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# Dynamic Ron Effect in GaN HEMT in a Zero-Voltage-Switching Circuit Due to Off-Resonance Operation

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**ABSTRACT** Dynamic ON resistance of GaN devices is a must-care point for users. In this paper, the reverse conduction of commercial GaN power transistors is studied. Even though the commercial HEMTs show stable performance in normal operation modes (off-to-on), significant dynamic ON resistance can be seen in some particular conditions. A test method is set up to evaluate dynamic  $R_{on}$  in a reverse-to-on mode. The conditions to activate the behavior are discussed, and the cause of dynamic  $R_{on}$  is possibly due to traps located in the gate region. Meanwhile, a wireless power transfer system operating at 6.78MHz is used to study the effect of reverse conduction mode on dynamic resistance at the circuit level. According to the change of the operation frequency, we find that the influence of reverse conduction on the dynamic  $R_{on}$  effect is not only affected by the value of reverse conduction voltage but also related to the operating mode of the device.

**INDEX TERMS** GaN, dynamic resistance, wireless power transfer, reverse conduction.

## I. INTRODUCTION

GaN HEMT is emerging as a promising candidate for next-generation power switching applications [1]. Throughout the years, many kinds of application schemes for GaN HEMT had been proposed. But one critical factor that needs solving before such a new scheme can address a mass market is its reliability [2], [3].

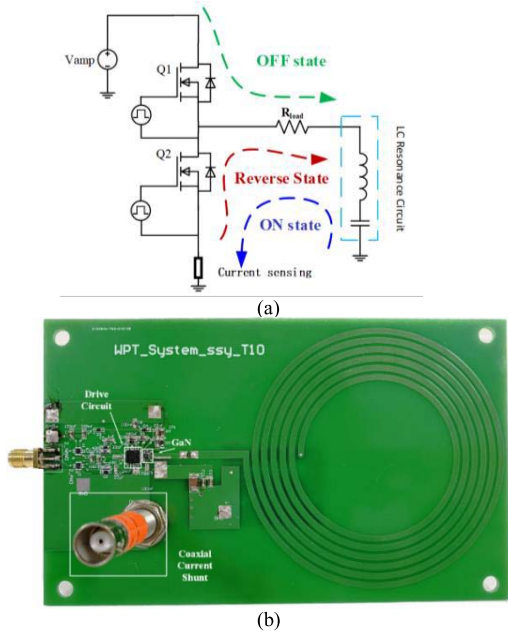
One of the reasons that cause reliability problems in GaN devices is the dynamic ON-resistance ( $R_{on}$ ) effect [4]. Dynamic  $R_{on}$  characteristics, the fact that GaN HEMT  $R_{on}$  does not remain constant, has attracted much attention. It will seriously limit the output power and efficiency of the device [5]. In addition, dynamic  $R_{on}$  could also cause reliability problems when the device operates for a long time [6].

However, most of the previous studies focus on off-state stress and the on-state behavior of GaN HEMT [7]. What happens in reverse conduction for GaN needs much more understanding. Despite the disproportionately little attention

it has drawn, reverse conduction is quite common in systems with an inductive or an LC resonant load.

In recent years, magnetic resonance wireless power transfer (WPT) has developed rapidly because of its advantages, such as long transmission distance and high efficiency [8]. AirFuel standard (A4WP) stipulates that the operation frequency of magnetic resonance wireless power transfer is 6.78MHz [9]. Compared with Si power devices, GaN HEMT is more suitable for this application.

In this paper, we studied the influence of reverse conduction on the dynamic  $R_{on}$  effect of commercial GaN devices. Firstly, we built a special test circuit that makes the device operate in a reverse-to-on mode to study the dynamic  $R_{on}$  effect on the device level. Secondly, a class-D zero-voltage-switching (ZVS) magnetic resonance WPT system with an LC resonant tank is built using GaN HEMT to observe the influence of reverse conduction mode on the dynamic  $R_{on}$  of the device on the circuit level. LTspice is used for simulation analysis. The original study is done in a WPT system. But



**FIGURE 1. (a) Simplified circuit diagram of the GaN half-bridge WPT system studied. (b) Photo of the transmitter of the magnetic resonance WPT system.**

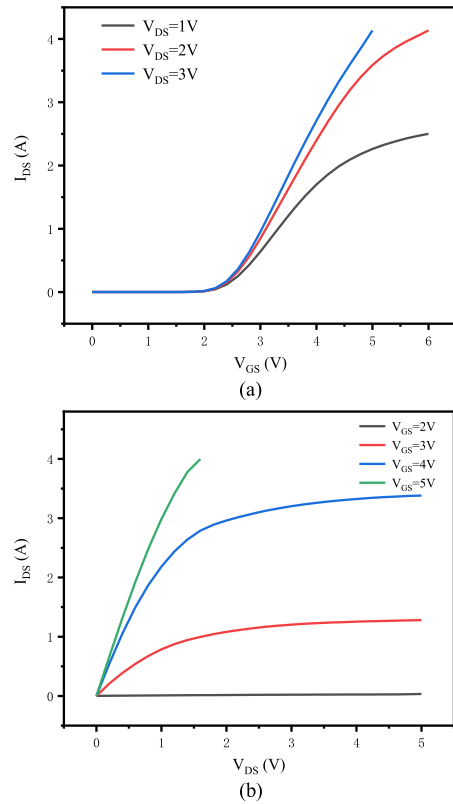
the findings can be general for other systems with a similar mode of operations.

## II. EXPERIMENT AND METHOD

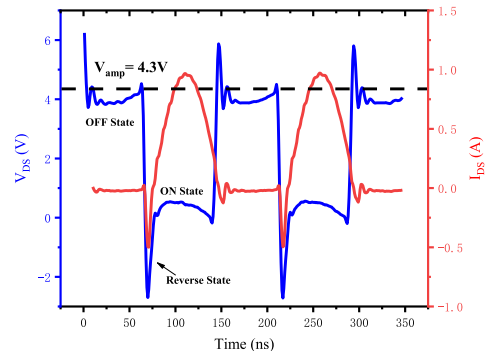
Fig. 1(a) shows a schematic of the WPT system. Reference [10] explains the details of this circuit.  $R_{load}$  is the equivalent resistance mapped to the transmission side from the receiver load. Three current paths are corresponding to the three states in Fig. 1(a). When  $Q_2$  turns off, and  $Q_1$  turns on, the current charges the LC resonance tank along the green line. Before  $Q_2$  turns on and  $Q_1$  turns off, there is a dead time when both GaN HEMTs are off. At the same time, the inductor current must be continuous, which makes  $Q_2$  operate in the reverse state (red line). After that,  $Q_2$  turns on, while  $Q_1$  turns off. The current flows along the blue line. Compared with the off-to-on mode in most previous studies, a special operation mode exists for  $Q_2$ : off-reverse-on.

Fig. 1(b) shows the photo of the magnetic resonance WPT system. Two EPC2107 GaN HEMTs were used to form a half-bridge [11]. The chip (EPC2017) consists of three transistors, two of which serve as half-bridge circuits and one that replaces the diode in the bootstrap circuit.  $R_{on}$  of the low-side GaN HEMT ( $Q_2$ ) was measured, and the DC characteristics are shown in Fig. 2. The drive circuit chip used LM5113 produced by Texas Instruments. A coaxial current shunt (part SSDN-10 manufactured by T&M Research Products Inc.) is used to detect the current flowing through the  $Q_2$  [12]. The reverse conduction can be further observed from the voltage waveform of  $Q_2$ , as shown in Fig. 3. The negative overshoot indicates the reverse state of  $Q_2$ .

To evaluate the effect of the reverse state on  $R_{on}$ , a special operation mode, reverse-to-on, is constructed through a separate setup shown in Fig. 4.  $V_{amp}$  and  $V_R$  are DC power



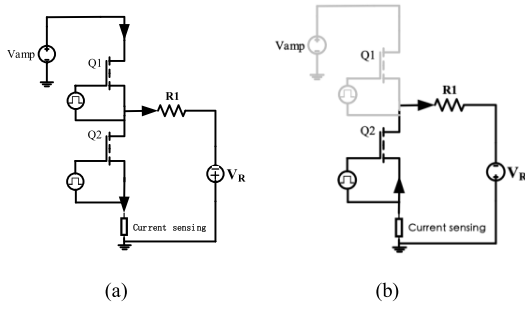
**FIGURE 2. DC performance of the  $Q_2$  (EPC2107) which is tested by Keysight B1505A. (a) The transfer characteristic of the  $Q_2$  under different  $V_{DS}$ . (b) The output characteristic of  $Q_2$  under different  $V_{GS}$ .**



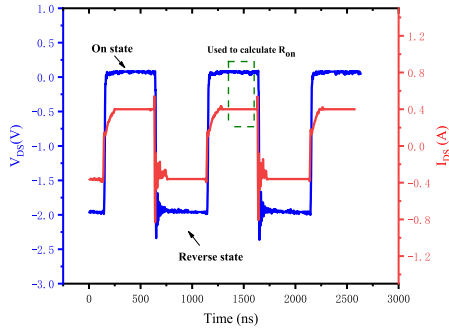
**FIGURE 3. Measured  $V_{DS}$  and  $I_{DS}$  for  $Q_2$  in a real WPT system. The  $V_{amp}$  is 4.3 V, and the test frequency is 6.78MHz. The  $V_{GS-On State}$  is 5 V.**

sources.  $Q_1$  and  $Q_2$  are turned on and off at the same time. For  $Q_2$ ,  $V_{amp}$  provides a positive voltage at on state.  $V_R$  provides a negative voltage and introduces reverse conduction. In Fig. 4 (a), the current flows through  $Q_2$  when both devices are turned on. When the devices are off ( $V_{GS}$  is 0 V),  $Q_2$  operates in a reverse state (Fig. 4 (b)).

The  $R_{on}$  of the low-side GaN device ( $Q_2$ ) is measured in on state. The setup senses the voltage ( $V_{DS}$ ) and current ( $I_{DS}$ ) of  $Q_2$  in real-time.  $V_{DS}$  can be obtained using an oscilloscope. A coaxial current shunt is used to detect the current. One example of the  $V_{DS}$  and  $I_{DS}$  waveforms is shown in Fig. 5. With caution, we can accurately measure



**FIGURE 4.** A special test circuit to make the  $Q_2$  operate in reverse-to-on mode. (a) The  $Q_2$  operates in an on state. (b) The  $Q_2$  operates in a reverse state.



**FIGURE 5.** The  $V_{DS}$  (blue) and  $I_{DS}$  (red) are the waveforms of  $Q_2$  operating in reverse-to-on mode. The  $V_{amp}$  is 0.3 V, and the test frequency is 1 MHz.

$R_{on} = V_{DS}/I_{DS}$  by averaging the data in the dotted box in Fig. 5.

The ON-state current is kept at 0.4 A to avoid  $R_{on}$ 's change due to the bias condition ( $I_{DS}$ ) shift. A limited number of pulses are transmitted to the gate to reduce the impact of self-heat effect.

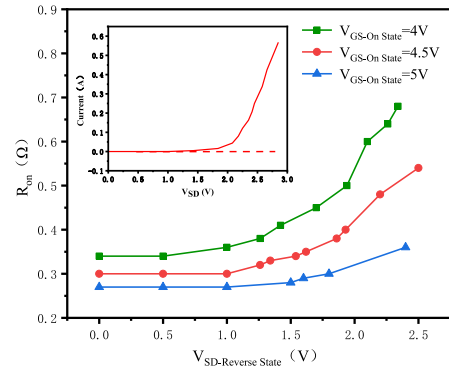
### III. RESULT AND DISCUSSION

#### A. EFFECT OF REVERSE CONDUCTION IN DEVICE LEVEL

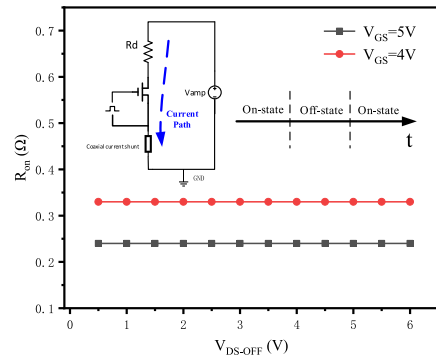
Fig. 6 shows the  $R_{on}$  with  $V_{SD-Reverse State}$  under different  $V_{GS-On State}$  (the test circuit is shown in Fig. 4).  $R_{on}$  increases the most when  $V_{SD-Reverse State}$  is high and  $V_{GS-On State}$  is low. According to the official EPC report: When the  $R_{on}$  of the device under dynamic conditions exceeds the static value by 20 %, it is considered that the device has a dynamic  $R_{on}$  [13]. For  $V_{GS-On State}$  of 4 V, with the  $V_{SD-Reverse State}$  increases from 0 V to 2 V.  $R_{on}$  increases from 0.33  $\Omega$  to 0.55  $\Omega$ , or over 60 % (green curve). It is illustrated that the device has a dynamic  $R_{on}$  effect in this mode. This rise in the dynamic  $R_{on}$  is dangerous for the circuit, which brings risks to the system.

The device turns on at reverse state, relying on  $V_{SD}$  ( $V_{GS}$  is 0 V). The  $V_{SD}-I_{SD}$  is shown in the inset of Fig. 6. With the increase of  $V_{SD-Reverse State}$  in this mode, the generation of dynamic  $R_{on}$  of the device requires the device to turn on at reverse state.

To determine whether such behavior (Fig. 6) is due to reversely biasing the gate [14], we performed the test in



**FIGURE 6.**  $R_{on}$  changes with  $V_{SD-Reverse State}$  under different  $V_{GS-On State}$ . The circuit operation frequency is 1 MHz, and  $V_{amp}$  is less than 1 V to guarantees the  $I_{DS-On State} = 0.4A$ . The inset figure is the  $V_{SD}-I_{SD}$  of the device under  $V_{GS}$  is 0 V. As the  $V_{SD}$  exceeds 1.25 V, the device will produce the reverse current.



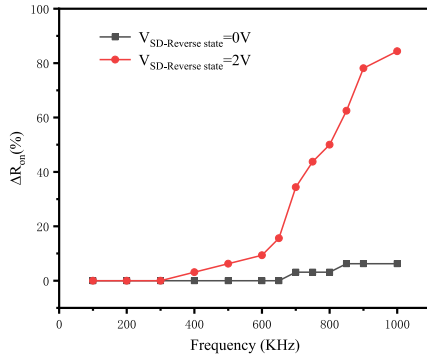
**FIGURE 7.** The device operates in a traditional switching mode (1 MHz). The red curve is with  $V_{GS}$  of 4 V. The black curve is with  $V_{GS}$  of 5 V. The test circuit is in the upper left corner.

Fig. 7. The device operates in a traditional on-to-off switching mode. In such a case, the gate-to-drain diode is reversely biased in an off state. As the  $V_{DS-OFF}$  reaches 6 V, there is little dynamic  $R_{on}$  in both curves. Hence, the answer to the question is negative.

We have swapped the source and drain's position of the device  $Q_2$  in Fig. 4 and repeated the measurement. The source of the  $Q_2$  is connected to  $Q_1$ , and the drain is connected to current sensing. A similar dynamic  $R_{on}$  phenomenon shows up in this condition. Therefore, such behavior is not because the drain is further away from the gate than the source.

This dynamic  $R_{on}$  effect also depends on the operating frequency. Fig. 8 shows that as the frequency increases above 300 kHz, the red curve rises rapidly, while the black curve remains almost unchanged. Therefore, the higher the operating frequency, the greater the influence of reverse conduction on the dynamic  $R_{on}$  [15].

Given the experimental data above, we postulate that certain types of shallow traps exist underneath the gate. They might be from the gate, the AlGaIn barrier [16], or the GaN buffer [17]. The most likely location of the traps is in the gate, though the exact position is still under investigation.



**FIGURE 8.** Dynamic  $R_{on}$  is a function of frequency.  $V_{GS}$  is 4 V. The black curve is  $V_{SD-Reverse State} = 0$  V, and the red curve is  $V_{SD-Reverse State} = 2$  V. The frequency increases from 100 kHz to 1 MHz. The  $V_{amp}$  is 0.4 V.

Several factors are needed to activate these traps: 1) some mild positive bias across the gate, so the device is not fully turned on (semi-on state). 2) Enough reverse conduction voltage ( $V_{SD-Reverse State}$ ). 3) Significant channel current to provide the source of electrons. 4) A proper operating frequency, probably determined by the time constants of these traps. As the phenomenon becomes more obvious with higher frequency, these are likely shallow traps [18].

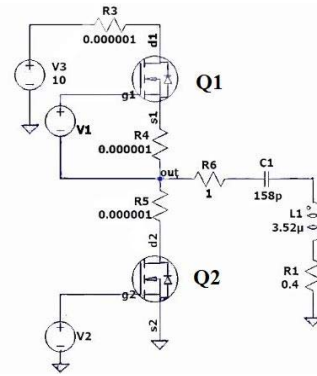
One mechanism can explain this phenomenon. When the device is reverse conducting, the value of  $V_{SD-Reverse State}$  is much higher than the normally  $V_{DS-On state}$ . The higher  $V_{SD-Reverse State}$  will generate a larger electric field in the device channel, and the  $I_{SD-Reverse State}$  provides a source of electrons. It will make the hot electron effect more likely to occur and lead  $R_{on}$  of the device to increase under high operation frequency [19], [20].

### B. EFFECT OF REVERSE CONDUCTION IN CIRCUIT LEVEL

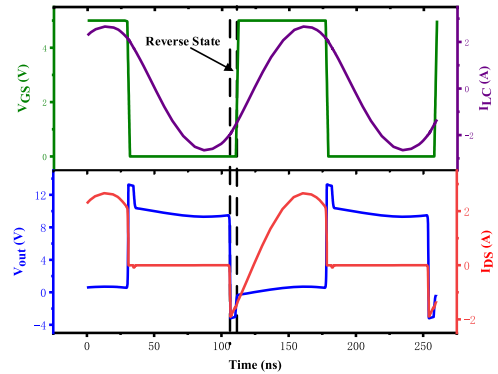
One factor that causes the device to appear reverse conduction in the system is the operating frequency. In a real WPT system, because the uniformity and processing accuracy of the components may cause the resonant frequency of the LC tank ( $f_{LC tank}$ ) to deviate from the operating frequency ( $f_{operation}$ ). So in this part, we study the influence of reverse conduction on the dynamic  $R_{on}$  of the device under different operating frequency.

First, we explain the reason why reverse conduction appears when the  $f_{LC tank}$  deviates from the  $f_{operation}$ . Fig. 9 is the schematic of the LTspice simulation circuit for the WPT system.  $V_1$  and  $V_2$  can generate square wave signals ( $V_{GS-On State} = 5$  V) with a phase difference of  $180^\circ$ . The model of the GaN device (GaN EPC2107) is from the EPC official website. The  $V_{amp}$  is a DC power source.  $C_1$  and  $L_1$  are composed of LC resonance circuit (LC tank).  $R_6$  is Equivalent load resistance and  $R_1$  is parasitic resistance coming from layout, packaging, and so on.

Fig. 10 is our simulation result. The  $f_{operation}$  is 6.8 MHz which is higher than  $f_{LC tank}$  (6.78MHz). Because  $f_{operation} > f_{LC tank}$ , the inductive of the LC tank causes the phase displacement between input current ( $I_{LC}$ ) and voltage



**FIGURE 9.** The schematic of magnetic resonance WPT system simulated by LTspice.



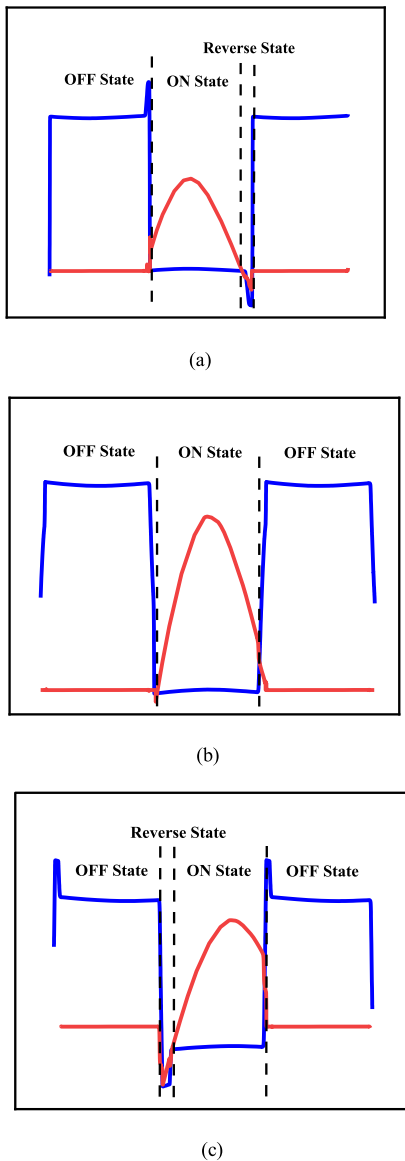
**FIGURE 10.** The reverse state appears for the device ( $Q_2$ ) in a WPT system. The  $V_{amp}$  is 10V. The green, red and blue curves are  $V_{GS}$ ,  $I_{DS}$ , and  $V_{DS}$ , respectively, for  $Q_2$  (in Fig. 9). The purple curve is the current flowing through the LC tank.

( $V_{out}$ ) [21]. To ensure the continuity of the inductor current, the reverse conduction appears for the device when  $V_{GS} = 0$  V (between two dashed lines). The reverse conduction voltage ( $V_{SD-Reverse State}$ ) is related to  $I_{LC}$  and  $f_{operation}$ .

Fig. 11 shows the operation mode of the GaN device under different  $f_{operation}$  in the WPT system. When  $f_{operation} < f_{LC tank}$ , the GaN device operation in off-on-reverse mode (Fig. 12 (a)) within one cycle. When  $f_{operation} = f_{LC tank}$ , the device reaches the ideal operating state and operates in off-to-on mode (Fig. 13 (b)). When  $f_{operation} > f_{LC tank}$ , the GaN device operates in off-reverse-on mode (Fig. 11 (c)).

Fig. 12 shows the relationship between the  $\Delta R_{on}$  of the device and reverse-conducting time under different  $V_{SD Reverse State}$ . When the  $V_{SD Reverse State}$  exceeds 1.5 V, the device will reverse conduction. So there is no dynamic  $R_{on}$  effect on the blue curve. The device has a dynamic  $R_{on}$  effect when the reverse conduction time exceeds 14 ns for the red curve. As the reverse conduction time increases, the dynamic  $R_{on}$  effect continues to deteriorate ( $\Delta R_{on} = 54\%$  at  $T_{Reverse State}$  is 32 ns). It is illustrated that the deterioration of the dynamic  $R_{on}$  of the device is both related to the  $V_{SD Reverse State}$  and the reverse conduction time.

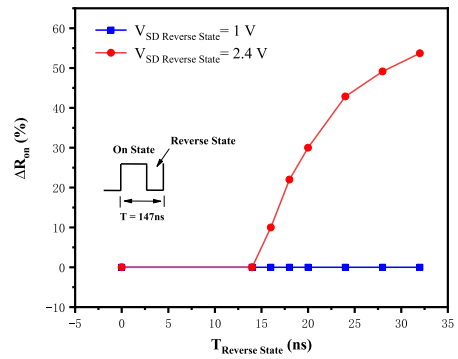
Fig. 13 shows the measurement result of the  $R_{on}$  and  $I_{LC}$  at different  $f_{operation}$  in a real WPT system. Fig. 1 (b) is



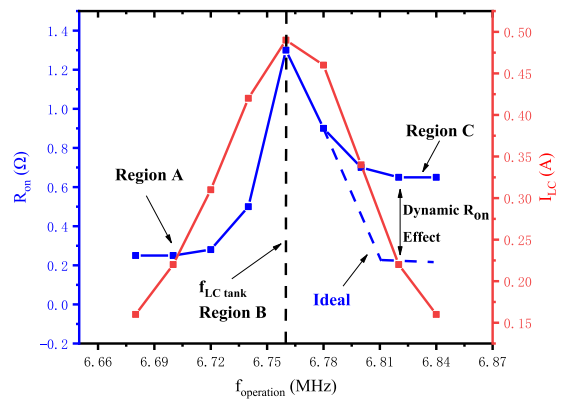
**FIGURE 11.** The operation mode of the device ( $Q_2$ ) under different operation frequencies in one cycle. The blue curve is the  $V_{DS}$ , and the red curve is the  $I_{DS}$  of the  $Q_2$ .

the photo of the WPT system, and Fig. 9 is the schematic of this system. In Fig. 13, the region A, region B, and region C corresponds to the  $Q_2$  operating in Fig. 11 (a), Fig. 11 (b), and Fig. 11 (c) modes, respectively. In our test, the  $V_{GS-On State}$  is 5 V (recommended by vendor) and the  $V_{amp} = 5$  V. The  $f_{LC tank}$  is 6.76 MHz, and load resistance ( $R_6$  in Fig. 9) is 0  $\Omega$ . In Fig. 13, the red curve reaches its maximum value (0.48 A) when  $f_{operation} = f_{LC tank}$  at 6.76 MHz (black dotted line) and decreases as the  $f_{operation}$ , and  $f_{LC tank}$  deviation is greater. The changing trend of the  $R_{on}$  is similar to the  $I_{LC}$ . The difference is that the  $R_{on}$  in region A is 0.25  $\Omega$ , while it is 0.6  $\Omega$  in region C.

The variation of the red curve can be explained by equation (1). When  $f_{operation} = f_{LC tank}$ ,  $Z_{LC tank}$  is the smallest and the  $I_{LC}$  of the system is the largest. When  $f_{operation}$  deviates from the  $f_{LC tank}$ , the  $Z_{LC tank}$  increases and the  $I_{LC}$



**FIGURE 12.** The relationship between  $\Delta R_{on}$  and reverse state time. The test circuit is shown in Fig. 3. The test frequency is 6.78MHz, and the  $V_{GS-On State}$  is 5 V. The blue curve is  $V_{SD Reverse State} = 1$  V, and the red curve is  $V_{SD Reverse State} = 2.4$  V.



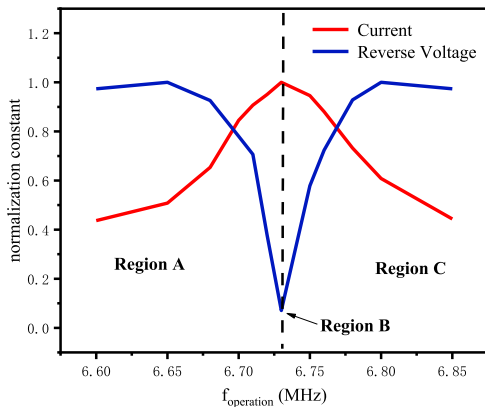
**FIGURE 13.** The blue curve is the  $R_{on}$  of the GaN device ( $Q_2$ ) and the red curve is  $I_{LC}$  (RMS) for the WTP system. The X-axis is  $f_{operation}$ .

decreases.

$$Z_{LC tank} = 2\pi L f_{operation} + \frac{1}{2\pi C f_{operation}} \quad (1)$$

For the blue curve, in the region I,  $I_{LC}$  is small and the  $R_{on}$  is the same as the static value of the device. As the  $f_{operation}$  rises, the larger  $I_{LC}$  makes the self-heating effect more serious, leading to the  $R_{on}$  of the device increasing [22]. Ideally, in region C, the small  $I_{LC}$  makes  $R_{on}$  decrease, such as the blue dotted line. However, in region C (solid line), the  $R_{on}$  of the device (0.6  $\Omega$ ) is increased by 140 % compared to the region A (0.25  $\Omega$ ) in our test. A noticeable dynamic  $R_{on}$  effect appears in this operating condition.

The simulation (LTspice) is used to analyze this phenomenon in Fig. 14. The vary of the  $I_{LC}$  is the same as the test results in Fig. 13. The blue curve is the reverse conduction voltage ( $V_{SD-Reverse State}$ ). Three regions are shown in Fig. 14, which is the same as Fig. 13. When the system is operating in region A and region C, reverse conduction is both appeared. In our test (Fig. 13), the  $V_{SD-Reverse State}$  can reach 4 V in region A and region C, which is similar to the simulation results. But in Fig. 13, only the dynamic  $R_{on}$  effect appears in region C. It is illustrated that the influence of reverse conduction on the dynamic  $R_{on}$  effect is also related to the operating mode of the device.



**FIGURE 14.** The simulation of the device in different operating frequencies. The schematic of the circuit is shown in Fig. 9. The red curve is  $I_{LC}$ , and the blue curve is reverse voltage ( $V_{SD-Reverse State}$ ).

We consider that the cause of this phenomenon is likely to be related to the traps inside the device, but the specific trap characteristics and mechanisms are still under study.

#### IV. CONCLUSION

In this research, we study the influence of reverse conduction on the dynamic characteristics of commercial GaN devices. A special reverse-to-on mode is used to study the device's dynamic  $R_{on}$  effect at the device level. The dynamic  $R_{on}$  is highly probable to appear in high  $V_{SD-Reverse State}$ , low  $V_{GS-On state}$  and high frequency. The cause of dynamic  $R_{on}$  may be the traps located in the gate region. The traps might be induced by non-uniform material growth or device processing. Because more than 50 devices are tested in the experiment. These devices come from different batches. About 60% of these devices show dynamic  $R_{on}$  in this mode of operation. Our research considers that for EPC2107, the reverse conduction voltage should be less than 2V (when  $V_{GS-On State} = 5 V$ ).

At the circuit level, we analyze the device operation mode under different operating frequency. We found that the dynamic  $R_{on}$  effect of the device is not only affected by the value of reverse conduction voltage but also related to the operating mode of the device in the system. Compared with the off-on-reverse mode, the off-reverse-on mode could make the dynamic  $R_{on}$  more susceptible to reverse conduction. Meanwhile, we suggest that future reliability standards consider including the test measurement mentioned in this paper to ensure the reliability of product operation.

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