

# Note Clarifying the Paper, “Charge Sheet Super Junction in 4H-Silicon Carbide: Practicability, Modeling and Design”

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**ABSTRACT** This note clarifies an important approximation used to simulate the breakdown field in the SiO<sub>2</sub> liner of a SiC Charge-Sheet Superjunction - a new power device structure - reported by Akshay and Karmalkar (2020). This electric field simulation sought to assure that the new device does not suffer from SiO<sub>2</sub> reliability problems. The note answers two questions: (a) Why do we remove the SiO<sub>2</sub> liner which is the very region of our interest during device simulation, when a simulator allows inclusion of such a region? (b) How can one solve for the field in a region (SiO<sub>2</sub> in the present case) by neglecting that very region during device simulations? Our note reinforces the insight – “Modeling is the art of making approximations.”

**INDEX TERMS** 4H-SiC, breakdown voltage, specific on-resistance, TCAD simulation, analytical model.

## I. INTRODUCTION

This note is related to an accompanying paper [1] which discussed the practicability, modeling and design of a variation of the Superjunction (SJ) called the Charge Sheet SJ (CSSJ) in 4H-Silicon Carbide (SiC) material (see Fig. 1(a)). Here a thin Al<sub>2</sub>O<sub>3</sub> layer deposited on a thermally grown SiO<sub>2</sub> liner in an etched trench replaces the p-pillar of the SJ. The Al<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub> interface has a negative fixed charge of magnitude  $N_I$  which acts like the ionized dopant charge of the p-pillar and can be controlled via the Al<sub>2</sub>O<sub>3</sub> deposition temperature.

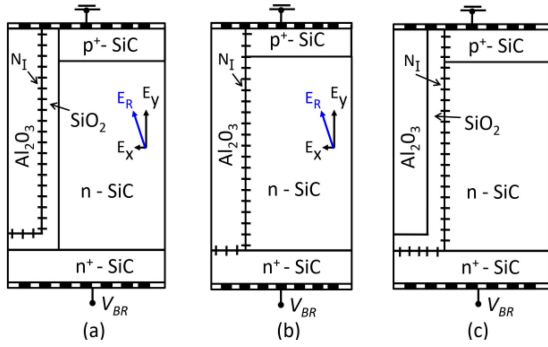
In any SiC power device operating in the OFF state, when the bias is raised, the field in SiO<sub>2</sub> can exceed its critical field of  $\sim 5$  MV/cm well before the field in SiC reaches its critical value of  $\sim 3$  MV/cm, if the field at the SiO<sub>2</sub>/SiC interface has a significant normal component. This is because, as per Gauss’s law, the normal field in SiO<sub>2</sub> is  $\epsilon_{SiC}/\epsilon_{SiO_2} \approx 2.5$  times of that in SiC, where  $\epsilon_{SiC}$  and  $\epsilon_{SiO_2}$  are the dielectric constants of SiO<sub>2</sub> and SiC. Hence, while designing SiC power devices containing a SiO<sub>2</sub> layer, it is important to ascertain by 2D/3D numerical simulation that the field in the SiO<sub>2</sub> layer remains well below  $\sim 5$  MV/cm when the SiC region breaks down.

Accordingly, Fig. 3(c) of [1] which is reproduced here as Fig. 2(a), reported the simulated resultant field,  $E_{R,SiO_2}$ , in the SiO<sub>2</sub> layer of our proposed CSSJ when the SiC region of this device breaks down, and confirmed that this  $E_{R,SiO_2}$  remains well below 5 MV/cm. It is the purpose of the present note to clarify an important approximation employed in [1] to simulate  $E_{R,SiO_2}$ .

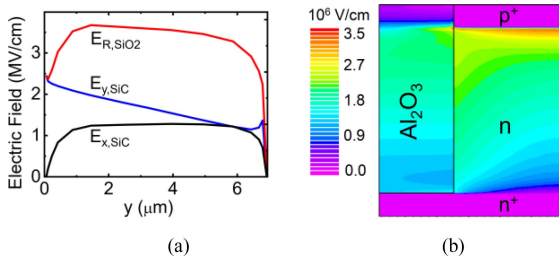
## II. THE APPROXIMATION

Instead of simulating  $E_{R,SiO_2}$  in the actual structure of Fig. 1(a) directly, we simulated the field distribution in the structure shown in Fig. 1(b), where the SiO<sub>2</sub> layer was removed and  $N_I$  was placed at the Al<sub>2</sub>O<sub>3</sub>/SiC interface. From this distribution, which is reproduced here in Fig. 2(b) from Fig. 3(a) of [1], we obtained the fields  $E_{y,SiC}$  and  $E_{x,SiC}$  in SiC that are parallel and normal to the vertical Al<sub>2</sub>O<sub>3</sub>/SiC interface (see Fig. 2(a)). Then, we derived  $E_{R,SiO_2}$  shown in Fig. 2(a) by applying Gauss law as per which  $E_y$  is continuous across the vertical SiO<sub>2</sub>/SiC interface while the field  $E_x$  in SiO<sub>2</sub> is  $\epsilon_{SiC}/\epsilon_{SiO_2} \approx 2.5$  times that in SiC, so that

$$E_{R,SiO_2} = \sqrt{E_{y,SiC}^2 + (2.5E_{x,SiC})^2}. \quad (1)$$



**FIGURE 1.** (a) Cross-section of the unit cell of the proposed Charge-Sheet SuperJunction [1]. Diagram not to scale; the actual  $\text{SiO}_2$  liner is much thinner than shown. (b) A variation of (a) with  $\text{SiO}_2$  liner removed. (c) A variation of (a) with the negative interface charge  $N_I$  moved to the  $\text{SiO}_2/\text{SiC}$  interface.



**FIGURE 2.** Simulations at breakdown in a 4H-SiC Charge-Sheet SuperJunction with  $W_n = 0.7 \mu\text{m}$ ,  $W_l = 0.5 \mu\text{m}$ ,  $L = 7 \mu\text{m}$ ,  $N_d = 1 \times 10^{17} \text{cm}^{-3}$ ,  $N_I = N_d W_n = 7 \times 10^{12} \text{cm}^{-2}$  and  $V_{BR} = 1 \text{ kV}$ ; reproduced from [1]. (a) Components of the n-pillar field ( $E_{y,SiC}$  and  $E_{x,SiC}$ ) and the resultant field in  $\text{SiO}_2$  liner ( $E_{R,SiO2}$ ) along the vertical  $\text{Al}_2\text{O}_3/\text{SiC}$  interface, over the pillar length,  $L$ . (b) Field contours.

The motivation for and the validity of the above approximate procedure are explained below. We did not consider the  $E_{R,SiO2}$  along the horizontal  $\text{SiO}_2/\text{SiC}$   $n^+$  region interface, since this field would be rather low, as anticipated from the  $\sim 1 \text{ MV/cm}$  field along the  $\text{Al}_2\text{O}_3/\text{SiC}$   $n^+$  region interface in Fig. 2 (b).

First, we answer the question: Why do we remove the  $\text{SiO}_2$  liner which is the very region of our interest during simulation, when a simulator allows inclusion of such a region? The Silvaco device simulator [2] employed by us can simulate the  $\text{Al}_2\text{O}_3 / \text{SiO}_2/\text{SiC}$  system of Fig. 1(a) but only *without* the interface charge,  $N_I$ . This is because  $N_I$  happens to be at  $\text{Al}_2\text{O}_3 / \text{SiO}_2$  which is an insulator / insulator interface, and the simulator does not allow placing of a charge at an insulator / insulator interface. Hence our device structure cannot be simulated as it is. However, the simulator allows the placing of an interface charge at a semiconductor / insulator interface such as  $\text{Al}_2\text{O}_3/\text{SiC}$  in Fig. 1(b) or  $\text{SiO}_2/\text{SiC}$  in Fig. 1(c). Hence, the variations Fig. 1(b),(c) of the actual structure of Fig. 1(a) can be simulated. However, the field in the  $\text{SiO}_2$  layer of Fig. 1(c) will not be the same as that of Fig. 1(a); this is because, unlike the  $\text{SiO}_2$  layer of Fig. 1(a), the  $\text{SiO}_2$  layer of Fig. 1(c) will not experience the field lines which emanate from the ionized donors of n-SiC and terminate on  $N_I$ . Hence, we need to work with the structure of Fig. 1(b) in simulations.

Next we answer the question: How can one solve for the field in a region ( $\text{SiO}_2$  in the present case) by neglecting that very region during the simulations? This is possible if the field in the region of interest depends on that in another region of the device, whose field is however negligibly dependent on the region of interest. Consider an analogy: we can solve for  $x$  in the following equation

$$e^x = 1000 + x \quad (2)$$

by neglecting the very  $x$  to be solved for on the RHS, because contribution of  $x$  to the RHS is small, i.e.,  $x \ll 1000$ ; this is confirmed from the fact that  $x = \ln 1000 = 6.91$  obtained by this approach is indeed only 0.691% of 1000. Yet another analogy is the derivation of the text book ideal diode equation

$$I = I_0(e^{V/V_t} - 1) \quad (3)$$

where  $I_0$  is the reverse saturation current and  $V_t$  is the thermal voltage. This equation is based on the law of the junction, namely – at applied bias  $V$ , the minority carrier concentration at the depletion edge is  $e^{V/V_t}$  times the equilibrium concentration at the same location. This law is derived by neglecting the very  $I$  to be solved for compared to the average drift and diffusion currents over the depletion width. Apart from this quasi-equilibrium approximation, the quasi-static and quasi-neutrality approximations commonly employed in semiconductor device modeling can also be shown to follow the approach of neglecting the very quantity being solved for somewhere in the initial stages of the solution [3].

Returning to the question at hand, the  $\text{SiO}_2$  liner thickness ( $\sim 7 \text{ nm}$ ) is  $\ll \text{Al}_2\text{O}_3$  (500 nm) or SiC n-pillar thickness (700 nm). Hence neither removal of this liner nor relocation of  $N_I$  from the  $\text{Al}_2\text{O}_3/\text{SiO}_2$  interface to the SiC surface affect the n-pillar field. Thus, the simulated field distributions in the SiC and  $\text{Al}_2\text{O}_3$  regions of Fig. 1(b) would be almost the same as those in Fig. 1(a). Hence, the  $E_{R,SiO2}$  derived from the SiC region fields using (1) would match the actual  $E_{R,SiO2}$  from the  $\text{SiO}_2$  region fields using (1). The validity of our approximation is further confirmed by the fact that, in Fig. 2(a), over most of the pillar length, the simulated  $E_{x,SiC}$  matches the value  $qN_I/\epsilon_{SiC}\epsilon_0$  where  $N_I = 7 \times 10^{12} \text{cm}^{-2}$  as predicted by sound analytical theory.

### III. CONCLUSION

We have clarified an elegant approximation employed in [1] to numerically simulate the field in the  $\text{SiO}_2$  layer of the Charge-Sheet Superjunction overcoming the interface charge placement limitation of the device simulator. Our present approximation was shown to be a case of transfer of an existing approach to new surroundings. Our note reinforces the insight – “Modeling is the art of making approximations.”

### REFERENCES

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