} (t - t_{j-1}). \quad (15)$$

Still considering the time interval  $[t_{j-1}, t_j)$ , by substituting (15) and (8) into (6), we obtain

$$\dot{\varepsilon}_1 = -\frac{\eta}{t_c - t} \varepsilon_1(t) + \varepsilon_2(t_{j-1}) - \kappa_2 s_{1,j-1} (t - t_{j-1}), \quad (16)$$

which can be immediately integrated, yielding

$$\varepsilon_1(t) = \frac{t_c - t}{(\eta - 2)(\eta - 1)} \alpha(t) + \beta(t_{j-1}) \left( \frac{t_c - t}{t_c - t_{j-1}} \right)^\eta, \quad (17)$$

where  $\alpha(t)$  and  $\beta(\cdot)$  are as defined in (13)–(14).  $\square$

*Corollary 1:* Consider the IVP described in Proposition 1 and assume that  $\eta \geq 3$ . It holds that  $\varepsilon_1(t) \rightarrow 0$  as  $t \rightarrow t_c$ .

*Proof:* From (12), we see that  $\varepsilon_2(t)$  will remain bounded in every finite time interval  $[t_{j-1}, t_j)$  if its initial condition  $\varepsilon_2(t_0)$  and the switching gain  $\kappa_2$  are finite. Therefore, from (11), we see that for any  $\eta \geq 3$ , it holds that  $\varepsilon_1(t)$  approaches zero as  $t$  approaches  $t_c$ .  $\square$

*Corollary 2:* Assuming that  $\eta \geq 3$ , the unperturbed system (6)–(7) is finite-time stable.

*Proof:* From Corollary 1, it holds that  $\mathbf{\varepsilon}(t_c) = [0, \varepsilon_2(t_c)]$ . Consequently, it is also true that the system (6)–(7) assumes the conventional STA behavior after  $t_c$  with finite initial conditions. Therefore, by satisfying (5), the system states will converge to the origin in finite time and remain there afterward.  $\square$

The following theorem demonstrates that sufficient conditions exist for the parameters  $\kappa_2$  and  $\eta$ , which ensure that  $\varepsilon_2(t)$  also approaches zero as  $t$  approaches  $t_c$ .

*Theorem 1:* Consider the IVP consisting of (6)–(7) with  $\delta \equiv 0$ , a known initial condition  $\mathbf{\varepsilon}(t_0) = (\varepsilon_1(t_0), \varepsilon_2(t_0)) \in \mathbb{R}^2$ , and  $\eta \geq 3$ . If the following conditions are satisfied

$$\kappa_2 (t_c - t_0) \geq |\varepsilon_2(t_0)|, \quad (18)$$

$$\begin{cases} -\kappa_2 (t_c - 2t_1 + t_0) \leq |\varepsilon_2(t_0)| \leq \kappa_2 (t_c - t_0), s_{1,0} = s_{2,0}, \\ -\kappa_2 (t_c - 2t_1 + t_0) \leq -|\varepsilon_2(t_0)| \leq \kappa_2 (t_c - t_0), s_{1,0} \neq s_{2,0}. \end{cases} \quad (19)$$

then  $\varepsilon_2(t)$  converges to zero at the prescribed time  $t_c$ .

*Proof:* Consider a geometric set  $\mathcal{E}(\kappa_2)$  defined as

$$\mathcal{E}(\kappa_2) \triangleq \{(t, \varepsilon_2(t)) : -\kappa_2 (t_c - t) \leq \varepsilon_2(t) \leq \kappa_2 (t_c - t)\}, \quad (20)$$

for a given  $\kappa_2 < \infty$ . This definition directly implies that if the pair  $(t_{j-1}, \varepsilon_2(t_{j-1}))$  is in  $\mathcal{E}(\kappa_2)$  for all  $j = 1, \dots, n_r$ , then  $\lim_{t \rightarrow t_c^-} \varepsilon_2(t) = 0$ . Consequently, ensuring the fulfillment of this bounding condition guarantees the convergence of  $\varepsilon_2$  to zero at the prescribed time  $t_c$ .

From (20) and the known initial condition  $\varepsilon_2(t_0)$ , we see that choosing  $\kappa_2$  satisfying

$$\kappa_2(t_c - t_0) \geq |\varepsilon_2(t_0)|, \quad (21)$$

ensures that  $(t_0, \varepsilon_2(t_0)) \in \mathcal{E}(\kappa_2)$ .

The next step is to ensure that  $(t, \varepsilon_2(t))$  belongs to  $\mathcal{E}(\kappa_2)$  at the instant  $t_1$  that  $\varepsilon_1(t)$  crosses the time axis for the first time. From (12), this value is given by

$$\varepsilon_2(t_1) = \varepsilon_2(t_0) - \kappa_2 s_{1,0} (t_1 - t_0). \quad (22)$$

Considering  $t = t_1$  and (20), it must hold that

$$-\kappa_2(t_c - t_1) \leq \varepsilon_2(t_1) \leq \kappa_2(t_c - t_1), \quad (23)$$

which can be expanded using (22) to

$$\begin{aligned} & -\kappa_2 (t_c - t_1 - s_{1,0} (t_1 - t_0)) \\ & \leq \varepsilon_2(t_0) \leq \kappa_2 (t_c - t_1 + s_{1,0} (t_1 - t_0)). \end{aligned} \quad (24)$$

Considering all the possible values that  $s_{1,0}$  and  $s_{2,0}$  can assume, we can develop (24) further to obtain

$$\begin{cases} -\kappa_2 (t_c - 2t_1 + t_0) \leq |\varepsilon_2(t_0)| \leq \kappa_2 (t_c - t_0), s_{1,0} = s_{2,0}, \\ -\kappa_2 (t_c - 2t_1 + t_0) \leq -|\varepsilon_2(t_0)| \leq \kappa_2 (t_c - t_0), s_{1,0} \neq s_{2,0}. \end{cases} \quad (25)$$

To compute the boundaries in (25), instant  $t_1$  can be calculated by solving (11) for  $t$ , considering  $\varepsilon_1(t) = 0$  and adopting parameters  $\eta$  satisfying  $\eta \geq 3$ , and  $\kappa_2$  satisfying (5) and (21). Note that by increasing  $\eta$ ,  $\varepsilon_1(t)$  approaches zero faster in (11), reducing the value of  $t_1$ . Additionally, increasing  $\kappa_2$  steepens the slope of  $\varepsilon_2(t)$  in (12), which also reduces  $t_1$ . Therefore, (25) can be satisfied by tuning either  $\kappa_2$  or  $\eta$ .

Given the linear time response of  $\varepsilon_2(t)$  and satisfying the conditions in equations (21) and (25), we can conclude that

for all  $t$  within the interval  $[t_0, t_1)$ , the pair  $(t, \varepsilon_2(t))$  lies within  $\mathcal{E}(\kappa_2)$ .

Following a similar mathematical procedure for the pair  $(t, \varepsilon_2(t))$  at  $t = t_2$  yields the inequality

$$\begin{cases} -\kappa_2(t_c - 2t_2 + t_1) \leq |\varepsilon_2(t_1)| \leq \\ \qquad \qquad \qquad \kappa_2(t_c - t_1), s_{1,1} = s_{2,1}, \\ -\kappa_2(t_c - 2t_2 + t_1) \leq -|\varepsilon_2(t_1)| \leq \\ \qquad \qquad \qquad \kappa_2(t_c - t_1), s_{1,1} \neq s_{2,1}, \end{cases} \quad (26)$$

where  $s_{1,1} = -s_{1,0}$ . The time instant  $t_2$  is similarly determined using (11), with the state vector at  $t_1$  serving as the initial condition. It can be inferred from the fulfillment of the inequalities (25) and (26) that  $(t, \varepsilon_2(t)) \in \mathcal{E}(\kappa_2)$  for all  $t \in [t_1, t_2)$ . Furthermore, it is worth noting that the value of  $t_2$  obtained by solving (11) with the same parameters  $\eta$  and  $\kappa_2$  that satisfy (25) also satisfies condition (26).

Consider now the generalization of (22) to evaluate  $\varepsilon_2(t)$  at every instant that  $\varepsilon_1(t)$  crosses the time axis. With  $j \geq 1$  and  $t_j < t_c$ , (23) can be rewritten as

$$-\kappa_2(t_c - t_j) \leq \varepsilon_2(t_j) \leq \kappa_2(t_c - t_j), \quad (27)$$

which analogously yields

$$\begin{cases} -\kappa_2(t_c - 2t_j + t_{j-1}) \leq |\varepsilon_2(t_{j-1})| \leq \\ \qquad \qquad \qquad \kappa_2(t_c - t_{j-1}), s_{1,j-1} = s_{2,j-1}, \\ -\kappa_2(t_c - 2t_j + t_{j-1}) \leq -|\varepsilon_2(t_{j-1})| \leq \\ \qquad \qquad \qquad \kappa_2(t_c - t_{j-1}), s_{1,j-1} \neq s_{2,j-1}, \end{cases} \quad (28)$$

where  $s_{1,j} = -s_{1,j-1}$ . By induction, we can deduce that if equation (28) holds true, assuming  $(t_{j-1}, \varepsilon_2(t_{j-1})) \in \mathcal{E}(\kappa_2)$ , then  $(t, \varepsilon_2(t)) \in \mathcal{E}(\kappa_2)$  for all  $t \in [t_{j-1}, t_j)$ . Additionally, it is noticeable that equation (28) is satisfied at every time instant  $t_j$ , computed from (11), utilizing the state vector at  $t_{j-1}$  as the initial condition and the same parameters  $\eta$  and  $\kappa_2$  that fulfill (25).

Therefore, a convergence rate  $\eta \geq 3$  and a switching gain  $\kappa_2$  that ensure equations (21) and (25) are satisfied, are sufficient to guarantee that  $(t_{j-1}, \varepsilon_2(t_{j-1})) \in \mathcal{E}(\kappa_2)$ ,  $\forall j = 1, 2, \dots, n_r$ . Consequently,  $\lim_{t \rightarrow t_c^-} \varepsilon_2(t) = 0$ , thus concluding the proof.  $\square$

The proofs of Corollary 1 and Theorem 1 guarantee the prescribed-time convergence of the complete state vector to the origin of the undisturbed system (6)–(7).

*Remark 1:* The definition of  $\mathcal{E}(\kappa_2)$  makes it evident that its bounding functions are directly influenced by the switching gain  $\kappa_2$ , which, as deduced from (21), relies on the initial value of  $\varepsilon_2(t)$ . Consequently, since the system parameters depend on its initial conditions, the proposed methodology cannot be classified as fixed-time stable. Furthermore, the initial states of the system are typically unknown in practical scenarios. Nevertheless, it is still feasible to empirically adjust the parameters  $\eta$  and  $\kappa_2$  to satisfy equations (21) and (25).

*Remark 2:* Obtaining a convergence proof for the proposed algorithm using conventional Lyapunov methods has

proven challenging. This difficulty arises because the method is nonautonomous and discontinuous within the specified interval  $[t_0, t_c)$ . Motivated by the linear time-response of  $\varepsilon_2(t)$ , we have explored an alternative approach to establish convergence, which involves employing a bounding region and utilizing the analytic solution of the algorithm in different segments of the prescribed interval.

We present a mathematical analysis in three parts to extend the results of Theorem 1 to disturbed systems. First, we propose formulating two new second-order systems perturbed by constant disturbances of amplitude  $L$  and  $-L$ . Second, we define the parameter conditions that ensure that the states of both systems converge to the origin at the prescribed time  $t_c$ . Finally, we demonstrate that the original system will also present prescribed-time convergence if we employ the same parameters that satisfy the conditions obtained in the second part of the analysis.

Consider the IVP consisting of (6)–(7) with a known initial condition  $\mathbf{e}(t_0) = (\varepsilon_1(t_0), \varepsilon_2(t_0)) \in \mathbb{R}^2$  and a bounded disturbance  $|\delta| \leq L$ , with known bound  $L$ . The bounding systems

$$\dot{\check{\varepsilon}}_1 = -\sigma(t, \check{\varepsilon}_1) + \check{\varepsilon}_2, \quad (29)$$

$$\dot{\check{\varepsilon}}_2 = -\kappa_2 \text{sign}(\check{\varepsilon}_1) - L, \quad (30)$$

and

$$\dot{\hat{\varepsilon}}_1 = -\sigma(t, \hat{\varepsilon}_1) + \hat{\varepsilon}_2, \quad (31)$$

$$\dot{\hat{\varepsilon}}_2 = -\kappa_2 \text{sign}(\hat{\varepsilon}_1) + L, \quad (32)$$

are obtained by replacing the disturbance  $\delta(t)$  by its minimum and maximum values, respectively. Consider also that these bounding systems, as well as the original one (6)–(7), have the same initial conditions and parameters.

The following theorem demonstrates that there exist sufficient conditions for the parameters  $\kappa_2$  and  $\eta$  which ensure that  $\check{\mathbf{e}}(t)$  and  $\hat{\mathbf{e}}(t)$  converge to the origin as  $t$  approaches  $t_c$ .

*Theorem 2:* Consider the IVPs consisting of (29)–(30) with a known initial condition  $\check{\mathbf{e}}(t_0) = \mathbf{e}(t_0)$ , and (31)–(32) with a known initial condition  $\hat{\mathbf{e}}(t_0) = \mathbf{e}(t_0)$ . Consider also a common parameter  $\eta \geq 3$  for both IVPs. If the following conditions are satisfied

$$(\kappa_2 - L)(t_c - t_0) \geq |\varepsilon_2(t_0)|, \quad (33)$$

$$\begin{aligned} -\kappa_2(t_c - \check{t}_1 - \check{s}_{1,0}(\check{t}_1 - \check{t}_0)) + L(t_c - \check{t}_0) \\ \leq \check{\varepsilon}_2(\check{t}_0) \leq \\ \kappa_2(t_c - \check{t}_1 + \check{s}_{1,0}(\check{t}_1 - \check{t}_0)) - L(t_c - 2\check{t}_1 + \check{t}_0). \end{aligned} \quad (34)$$

$$\begin{aligned} -\kappa_2(t_c - \hat{t}_1 - \hat{s}_{1,0}(\hat{t}_1 - \hat{t}_0)) + L(t_c - 2\hat{t}_1 + \hat{t}_0) \\ \leq \hat{\varepsilon}_2(\hat{t}_0) \leq \\ \kappa_2(t_c - \hat{t}_1 + \hat{s}_{1,0}(\hat{t}_1 - \hat{t}_0)) - L(t_c - \hat{t}_0), \end{aligned} \quad (35)$$

then both  $\check{\mathbf{e}}$  and  $\hat{\mathbf{e}}$  converge to zero at the prescribed time  $t_c$ .

*Proof:* The analytic solution to the IVP (29)–(30), in each interval  $t \in [\check{t}_{j-1}, \check{t}_j)$ , where  $\check{t}_j$  is defined analogously to (9) considering the current system, can be obtained

similarly to (11)–(12) as

$$\check{\varepsilon}_1(t) = \frac{t_c - t}{(\eta - 2)(\eta - 1)} \check{\alpha}(t) + \check{\beta}(\check{t}_{j-1}) \left( \frac{t_c - t}{t_c - \check{t}_{j-1}} \right)^\eta, \quad (36)$$

$$\check{\varepsilon}_2(t) = \check{\varepsilon}_2(\check{t}_{j-1}) - (\kappa_2 \check{s}_{1,j-1} + L) (t - \check{t}_{j-1}), \quad (37)$$

where  $\check{s}_{i,j-1} \triangleq \text{sign}(\check{\varepsilon}_i(\check{t}_{j-1}))$  and

$$\check{\alpha}(t) \triangleq (\kappa_2 \check{s}_{1,j-1} + L) (t_c - t - (\eta - 2)(t - \check{t}_{j-1})) + (\eta - 2) \check{\varepsilon}_2(\check{t}_{j-1}), \quad (38)$$

$$\begin{aligned} \check{\beta}(\tau) \triangleq & \check{\varepsilon}_1(\tau) - \frac{t_c - \tau}{\eta - 1} \check{\varepsilon}_2(\tau) \\ & - \frac{(t_c - \tau)^2}{(\eta - 2)(\eta - 1)} (\kappa_2 \check{s}_{1,j-1} + L). \end{aligned} \quad (39)$$

Since the analysis in the proof of Corollary 1 is also valid for system (29)–(30), it is also true that  $\check{\varepsilon}_1(t)$  approaches zero as  $t$  approaches  $t_c$ .

Similarly to the proof of Theorem 1, let us consider a geometric set  $\mathcal{E}^+(\kappa_d)$  defined as

$$\mathcal{E}^+(\kappa_d) \triangleq \{(t, x(t)) : -\kappa_d (t_c - t) \leq x(t) \leq \kappa_d (t_c - t)\}, \quad (40)$$

where  $x(t)$  is the evaluated state, and  $\kappa_d \triangleq \kappa_2 - L$ . Once again, by ensuring that  $(\check{t}_{j-1}, \check{\varepsilon}_2(\check{t}_{j-1})) \in \mathcal{E}^+(\kappa_d)$  for all  $j = 1, \dots, n_r$ , we guarantee that  $\lim_{t \rightarrow t_c^-} \check{\varepsilon}_2(t) = 0$ .

From (40) and the known values of  $\check{\varepsilon}_2(\check{t}_0)$  and  $L$ , by choosing  $\kappa_2$  satisfying

$$(\kappa_2 - L)(t_c - \check{t}_0) \geq |\check{\varepsilon}_2(\check{t}_0)|, \quad (41)$$

the pair  $(\check{t}_0, \check{\varepsilon}_2(\check{t}_0))$  will belong to  $\mathcal{E}^+(\kappa_d)$ .

From (37), we can evaluate the value of  $\check{\varepsilon}_2(\check{t}_1)$  as

$$\check{\varepsilon}_2(\check{t}_1) = \check{\varepsilon}_2(\check{t}_0) - (\kappa_2 \check{s}_{1,0} + L) (\check{t}_1 - \check{t}_0). \quad (42)$$

To ensure that  $(t, \check{\varepsilon}_2(t)) \in \mathcal{E}^+(\kappa_d)$  at  $\check{t}_1$ , it suffices to use the definition of  $\mathcal{E}^+(\kappa_d)$  to obtain

$$-\kappa_d(t_c - \check{t}_1) \leq \check{\varepsilon}_2(\check{t}_1) \leq \kappa_d(t_c - \check{t}_1), \quad (43)$$

which can be expanded using (42), yielding

$$\begin{aligned} -\kappa_2 (t_c - \check{t}_1 - \check{s}_{1,0} (\check{t}_1 - \check{t}_0)) + L (t_c - \check{t}_0) \\ \leq \check{\varepsilon}_2(\check{t}_0) \leq \\ \kappa_2 (t_c - \check{t}_1 + \check{s}_{1,0} (\check{t}_1 - \check{t}_0)) - L (t_c - 2\check{t}_1 + \check{t}_0). \end{aligned} \quad (44)$$

The instant  $\check{t}_1$  can be found by solving (36) for  $t$ , considering  $\check{\varepsilon}_1(t) = 0$  as well as parameters  $\eta \geq 3$  and  $\kappa_2$  satisfying equations (5) and (41). Similar to the undisturbed case, we ensure that  $(\check{t}_1, \check{\varepsilon}_2(\check{t}_1)) \in \mathcal{E}^+(\kappa_d)$  if  $\eta$  and  $\kappa_2$  are such that (44) holds true. Analogously, it can be shown by induction that these parameters also ensure that

$$\begin{aligned} -\kappa_d(t_c - \check{t}_j) \\ \leq \check{\varepsilon}_2(\check{t}_0) - \sum_{m=1}^j (\kappa_2 \check{s}_{1,m-1} + L) (t_m - t_{m-1}) \leq \\ \kappa_d(t_c - \check{t}_j) \end{aligned} \quad (45)$$

for every instant  $\check{t}_j$  obtained by inverting (36) considering  $\check{\varepsilon}_1(t) = 0$ . Therefore, there exist parameters  $\eta$  and  $\kappa_2$  such that  $(t, \check{\varepsilon}_2(t)) \in \mathcal{E}^+(\kappa_d)$ ,  $\forall t \in [t_0, t_c)$ .

The prescribed-time convergence of  $\hat{\varepsilon}_1(t)$  and existence of parameters that guarantee  $(t, \hat{\varepsilon}_2(t)) \in \mathcal{E}^+(\kappa_d)$ ,  $\forall t \in [t_0, t_c)$  can be analogously deduced. In this case, it suffices to satisfy the following inequality instead of (44)

$$\begin{aligned} -\kappa_2 (t_c - \hat{t}_1 - \hat{s}_{1,0} (\hat{t}_1 - \hat{t}_0)) + L (t_c - 2\hat{t}_1 + \hat{t}_0) \\ \leq \hat{\varepsilon}_2(\hat{t}_0) \leq \\ \kappa_2 (t_c - \hat{t}_1 + \hat{s}_{1,0} (\hat{t}_1 - \hat{t}_0)) - L (t_c - \hat{t}_0), \end{aligned} \quad (46)$$

where  $\hat{t}_1$  is obtained by inverting

$$\hat{\varepsilon}_1(t) = \frac{t_c - t}{(\eta - 2)(\eta - 1)} \hat{\alpha}(t) + \hat{\beta}(\hat{t}_0) \left( \frac{t_c - t}{t_c - \hat{t}_0} \right)^\eta, \quad (47)$$

considering  $\hat{\varepsilon}_1(t) = 0$ , and defining  $\hat{s}_{1,0} \triangleq \text{sign}(\hat{\varepsilon}_1(\hat{t}_0))$  and

$$\begin{aligned} \hat{\alpha}(t) \triangleq & (\kappa_2 \hat{s}_{1,0} - L) (t_c - t - (\eta - 2)(t - \hat{t}_0)) \\ & + (\eta - 2) \hat{\varepsilon}_2(\hat{t}_0), \end{aligned} \quad (48)$$

$$\begin{aligned} \hat{\beta}(\hat{t}_0) \triangleq & \hat{\varepsilon}_1(\hat{t}_0) - \frac{t_c - \hat{t}_0}{\eta - 1} \hat{\varepsilon}_2(\hat{t}_0) \\ & - \frac{(t_c - \hat{t}_0)^2}{(\eta - 2)(\eta - 1)} (\kappa_2 \hat{s}_{1,0} - L). \end{aligned} \quad (49)$$

Hence, if  $\eta$  and  $\kappa_2$  are chosen to simultaneously satisfy (44) and (46), then the solutions  $\check{\varepsilon}_2(t)$  and  $\hat{\varepsilon}_2(t)$  will remain in  $\mathcal{E}^+(\kappa_d)$ .  $\square$

*Corollary 3:* Consider the geometric set  $\mathcal{E}^+(\kappa_d)$ , and the IVPs (6)–(7), (29)–(30), and (31)–(32). The parameters which ensure the prescribed-time convergence of  $\check{\varepsilon}$  and  $\hat{\varepsilon}$  also ensure the prescribed-time convergence of  $\varepsilon$ .

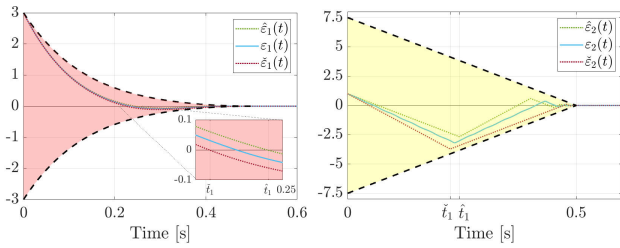
*Proof:* The proof of Theorem 2 readily implies that if the solutions of the IVPs for two systems, subject to constant disturbances whose amplitudes correspond to the maximum and minimum values of an unknown disturbance  $\delta$ , remain bounded by the geometric set  $\mathcal{E}^+(\kappa_d)$ , then the solution of the IVP for a system affected by the intermediate disturbance  $\delta$  will also remain bounded by this set.  $\square$

It is possible to obtain functions that delimit a similar geometric set for  $(t, \varepsilon_1(t))$  by replacing  $\varepsilon_2(t)$  in (6) by the upper and lower line segments that bound  $\mathcal{E}^+(\kappa_d)$ . Denote this set by  $\mathcal{Z}(\kappa_d) \triangleq \{(t, \varepsilon_1(t)) : -\lambda(t, \varepsilon_1) \leq \varepsilon_1(t) \leq \lambda(t, \varepsilon_1)\}$ , where  $\lambda(t, \varepsilon_1)$  is given by

$$\begin{aligned} \lambda(t, \varepsilon_1) \triangleq & \left( |\varepsilon_1(t_0)| - \frac{\kappa_d(t_c - t_0)^2}{\eta - 2} \right) \left( \frac{t_c - t}{t_c - t_0} \right)^\eta \\ & + \frac{\kappa_d(t_c - t)^2}{\eta - 2}. \end{aligned} \quad (50)$$

Thus, if inequalities (44) and (46) are satisfied, then the trajectories of  $\varepsilon_1$  and  $\varepsilon_2$  are confined in  $\mathcal{Z}(\kappa_d)$  and  $\mathcal{E}^+(\kappa_d)$ , respectively, for any instant  $t \in [t_0, t_c)$ .

*Corollary 4:* Consider the  $\sigma$ -function in (8) and the geometric sets  $\mathcal{Z}(\kappa_d)$  and  $\mathcal{E}^+(\kappa_d)$ . It holds that triggering the behavior switch of  $\sigma$  at an instant  $t$  slightly earlier than  $t_c$



**FIGURE 1.** State trajectories of the modified STA under different values of disturbance, with the geometric sets  $\mathcal{Z}(\kappa_d)$  shaded in red, and  $\mathcal{E}^+(\kappa_d)$  shaded in yellow.

is equivalent to starting a conventional STA with very small initial conditions.

*Proof:* Consider an instant  $t_e = (1 - \Delta)t_c$ , where  $\Delta \ll 1$  is a user-defined correction factor. With the proper choice of parameters, the time responses of  $\varepsilon_1$  and  $\varepsilon_2$  will be respectively enveloped by  $\mathcal{Z}(\kappa_d)$  and  $\mathcal{E}^+(\kappa_d)$  for all  $t \in [t_0, t_c)$ . Therefore, given that the functions that delimit these sets monotonically converge to the origin as  $t$  approaches  $t_c$ , as illustrated by the dashed lines in Figure 1, it is evident that any function enclosed by these sets will present a value very close to the origin at an instant close to  $t_c$ . From this instant forward, the conventional STA ensures the finite-time convergence of the system states to the origin.  $\square$

*Example 1:* Consider the systems (6)–(7), (29)–(30) and (31)–(32), with initial conditions  $\varepsilon(t_0) = \check{\varepsilon}(t_0) = \hat{\varepsilon}(t_0) = (3, 1)$  and  $t_0 = \check{t}_0 = \hat{t}_0 = 0$ . Consider that the original system is disturbed by  $\delta(t) = L \sin(50\pi t)$ , with  $L = 3$ . Figure 1 illustrates the simulated state trajectories of the three systems with parameters  $t_c = 0.5$  s,  $\eta = 5$ ,  $\kappa_1 = 5$ , and  $\kappa_2 = 18$ , which satisfy equations (5), (41), (44), and (46).

#### IV. STATE ESTIMATION OF A DISTURBED PENDULUM

In this section, the proposed algorithm is employed in formulating a state estimator for a free damped pendulum affected by a disturbance torque.

##### A. OBSERVER FORMULATION

The pendulum dynamics are described by

$$\ddot{\theta} = -a \sin(\theta) - \gamma \dot{\theta} + \frac{\nu}{ml^2}, \quad (51)$$

where  $\theta \in \mathbb{R}$ , and  $\dot{\theta} \in \mathbb{R}$  are the pendulum’s angular position and velocity, respectively,  $a \triangleq g/l$ ,  $\gamma \triangleq b/(ml^2)$ ,  $m$  is the pendulum mass,  $l$  is its length,  $g$  is the gravity acceleration,  $b$  is the friction coefficient, and  $\nu \in [-\rho, \rho]$  is a bounded disturbance torque.

By defining the state vector  $\mathbf{x} \triangleq (x_1, x_2) \in \mathbb{R}^2$ , with  $x_1 \triangleq \theta$  and  $x_2 \triangleq \dot{\theta}$ , and the disturbance input  $d \triangleq \nu/(ml^2) \in \mathbb{R}$ , we can rewrite (51) as

$$\dot{x}_1 = x_2, \quad (52)$$

$$\dot{x}_2 = f(\mathbf{x}) + d, \quad (53)$$

where  $f(\mathbf{x}) \triangleq -a \sin(x_1) - \gamma x_2$ . Let us assume that  $d$  is bounded according to  $d \in [-\rho/ml^2, \rho/ml^2]$ .

**TABLE 1.** Simulation parameters.

Symbol	Description	Value
$t_0$	Initial time	0 s
$T_s$	Integration step	0.0001 s
$l$	Pendulum length	3 m
$m$	Pendulum mass	1 kg
$g$	Gravity acceleration	9.81 m/s <sup>2</sup>
$b$	Friction coefficient	1 Nms
$x_1(t_0)$	Initial angle	0.5 rad
$x_2(t_0)$	Initial angular velocity	0 rad/s
$\hat{x}_1(t_0)$	Initial estimated state	0 rad
$\hat{x}_2(t_0)$	Initial estimated state	0 rad/s

Denote the state estimate by  $\hat{\mathbf{x}} \triangleq (\hat{x}_1, \hat{x}_2) \in \mathbb{R}^2$  and define the estimation error as  $\mathbf{e} \triangleq \mathbf{x} - \hat{\mathbf{x}}$ . By substituting the estimation error definition in (6)–(7), considering the pendulum dynamics in (52)–(53), the modified super-twisting sliding-mode observer (ModSTSMO) is given by

$$\dot{\hat{x}}_1 = \sigma(t, (x_1 - \hat{x}_1)) + \hat{x}_2, \quad (54)$$

$$\dot{\hat{x}}_2 = f(\hat{\mathbf{x}}) + \kappa_2 \text{sign}(\varepsilon_1). \quad (55)$$

In this case, the disturbance term in (7) is represented by  $\delta \triangleq (f(\mathbf{x}) - f(\hat{\mathbf{x}})) + d$ , thus containing both the model uncertainty and the external disturbance. Let us assume that  $\delta$  is bounded by  $\delta \in [-L, L]$ , with known  $L < \infty$ . The conventional super-twisting sliding-mode observer (STSMO) is analogously obtained by substituting the estimation error definition into (3)–(4) instead.

##### B. SIMULATION RESULTS

The simulation study is conducted in MATLAB using the first-order explicit Euler method. First, we present a numerical verification of the proposed observer’s robustness and prescribed-time convergence properties. Next, we present a comparative analysis between our proposed observer and another state-of-the-art prescribed-time convergent observer. Table 1 contains the adopted parameters.

The pendulum starts from rest and is disturbed by  $\nu = 0.8\rho \sin(2\pi t) + 0.2\rho \sin(20\pi t)$ , where  $\rho \triangleq ml^2$ , implying that  $d \in [-1, 1]$ . To account for the bounds of the external disturbance and model uncertainties in  $\delta$ , we adopt  $L = 3$ . Consider the observer parameters  $\kappa_1 = 6$ ,  $\kappa_2 = 12$ ,  $\eta = 5$ , and  $t_c = 0.5$  s. Figures 2–3 show the system states, their estimates, and the estimation error, respectively. Verifying that the chosen parameters satisfy the gain criteria (5) and inequality (41) is straightforward. Also, by following the procedure in Theorem 2, inequality (44) is reduced to  $-1.04 \leq \check{\varepsilon}_2(t_0) \leq 5.37$ , whereas inequality (46) leads to  $-1.51 \leq \hat{\varepsilon}_2(t_0) \leq 4.5$ . Since  $\varepsilon_2(t_0) = \hat{\varepsilon}_2(t_0) = \check{\varepsilon}_2(t_0) = 0.5$  rad, both inequalities hold true.

The previous simulation is repeated with the same parameters, except for the convergence instant, now set to  $t_c = 1$  s. The results are shown in Figures 4–5. In all the simulated cases, the prescribed instant  $t_c$  is the exact settling instant, and the states remain stable thereafter.

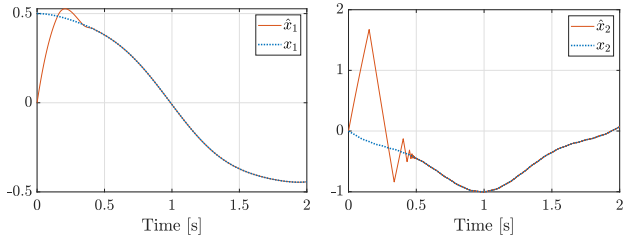


FIGURE 2. Time response of the system states and its estimates obtained with the proposed observer set with  $t_c = 0.5$  s.

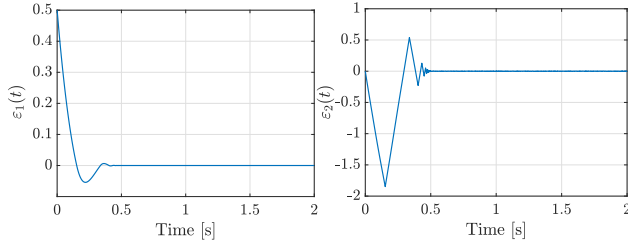


FIGURE 3. Time response of the state estimation error obtained with the proposed observer set with  $t_c = 0.5$  s.

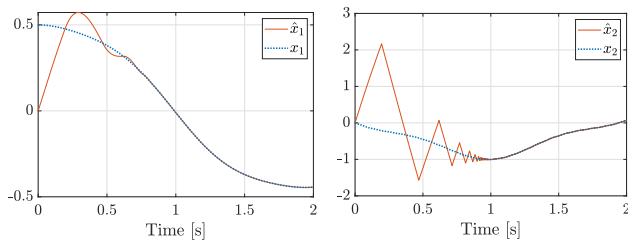


FIGURE 4. Time response of the system states and its estimates obtained with the proposed observer set with  $t_c = 1$  s.

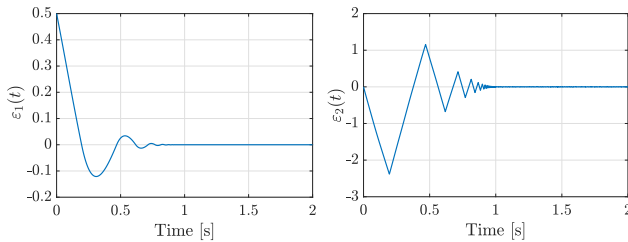


FIGURE 5. Time response of the state estimation error obtained with the proposed observer set with  $t_c = 1$  s.

Now, the proposed observer is compared to one of the most recently developed methods for second-order estimators with prescribed-time convergence, named here as prescribed-time observer (PTO) [13]. This method uses time-varying gains in both component state equations to drive the system to the origin at precisely the specified instant. As the PTO has been defined only in  $[t_0, t_c)$ , for fairness of comparison, here we extend it with the conventional STSMO in  $t \geq t_c$ , yielding

$$\dot{\hat{x}}_1 = g_1(t, \varepsilon_1) + \hat{x}_2, \quad (56)$$

$$\dot{\hat{x}}_2 = g_2(t, \varepsilon_1) + f(\hat{x}), \quad (57)$$

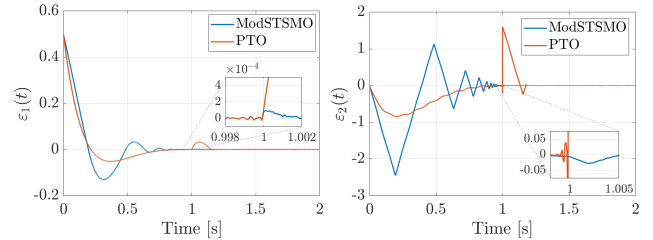


FIGURE 6. Comparative simulations: time response of the ModSTSMO and PTO estimation errors with  $t_c = 1$  s.

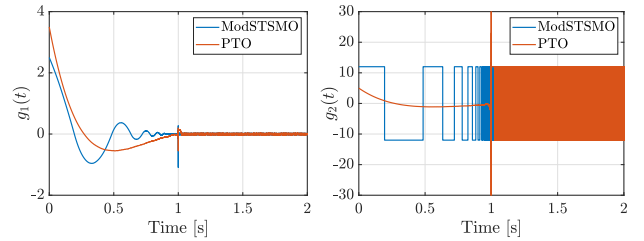


FIGURE 7. Comparative simulations: time response of the ModSTSMO and PTO injection terms, with  $t_c = 1$  s.

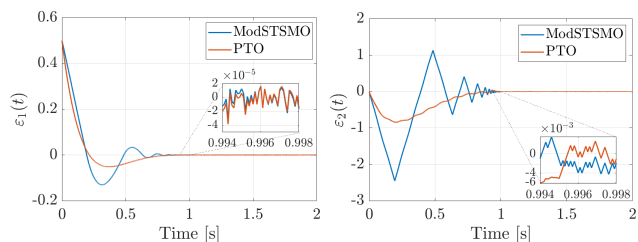
where the injection terms are

$$g_1(t, \varepsilon_1) \triangleq \begin{cases} \left( \ell_1 + 2 \frac{m+2}{t_c-t} \right) \varepsilon_1, & t \in [t_0, t_c), \\ \kappa_1 |\varepsilon_1|^{1/2}, & t \in [t_c, \infty), \end{cases} \quad (58)$$

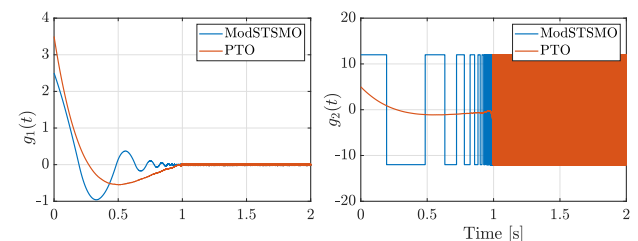
$$g_2(t, \varepsilon_1) \triangleq \begin{cases} \left( \ell_2 + \ell_1 \frac{m+2}{t_c-t} + \frac{(m+1)(m+2)}{(t_c-t)^2} \right) \varepsilon_1, & t \in [t_0, t_c), \\ \kappa_2 \text{sign}(\varepsilon_1), & t \in [t_c, \infty). \end{cases} \quad (59)$$

The following simulations consider that the angle measurements contain additive zero-mean truncated Gaussian noise with a standard deviation of  $10^{-5}$  on support  $[-5 \times 10^{-5}, 5 \times 10^{-5}]$ . Also, to compare the injection terms, we consider that for the proposed method,  $g_1(t) = \sigma(t, \varepsilon_1)$  and  $g_2(t) = \kappa_2 \text{sign}(\varepsilon_1)$ . Considering the parameters  $\eta = 5, \kappa_1 = 6, \kappa_2 = 12, t_c = 1$  s,  $\ell_1 = 3, \ell_2 = 2$ , and  $m = 1$ , we obtain the results shown in Figures 6–7.

The PTO method presents numerical problems near the prescribed instant  $t_c$ , as the gains go to infinity while multiplied by a noisy estimation error [13]. Although a similar behavior can be observed in the proposed method, the PTO is shown to be much more susceptible to this effect, as it uses time-varying gains to multiply the estimation error in both observer equations. To mitigate this problem, we adopt an earlier switching instant to the conventional STSMO behavior, as introduced in Corollary (4). With a correction factor  $\Delta = 0.005$ , we trigger the behavior switch at  $t_e = 0.995$  s. Although this approach sacrifices the exactness of the converging instant, Figures 8–9 show that this change eliminates the state divergence caused by the measurement error.



**FIGURE 8. Comparative simulations: time response of the ModSTSMO and PTO estimation errors with  $t_c = 1$  s, considering an earlier switching instant  $t_e = 0.995$  s.**



**FIGURE 9. Comparative simulations: time response of the ModSTSMO and PTO injection terms with  $t_c = 1$  s, considering an earlier switching instant  $t_e = 0.995$  s.**

**V. CONCLUSION**

The present paper introduced a modification of the super-twisting algorithm. It showed that, with the appropriate selection of parameters, the transitory behavior of its states remains enveloped by time functions that approach the origin as time approaches the prescribed instant of convergence. Compared to a similar algorithm, our method shows convergence at the prescribed instant, maintaining robust stability thereafter, with a minor sensitivity to inaccurate measurements. In future works, the effectiveness of the proposed method will be evaluated in practical scenarios.

**REFERENCES**

[1] A. Levant, “Robust exact differentiation via sliding mode technique,” *Automatica*, vol. 34, no. 3, pp. 379–384, Mar. 1998.

[2] J. A. Moreno and M. Osorio, “Strict Lyapunov functions for the super-twisting algorithm,” *IEEE Trans. Autom. Control*, vol. 57, no. 4, pp. 1035–1040, Apr. 2012.

[3] J. Davila, L. Fridman, and A. Levant, “Second-order sliding-mode observer for mechanical systems,” *IEEE Trans. Autom. Control*, vol. 50, no. 11, pp. 1785–1789, Nov. 2005.

[4] H. Castañeda, O. S. Salas-Peña, and J. de León Morales, “Adaptive super twisting flight control-observer for a fixed wing UAV,” in *Proc. Int. Conf. Unmanned Aircr. Syst. (ICUAS)*, May 2013, pp. 1004–1013.

[5] I. Boiko and M. Chehadeh, “Sliding mode differentiator/observer for quadcopter velocity estimation through sensor fusion,” *Int. J. Control*, vol. 91, no. 9, pp. 2113–2120, 2018.

[6] J. F. Silva and D. A. Santos, “Attitude determination for multicopter aerial vehicle using a super-twisting sliding mode observer,” in *Proc. 26th Int. Congr. Mech. Eng. (COBEM)*, 2021.

[7] S. K. Kommuri, S. Han, and S. Lee, “External torque estimation using higher order sliding-mode observer for robot manipulators,” *IEEE/ASME Trans. Mechatronics*, vol. 27, no. 1, pp. 513–523, Feb. 2022.

[8] R. Seeber, M. Horn, and L. Fridman, “A novel method to estimate the reaching time of the super-twisting algorithm,” *IEEE Trans. Autom. Control*, vol. 63, no. 12, pp. 4301–4308, Dec. 2018.

[9] A. Polyakov, “Nonlinear feedback design for fixed-time stabilization of linear control systems,” *IEEE Trans. Autom. Control*, vol. 57, no. 8, pp. 2106–2110, Aug. 2012.

[10] E. Cruz-Zavala, J. A. Moreno, and L. M. Fridman, “Uniform robust exact differentiator,” in *Proc. 49th IEEE Conf. Decis. Control (CDC)*, 2010, pp. 2727–2733.

[11] R. Seeber, H. Haimovich, M. Horn, L. M. Fridman, and H. De Battista, “Robust exact differentiators with predefined convergence time,” *Automatica*, vol. 134, Dec. 2021, Art. no. 109858.

[12] Y. Song, Y. Wang, J. Holloway, and M. Krstic, “Time-varying feedback for regulation of normal-form nonlinear systems in prescribed finite time,” *Automatica*, vol. 83, pp. 243–251, Sep. 2017.

[13] J. Holloway and M. Krstic, “Prescribed-time observers for linear systems in observer canonical form,” *IEEE Trans. Autom. Control*, vol. 64, no. 9, pp. 3905–3912, Sep. 2019.

[14] D. Gómez-Gutiérrez, “On the design of nonautonomous fixed-time controllers with a predefined upper bound of the settling time,” *Int. J. Robust Nonlinear Control*, vol. 30, no. 10, pp. 3871–3885, 2020.

[15] R. Aldana-López, R. Seeber, D. Gómez-Gutiérrez, M. T. Angulo, and M. Defoort, “A redesign methodology generating predefined-time differentiators with bounded time-varying gains,” *Int. J. Robust Nonlinear Control*, vol. 33, no. 15, pp. 9050–9065, 2022.

[16] Y. Orlov, R. I. Verdés Kairuz, and L. T. Aguilar, “Prescribed-time robust differentiator design using finite varying gains,” *IEEE Control Syst. Lett.*, vol. 6, pp. 620–625, 2022.

[17] J. F. Silva and D. A. Santos, “A modified super-twisting algorithm with specified settling time,” in *Proc. 16th Int. Workshop Variable Struct. Syst. (VSS)*, Sep. 2022, pp. 1–5.

[18] R. Seeber, “Generalized Filippov solutions for systems with prescribed-time convergence,” 2023, *arXiv:2303.03133*.

[19] Y. Orlov, “Finite time stability and robust control synthesis of uncertain switched systems,” *SIAM J. Control Optim.*, vol. 43, no. 4, pp. 1253–1271, Jan. 2004.

[20] Y. Orlov, Y. Aoustin, and C. Chevallereau, “Finite time stabilization of a perturbed double integrator—Part I: Continuous sliding mode-based output feedback synthesis,” *IEEE Trans. Autom. Control*, vol. 56, no. 3, pp. 614–618, Mar. 2011.



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